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AERODYNAMIC CHARACTERISTICS AT M = 4.3 OF MONOPLANE, TRIFORM AND CRUCIFORM SLENDER DELTA WING BODIES WITH ALL-MOVING TAIL CONTROL SURFACES

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Summary

Supersonic wind tunnel tests were made over an incidence range from -4 to +30 degrees for a range of roll angles on a series of conical slender delta wing and body combinations with a short afterbody on which a rectangular tail control surface is mounted.

An examination is made of the characteristics of the wing and body combination and the approximate contributions of the individual wing panels are deduced.

The effectiveness of the tail control surfaces as stabilisers and as controls is examined for three different sizes of gap between the control and the wing trailing edge. The non linear behaviour of the controls tested is attributed at low incidences to the viscous losses due to the wing wake, and at high incidence to the influence of the expansion field from the wing trailing edge.

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* Replaces R.A.E. Technical Report 66343 - A.R.C. 28800

CONTENTS

1 INTRODUCTION

Engineering problems arising in the design of vehicles where there is a restriction in the permissible wing span of the vehicle. In such circumstances configurations based on the slender wing and body concept have much to commend them to the missile designer. Theoretically at least, they have the aerodynamic advantage of only small movements of aerodynamic centre over a considerable range of Mach number; thus the problem of guidance and control should prove simpler than in the case of non-slender combination where large movements are often encountered. A better behaviour of the aerodynamic characteristics at high lift might also be anticipated since the development of flow separations is known to be more orderly on slender wings.

The purpose of the present investigation is to examine experimentally the characteristics of slender shapes and, in particular, to study the effectiveness of the tail surfaces as controls and stabilisers. The configurations studied include combinations with either two, three or four wing panels. This study, which was confined to a conical wing body combination, was made at a Mach number of 4.3 in a small, 11 inch x 6 inch, supersonic wind tunnel at R.A.E. Farnborough.

In Section 4 the measured characteristics of the model with two wing panels is discussed with particular reference to the influence of the wings on the behaviour of the rear control surfaces. In Section 5 the variation of normal force, rolling moment and control behaviour with roll angle is examined for the various wing body combinations. Appendix A gives some notes on the theoretical methods applied and Appendix B gives tabulated results of the tunnel measurements.

2 DESCRIPTION OF THE MODELS TESTED

Fig.1 gives a sketch of the model with two wing panels. The wings have a delta planform of aspect ratio $\frac{1}{2}$ and an aerodynamic mean chord of 4 in. The section is formed from a flat plate which is chamfered at the leading and trailing edges. The basic body is a cone of 3° semi angle having a common apex with the wing panels and giving a ratio of body diameter to wing span of approximately 0.42. A short cylindrical extension of the cone aft of the wing trailing edge forms the afterbody on which the control surfaces are mounted with their hinge lines co-planar with the wing planes. The control surfaces,

of rectangular planform, have the same span as the wing panels and a chord of 0.60 of the body diameter giving a net aspect ratio of 1.16. The controls are hinged at their mid-chord points and may be mounted at three interchangeable positions behind the trailing edge giving gaps, of the minimum clearance practicable, and of 1.0 and 2.0 times the control chord. The models with three and four wing panels are constructed similarly but with angles of 120° and 90° respectively between the planes of the adjacent wing panels.

The notation used to designate the various configurations is given below:-

W_N - the combination of wing and the enveloped conical body; the subscript N denoting the number of wing panels,

W_NB - the wing-body combination with the cylindrical afterbody added to W_N,

$W_NBC^{F,M,R}$ - the wing-body-control combination; the superscript denoting the forward, middle and rear location of the control respectively.

The deflections of the controls is given in terms of a rotation $\xi_{y,-y,z,-z}$ about the hinge line and is considered positive for a clockwise rotation when viewed from inboard. The subscripts denote the axes to which each control hinge line is parallel. The axes are defined later. (No special notation has been introduced for the three panel combinations since only the -z control was deflected in the present tests.) The elevator angle, η, is defined in terms of the individual deflection by

$$\eta \equiv \tfrac{1}{2}(\xi_y - \xi_{-y}) \quad ;$$

and the aileron angle, ξ, is defined by

$$\xi \equiv \frac{1}{N} \times \begin{pmatrix}\text{Sum of the deflection} \\ \text{angles of the individual panels}\end{pmatrix} \quad .$$

3 DESCRIPTION OF TESTS

The tests were made in the No.6 (11 inch x 6 inch) supersonic wind tunnel at R.A.E. Farnborough at a Mach number of 4.3 and a Reynolds number of 10^6 based on the aerodynamic mean chord of the wing of 4 inches. The model was mounted on a rear sting balance which was fitted with a wind shield, and was strain gauged to measure normal force, side force pitching moment, yawing

moment and rolling moment. The table below gives the range of incidence, roll angle and control settings covered by the test programme.

Configuration	Body incidence σ(degrees)	Roll angle λ(degrees)	Control angle η, ξ_{-z} (degrees)
W_2	-5(1)5 6(2)30	0(5)90,	-
W_3	-5(1)5 6(2)30	0(5)60,	-
W_4	-5(1)5 6(2)30	0(5)45,	-
W_2B	-5(1)5 6(2)30	0	-
W_2BC^F	-5(1)5 6(2)30	0	η, -20(5)20
W_2BC^M	-5(1)5 6(2)30	0	η, -20(5)20
W_2BC^R	-5(1)5 6(2)30	0	η, -20(5)20
W_3BC^R	-4(4)28	0, (15) 180	ξ_{-z}, 0 and ±20
W_4BC^F	-4(4)28	0, (15) 180	ξ_{-z}, 0 and ±20
W_4BC^R	-4(4)28	0, (15) 180	ξ_{-z}, 0 and ±20

In this table λ is the roll angle and σ is the body incidence in the text σ is replaced by α for $\lambda = 0$.

The forces and moments were measured relative to a right-handed system of body fixed axes O, x, y, z as shown in the sketch given in Fig.2. The x axis is positive forwards and and y axis is fixed in the plane of the starboard wing panel for combinations with W_2 and W_4, but for W_3 the negative z axis is contained in the vertical wing panel. In presenting the results an alternative axis system, O, x', y', z' is also used where Oy' and Oz' are rotated anti-clockwise about the Ox axis through the angle λ such that the Oz' axis lies in the plane containing the Ox axis and the wind vector.

The pitching and yawing moments are referred to a point located at 2/3 of the root chord of the wing (i.e. axis through the mid point of the aerodynamic mean chord). The coefficients have been reduced to a non-dimensional form using a common wing area S_W and length $\bar{\bar{c}}$ for S for all the combinations tested.

$$C_{y,y',z,z'} = \frac{Y, Y', Z, Z'}{q S_W}$$

$$C_{m,m',n,n'} = \frac{M, M', N, N'}{q S_W \bar{\bar{c}}}$$

$$C_\ell = \frac{L}{q\, S_W\, 2s}$$

where S_W is the gross wing area of W_2 (i.e. including the area of the cone), $\bar{\bar{c}}$ aerodynamic mean chord, s is the semi span of W_2 and q the kinetic pressure.

The probable accuracy of the model settings and flow conditions are listed below.

σ, α	$\pm 0.02^\circ$
ξ_y etc	$\pm 0.2^\circ$
λ	$\pm 0.25^\circ$
M	± 0.03
q	$\pm 0.2\%$ due to variation in stagnation pressure H_∞.

The accuracy of the measured coefficients is

$C_{y,y',z,z'}$	± 0.004
$C_{m,m',n,n'}$	± 0.002
C_ℓ	± 0.0001

these have been assessed from the repeatability and consistency of the strain gauge measurements and therefore do not include any errors arising from asymmetries of the model.

4 DISCUSSION OF THE RESULTS : COMBINATIONS WITH W_2 AT ZERO ROLL ANGLE

4.1 Body and cone (W_2)

The normal force coefficient C_z is shown plotted against incidence in Fig.3 together with an estimate of the slope at zero incidence given by equation (A1) (Appendix A), which was obtained from Ref.4. The estimated value is approximately 3% lower than the theoretical value given by linearised theory for the basic thin wing, and it appears to underestimate slightly the measured values. It can be seen that there is a considerable amount of non linear lift at high incidence accounting for some 30% of the total lift at 30° incidence.

The normal force curve can be closely fitted by the simple quadratic* form

$$-C_z = 0.625\,\alpha + 0.92\,\alpha|\alpha| \quad , \qquad (1)$$

where α is in radians. A comparison of this result with the empirical method given by Collingbourne[3] suggests that for $\alpha < 12^\circ$ the non linear term can almost entirely be accounted for by the vortex normal force contribution.

Shock waves are detached from the leading edge of the wing as is clearly seen from the table below which gives the Mach number, M_n, and incidence normal to the leading edge, α_n, together with the maximum deflection angle, θ_{max}, for an oblique shock wave.

α degrees	10	20	30
M_n	0.9	1.6	2.2
α_n degrees	59	71	77
θ_{max} degrees	-	15	26

Pitching moments and centres of pressure locations are shown in Figs.4 and 5. The centre of pressure is ahead of the theoretical position for the equivalent thin wing; that is at 2/3 of the root chord from the apex, although one might have expected that the presence of the cone would have produced a centre of pressure slightly aft of this point. There is an indication that the centre of pressure moves forward with increasing incidence which might be attributable to a flow separation from the upper surface near the trailing edge although no evidence of this could be obtained by oil flow studies.

The somewhat erratic behaviour of the centre of pressure for small incidences shown in Fig.5 is partly due to inaccuracy in the measurements, although it was found that the model had small asymmetry at the trailing edge, which was displaced by about 0.002 in. from the plane of the wing due to a manufacturing error when the edge was chamfered.

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* This quadratic form, $\alpha|\alpha|$, was found to fit the measurements better than the form $\alpha^{1.7}$ suggested for low speeds by Smith[2].

4.2 Wing body combination (W_2B)

Fig.3 shows a slight increase in the normal force when the afterbody is present both in the linear and non linear components. The effect on pitching moment shown in Fig.4 is seen to be quite considerable, giving an aft movement of the centre of pressure of 0.34 body diameter at low incidence and 0.52 at 30°. The rearward movement of the centre of pressure with incidence can be associated with the non linear normal force due to cross flow separation over the afterbody, and the non linear development of the downwash at high incidence. The latter effect arises from the existence of leading edge vortices and modifications in the spanwise loading distribution when the flow is separated from the leading edge, or from the development of strong shock waves at the trailing edge.

4.3 Wing-body-control ($W_2BC^{F,M,R}$)

The normal force, pitching moment, and centre of pressure for zero control angle are shown in Figs.3, 4 and 5.

The normal force and pitching moment variations with control settings from -20 to +20 are shown in Figs.6 to 11 for the three control locations. The greatly increased control power for the rear control location is immediately obvious. The corresponding curves of C_m against $-C_z$ are given in Figs.12, 13 and 14 which also include the curves for W_2 and W_2B for comparison. The value of the derivative $-\partial C_m/\partial C_z$, which may be regarded as a measure of the longitudinal static stability, is seen to be remarkably constant for zero control angle for all these control locations. However, there is a marked effect of control deflection on this stability parameter which is dependent on the location of the control, and Fig.12 shows that for the forward control location there is a very large destabilising influence with positive elevator angle. At high incidence there is a consistent trend shown by all the control locations in which there is a destabilising effect for negative elevator angles and a slightly stabilising effect of positive angles.

The table given below helps to put these changes in perspective by giving the range of travel for each configuration of the neutral point, which in the present context is loosely defined as the point at which $\partial C_m/\partial C_z = 0$.

		W_2BC^F	W_2BC^M	W_2BC^R
Distance of neutral point aft of the datum for the range $-4^\circ < \alpha < 30^\circ$ and $-20^\circ < \eta < 20^\circ$	Forward limit	0.050 $\bar{\bar{c}}$ 0.48 d	0.056 $\bar{\bar{c}}$ 0.53 d	0.056 $\bar{\bar{c}}$ 0.53 d
	Aft limit	0.092 $\bar{\bar{c}}$ 0.88 d	0.103 $\bar{\bar{c}}$ 0.98 d	0.114 $\bar{\bar{c}}$ 1.09 d
Range of travel		0.042 $\bar{\bar{c}}$ 0.40 d	0.047 $\bar{\bar{c}}$ 0.45 d	0.058 $\bar{\bar{c}}$ 0.56 d

The range of travel is seen to be of the order of half a calibre with a tendency to increase with increase in control moment arm. This adverse effect is however more than compensated for by the rapid increase in the power of the control with increase in tail arm.

The characteristics of the controls are given in more detail in Figs. 15, 16 and 17. Fig. 15 gives the increment in pitching moment, ΔC_{m_c}, produced by the addition of the undeflected control surface to the basic body wing combination W_2B in the three control positions; whilst Figs. 16(a), (b) and (c) give the increments in pitching moments, ΔC_{m_η}, due to deflection of the control. These increments are evaluated for a given incidence from

$$\Delta C_{m_c} = C_m(W_2BC \text{ with } \eta = 0) - C_m(W_2B)$$

$$\Delta C_{m_\eta} = C_m(W_2BC \text{ with controls at angle } \eta) - C_m(W_2BC \text{ with } \eta = 0)$$

where η is the elevator control angle (i.e. $\eta = \frac{1}{2}[\xi_y - \xi_{-y}]$). The corresponding increments in normal force ΔC_{z_η} are given in Fig. 17 for specific incidences, however, they could not be determined with very great accuracy since they involved differencing two relative large quantities. For this reason the data obtained from the pitching moments have been used in analysing the control characteristics.

Fig. 16(c) shows that even for the rear control location the control moment is a non linear function both of control angle and incidence, and

Fig.16(b) and 16(a) show that the non linear behaviour gets pregressively worse as the gap between the control and the wing trailing edge is reduced. Possible explanations for this non linear behaviour are not hard to find as the list given below indicates.

1 At the high Mach number of these tests the normal force on the control is a non linear function of local flow direction.

2 There are viscous losses since the control is immersed in the low energy air of the wing wake.

3 The wing downwash angle is a non linear function of incidence.

4 Conditions at the control may be influenced by local expansion fields from the wing trailing edge.

5 The control deflection may provoke a separation of the flow on the wing itself.

The last mentioned is probably reason for the low effectiveness for the forward controls with positive elevator angles as shown in Fig.16(a), whereas viscous losses are almost certainly the explanation of the low effectiveness at small incidence shown in Figs.16(a), (b) and (c) for all control locations.

The magnitude of the effect of the high Mach number on the linearity of the control characteristics can be assessed from Fig.18(a), which presents the calculation of the normal force for the control section using the exact two dimensional shock expansion theory. The factor F given in Fig.18(b) shows that at 20° incidence the exact value exceeds the linearised value (i.e. $4\alpha/\beta$) by some 40%. This high Mach effect can therefore be expected to account, at least in part, for the non linearity of the control moments. However the influence of the non linearity of the downwash has yet to be examined.

Before proceeding further it is convenient to introduce two quantities k and k_η which defined as the stabiliser effectiveness and control effectiveness of the control surfaces by the following equations,

$$\text{Stabiliser effectiveness}, \; k \equiv \frac{\Delta C_{m_c} \; (\eta = 0)}{(K_{B(C)} + K_{C(B)}) \frac{4\alpha}{\beta} \left(1 - \frac{1}{2 A_N \beta}\right) \frac{\ell_c}{\bar{c}} \frac{S_C}{S_W}} \quad , \qquad (2)$$

and control effectiveness;

$$k_\eta \equiv \frac{(d\Delta C_m/d\eta)\ \eta = 0}{(k_{B(C)} + k_{C(B)})\ \frac{4}{\bar{\beta}}\left(1 - \frac{1}{2\ A_N\ \bar{\beta}}\right)\ \frac{\ell_c}{\bar{\bar{c}}}\ \frac{S_C}{S_W}} \qquad (3)$$

where $K_{B(C)}$, $K_{C(B)}$, $k_{B(C)}$ and $k_{C(B)}$ are wing-body interference factors as defined in Ref.5; other quantities are defined in Appendix A. The denominator in the definitions represents the estimated value according to linearised theory, but with the omission of the wing downwash correction in the definition of k. If linearity is assumed then approximately, by using the theoretical results given in Appendix A equations (A3) and (A5), these effectiveness factors can be interpreted as

$$k \approx \frac{q_\ell(\alpha)}{q_\infty}\ \frac{\bar{\beta}_\infty}{\bar{\beta}_\ell}\left(1 - \frac{\bar{\varepsilon}}{\alpha}\right) \qquad (4)$$

and

$$k_\eta \approx \frac{q_\ell(\alpha)}{q_\infty}\ \frac{\bar{\beta}_\infty}{\bar{\beta}_\ell} \qquad (5)$$

k_η is therefore largely a measure of the local kinetic pressure whilst k depends upon this pressure and the mean downwash. The mean effective downwash $\bar{\varepsilon}$ can readily be determined from

$$\frac{\bar{\varepsilon}}{\alpha} \approx 1 - \frac{k}{k_\eta} \quad . \qquad (6)$$

This is, of course, on the assumption that the control moment is a linear function of the mean local incidence, however, it provides a first approximation to the downwash for the rear control station. The greater non linearity of the control characteristics for the other two locations leads to less reliable results for the downwash at these positions.

The control and stabilising effectiveness parameters k_η and k are given in Fig.19. It will be seen that, for the rear and middle control locations, the value of k_η exceeds unity. At first sight this seems surprising since it will be remembered that k_η is a measure of $q_\ell/q_\infty\ \beta_\infty/\beta_\ell$, in which the first term might be expected to be less than unity for a control immersed in the low energy wake of the wing. This is indeed the case at small angles of incidence; however, an explanation of this high value of k_η at high incidence can be found after considering the downwash given in Fig.20.

This downwash curve has been determined for the rear control location. The full line shown in the figure was determined from k and k_η given in Fig.19 and assuming equation (6).

Alternatively the effective mean downwash may be found by determining the control deflection $\bar{\eta}$ which corresponds to zero load on the tail at a particular incidence $\bar{\alpha}$. In the absence of the direct measurement of panel loads this must be deduced from the overall pitching moments measured on the configurations with and without the control surfaces present. Use can be made of the relationships given in Appendix A if it is assumed that the moments are linearly related to the mean angle of inclination of the flow at the control.

For when

$$0 = \Delta C_{m_c}(\bar{\alpha}) + \Delta C_{m_\eta}(\bar{\eta}) \qquad (7)$$

it follows from equations (A3) and (A5) (Appendix A) that the downwash angle $\bar{\varepsilon}$ at the incidence $\bar{\alpha}$ is given by

$$\frac{\bar{\varepsilon}}{\bar{\alpha}} = 1 + \left(\frac{K_{B(C)} + k_{C(B)}}{K_{B(C)} + K_{C(B)}}\right)\bar{\eta} \qquad (8)$$

The two methods will, in general, lead to slightly different answers mainly since the control moment does not vary linearly with control angles. The points shown were obtained from the condition (7) and equation (8). The two methods are seen to give substantially the same results for this case when the incidence is small for the rear locations of the control.

Some theoretical results are shown for comparison in Fig.20 which are based on linearised theory and simple two dimensional shock expansion theory. The linear theory values quoted, based on the mean value of $\bar{\varepsilon}$ over the control span using the methods described in Section 4 of Appendix A, are given for a station just downstream of the trailing edge and for a station far downstream in the Trefftz plane. The latter calculation ignores the presence of the body. At the trailing edge the linearised theory gives a value for the $d\bar{\varepsilon}/d\bar{\alpha}$ of -0.40 if the body is ignored, or -0.57 if the body is included as described in Appendix A. The $d\bar{\varepsilon}/d\bar{\alpha}$ in the Trefftz plane is +0.815. This dependence of the downwash on the distance from the trailing edge is also illustrated by Fig.21 which has taken from the calculations made by Lomax and Sluder in Ref.8. Although their calculations were for a value of $\beta \tan\gamma$ of 0.60 compared with a value of 0.52 for the present investigation, the behaviour is

not likely to be significantly different. Fig.21 suggests that the value of $d\bar{\varepsilon}/d\alpha$ must increase rapidly over a distance of 0.4 of a wing chord downstream of the wing trailing edge. On the basis of this theoretical result it would appear that some advantage might be gained in stabilising effectiveness by placing the tail surfaces close to the trailing edge of the wing. However, as we can see from the experimental results, any potential advantage which might be gained at small incidence is overshadowed by the losses in kinetic pressure in the wake of the wing, and in absolute terms by the shorter tail arm involved. The upwash at small incidence predicted by the linear theory close to the trailing edge is apparent in the experimental results shown in Fig.20. An upwash is also given by a simple two dimensional shock expansion calculation. Though the use of a two dimensional approach is difficult to defend in the present example, it can serve to provide a possible explanation of the rapid increase in downwash inferred from the measurements at incidence above 10 degrees.

Fig.22 shows a sketch of an idealised two dimensional flow at the wing trailing edge. On the basis of this figure the controls may be expected, as the incidence increases, to enter the field of the expansion from the trailing edge of the wing. Not only is there a tendency for the downwash at the control to increase with increase in incidence, but also the local kinetic pressure increases and the value of $\bar{\beta}_\ell$ decreases, since the local Mach number is reduced to some value between that assumed on the lower surface of the wing and that at the completion of the expansion. At 20°, for example, the Mach number is between 2.6 and 3.93. It is interesting to compare the local values of q_ℓ and $\bar{\beta}_\ell$ for the incidences of 10 and 20 degrees, based on the crude flow model of Fig.22.

The results are given in the table below which also includes corresponding values assuming that the compression on the undersurface of the wing is isentropic.

α deg	M_ℓ	$\bar{\beta}_\ell$	$\frac{H_\ell}{H_\infty}$	$\frac{q_\ell}{q_\infty}$	$\frac{\bar{\beta}_\infty}{\bar{\beta}_\ell}$	$\frac{q_\ell}{q_\infty}\frac{\bar{\beta}_\infty}{\bar{\beta}_\ell}$	Assumptions
10	4.15	4.03	0.90	0.96	1.04	1.00	Shock expansion theory
20	3.45	3.30	0.60	1.22	1.27	1.55	
10	4.32	4.20	1.00	0.98	0.99	0.98	Isentropic compression
20	3.91	3.78	1.00	1.38	1.10	1.52	

Remarkably, although perhaps fortuitously, the ratio of the values of $\frac{q_\ell}{q_\infty}\frac{\bar{\beta}_\infty}{\beta_\ell}$ at 10 and 20 degree is 1.5 regardless of the assumption made regarding the compression on the wing undersurface; and this ratio corresponds well with the ratios of the control effectiveness as given in Fig.19 at the corresponding incidences for the middle and rear control locations (i.e. $k_\eta(20)/k_\eta(10)$ is 1.8 approximately for both positions). The mean downwash one might infer from Fig.22 is also not unreasonable for the rear position although again this may well be fortuitous. Nevertheless this crude flow model does seem to suggest a possible explanation of the behaviour of the control and stabiliser effectiveness. The increase in the control effectiveness with incidence shown in Fig.19(a) offsets the reduction of the downwash factor in the stabiliser effectiveness and the stabiliser effectiveness consequently remains fairly constant as shown in Fig.19(b).

The low value of the control effectiveness when the control is in the forward position cannot be explained on the basis of Fig.22, although clearly, from the non uniformity of the flow field in which it is operating it is difficult to make any predictions about its performance. It is most likely that the low control effectiveness arises simply from the fact that it is immersed in the low energy air of the viscous wake from the wing for most of the incidence range. The high value of its stabilising effectiveness may be simply a result of the decrease in downwash near the trailing edge as suggested by Fig.21 tending to offset the low value of kinetic pressure.

5 DISCUSSION OF THE RESULTS FOR THE TWO THREE AND FOUR PANEL MODELS WITH COMBINED INCIDENCE AND ROLL ANGLE

5.1 Wing and cone configurations (W_2, W_3 and W_4)

Fig.23 gives the measured values of the normal force component, C_z', which is the component in the plane of the body axis and wind vector. It will be seen that the initial slopes of the curves, as calculated by the theory given in Appendix A, are somewhat lower than the measured values. A large portion of the lift developed is non linear with body incidence.

The non linear lift on the four panel configuration is reduced slightly when the model is rolled to 45 degrees. Roll angle has a far greater effect on the three wing configuration. At a roll angle of zero, that is with two of the panels on the windward side of the body, the non linear component of the normal force exceeds that developed by the two or four panel combinations; whereas at a roll angle of 60°, that is with one panel directly to windward, only some 25% of this non linear lift is developed. Fig.24(a) illustrates.

the point further for a total incidence of 30° and Fig.24(b) also shows the variation of the force coefficient, C'_y, normal, to the plane of the body incidence. It can be seen that the three panel combination develops almost as much side force as the two panel combination or about six times that of the four panel combination.

It is interesting to examine whether, in the absence of panel load measurements, it is possible to synthesise the forces in terms of a normal force on a single wing panel together with any interference it may produce on the body. The force on such a panel is assumed to be dependent solely on the body incidence σ and roll orientation, λ_p, of the panel, so that, if the mutual interference between adjacent panels is ignored, the force on any multi-panel combination can be determined by a resolution and summation of the individual panel contributions. At a given incidence σ the dependence of the panel normal force ΔC_{N_p} upon λ_p can be crudely represented by 4 terms of a sine series such that

$$\Delta C_{N_p}(\sigma) = a_1(\sigma) \sin \lambda_p + a_2(\sigma) \sin 2\lambda_p + a_3(\sigma) \sin 3\lambda_p + a_4(\sigma) \sin 4\lambda_p \quad \ldots\ (9)$$

The normal force C'_z and the side force C'_y follow from

$$-C'_z = -C'_z \text{ (body alone)}^* + \sum_{\text{all } \lambda_p} \sum_{r=1}^{4} a_r \sin r(\lambda + \lambda_p) \sin (\lambda + \lambda_p) \quad \ldots\ (10)$$

$$-C'_y = \sum_{\text{all } \lambda_p} \sum_{r=1}^{4} a_r \sin r(\lambda + \lambda_p) \cos (\lambda + \lambda_p) \quad (11)$$

where λ_p is measured from the -z axis as a positive rotation with the same convention as for λ. The relations derived for W_2, W_3 and W_4 are given below.

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* Assumed to equal to C_z for W_2 at $\lambda = 90$ degrees.

	$-C_z' + C_z'$ body alone	$-C_y'$
W_2	$2a_1 \cos^2 \lambda - 2a_3 \cos \lambda \cos 3\lambda$	$-2a_1 \sin \lambda \cos \lambda + 2a_3 \sin \lambda \cos 3\lambda$
W_3	$\frac{3}{2} a_1 + \frac{3}{2} (-a_2 + a_4) \cos 3\lambda$	$\frac{3}{2} (a_2 + a_4) \sin 3\lambda$
W_4	$2a_1 - 2a_3 \cos 4\lambda$	$2a_3 \sin 4\lambda$

The conditions used to determine the coefficients a_1, a_2, a_3 and a_4 have been chosen somewhat arbitrarily from

$$C_y' \text{ for } W_2 \text{ at } \lambda = \pi/4$$

$$C_y' \text{ for } W_3 \text{ at } \lambda = \pi/6$$

$$C_z' \text{ for } W_3 \text{ at } \lambda = 0$$

$$C_z' \text{ for } W_3 \text{ at } \lambda = \pi/6 \quad .$$

From the dotted curves shown in Fig.24 it appears that the force characteristics are fitted fairly well by this simple series. The side force component given for W_4 has the wrong sign unfortunately. This discrepancy illustrates the limitations implied by two rather sweeping assumptions made:-

(1) that the mutual interference between the panels is negligible; which is clearly less and less true as the number of panels increases;

(2) the force tangential to the panel, which is the interference force on the body is small, again this effect is likely to become more significant as the number of panels increases.

The coefficients of equation (9) are shown in Fig.25 plotted against the square of the body incidence σ. It can be seen that the first and second harmonics are dominant in equation (9). With the exception of a_1 at small incidences, as would be expected from equation (1) (see also Ref.9), the coefficients are linear functions of σ^2.

The form of the panel load suggested by this analysis is given in Fig.26 and it is interesting to observe that the maximum panel force is developed by a panel with about 30 degrees of anhedral. The suggestion of a

negative panel load is somewhat surprising. This effect has, however, been discussed in Ref. 9 and noted in Ref. 5. In both these references a forebody is present and indeed Ref. 9 attributes the effect to the body vortices. Nevertheless the form of variation of the panel load deduced from the present measurements and given in Fig. 26 resembles the form given in Ref. 9.

Fig. 27(a), (b) and (c) give for the various wing body combinations the rolling moment as a function of incidence for various roll angles. The data for a body incidence of 30° have been replotted in Fig. 28 so that the relative characteristics of the three models can be compared more readily. It can be seen that the maximum rolling moments on W_3 and W_4 are roughly equal and about 60% of that developed on W_2.

Obviously there are N stable and N unstable equilibrium positions in roll, where N is the number of wing panels. In this context a stable roll position is one at which a small displacement increasing the roll angle produces a restoring, or negative, rolling moment. It is interesting to observe that for all three combinations the position of maximum rolling moment is nearer the unstable than the stable equilibrium roll position.

If the form of the rolling moment due to a single panel is taken to be similar to that given for ΔC_{N_p} in equation (9) i.e.

$$-\Delta C_{\ell_p}(\sigma) = b_1(\sigma) \sin \lambda_p + b_2(\sigma) \sin 2\lambda_p + b_3(\sigma) \sin 3\lambda_p + b_4 \sin 4\lambda \quad \ldots\ldots (12)$$

so that

$$-C_\ell = \sum_{\text{all } \lambda_p} \sum_{r=1}^{4} b_r(\sigma) \sin r(\lambda + \lambda_p) \quad . \qquad (13)$$

For W_2, W_3 and W_4 the relations are given below

	$-C_\ell$
W_2	$-2b_2 \sin 2\lambda + 2b_4 \sin 4\lambda$
W_3	$3b_3 \sin 3\lambda$
W_4	$4b_4 \sin 4\lambda$

Clearly more than 4 terms are necessary to represent the form of the rolling moments given in Fig.28. This analysis has not been developed further since it cannot be directly related to the analysis of the panel normal force which contains a component of force acting on the body and not appearing in the rolling moment. Nevertheless it is interesting that from the form of the rolling moment variation with λ from W_2 it can be deduced that b_2 and b_4 are both negative. This implies that, for W_4, C_ℓ is positive for $0 < \lambda < \pi/4$ in agreement with the sign of the measurements and in fact agreement in magnitude is also obtained, the predicted maximum value being about 0.018 for $\sigma = 20$ degrees. The fact that it appears possible to deduce the rolling moment in this way suggests that the mutual interference between the panels might not be the dominant feature.

Although it has been possible to get a slightly better understanding of the panel loads from the simple approach given, there is a considerable amount of conjecture involved, and a proper understanding of the problem requires the direct measurement of the panel loads.

5.2 Wing-body-control models (W_3BC^R, W_4BC^R and W_4BC^F)

Fig.29 gives the variation of C_m' with C_z' for the model W_4BC^R with $\eta = 0$ for roll angles λ of 0, 15, 30 and 45 degrees. At small values of C_z' there appears to be a slight forward movement of aerodynamic centre with increasing roll angle but for force coefficients between about -0.2 and -0.6 there is a significant forward movement of aerodynamic centre particularly between $\lambda = 0$ and 45°. The range of the movement of the aerodynamic centre is about $0.03\ \bar{\bar{c}}$ or 0.2 calibre.

The final aspect of the model which was studied is the aileron power of the controls. Increments in rolling moment, ΔC_ℓ, due to the deflection of a single control surface for the configurations with three and four wing panels are shown in Figs.30 and 31 for the rear control location. Additional results are given in Fig.32 for the forward control location for the four panel combination.

These results have not been analysed in any great detail but it is possible to make a few general remarks on the behaviour of the deflected panel at roll angles of 0, 90, 180 and 270 degrees.

Figs.31 and 32 give ΔC_ℓ for the configurations W_4BC^R and W_4BC^F at $\lambda = 90$ and 270 which can be compared with curves given in Figs.16(c) and 16(a) for the increment ΔC_m in the pitching moment produced when two controls are

deflected as elevators on the two panel configurations W_2BC^R and WBC^F. This is to be expected and therefore the remarks made in Section 4.3 regarding the elevator effectiveness apply equally well to the roll effectiveness. At $\lambda = 0$ Figs.31 and 32 show a considerable reduction in ΔC_ℓ as the body incidence, σ, increases; whereas at $\lambda = 180$ degrees, Fig.31 shows that the reverse is true. This effect may well be associated with changes in the local values of the kinetic pressure q_ℓ and $\bar{\beta}_\ell$ particularly over the outboard regions of the control which are directly influenced by the flow field of the horizontal wing panels. Analysis similar to that applied in Section 4.3 for the pitching moments suggests that $\Delta C_\ell(\sigma)/\Delta C_\ell(\sigma = 0) \approx q_\ell/q_\infty \bar{\beta}_\infty/\bar{\beta}_\ell$. On the basis of the idealised flow model of Fig.22 the table below has been prepared giving values of $q_\ell/q_\infty \bar{\beta}_\infty/\bar{\beta}_\ell$ for a body incidence, σ, of 10° and 20° which are appropriate to the outboard regions of the control.

λ degrees	0		180	
σ degrees	$\frac{q_\ell}{q_\infty}\frac{\bar{\beta}_\infty}{\bar{\beta}_\ell}$ Wing upper surface	$\frac{\Delta C_\ell(\sigma)}{\Delta C_\ell(\sigma = 0)}$ $\xi_{-z} = -20^\circ$ measured for W_4BC^R	$\frac{q_\ell}{q_\infty}\frac{\bar{\beta}_\infty}{\bar{\beta}_\ell}$ Wing lower surface	$\frac{\Delta C_\ell(\sigma)}{\Delta C_\ell(\sigma = 0)}$ $\xi_{-z} = -20^\circ$ measured for W_4BC^R
10	0.37	0.58	2.5	1.7
20	0.11	0.03	4.3	2.8

The table shows that the trend with σ of the value of $q_\ell/q_\infty \bar{\beta}_\infty/\bar{\beta}_\ell$ based on Fig.22 is clearly reflected in the measured values of the rolling moment due to the control for the rear control location. This is obviously an oversimplification of the problem and probably quite unrealistic for the case of $\lambda = 0$ where the wing leading edge vortices are likely to have a profound effect.

For the configuration with forward controls, W_4BC^F, the values of ΔC_ℓ given in Fig.32 for $\lambda = 180$ degrees are generally lower than the corresponding values for W_4BC^R, and it believed that this may be the result of a possible separation provoked on the wing by the close proximity of the control. This possibility was mentioned earlier in Section 4.3 in connection with the elevator effectiveness of model W_2BC^F.

Fig.30 shows that the behaviour of ΔC_ℓ for the three panel configuration BW_3C^R is broadly similar to that of the four panel configuration although no explanation can be offered for the low values at λ = 180 degrees for body incidences above 12 degrees.

Not withstanding the large variations in the contribution of an individual deflected panel it is rather remarkable that the rolling power produced when all the control surfaces are deflected is apparently fairly uniform as illustrated in Figs.33 and 34. Here also are shown for comparison the induced rolling moments produced by the wing which must be trimmed out by the control moment if equilibrium is to be obtained. Although the models tested make no pretence to be practical missile shapes, it is worth noting that controls of the size tested are really too small since a 20 degree control deflection is required to trim out the induced rolling moments at σ = 28 deg, and therefore any simultaneous lateral control would necessitate unreasonably large control deflections.

The further analysis, (perhaps on the basis of Ref. 9,) of the control data given by the present tests might be rewarding, but to understand the behaviour of the individual controls adequately requires a knowledge of the control panel loads as is available in Ref.5 for lower Mach numbers.

6 CONCLUSIONS

1 The normal force developed by the wing body combinations with two three and four wing panels exceeds the values estimated by methods based on linearised theory; and the non linear component of the normal force is found to be proportional to the square of the incidence.

2 Relatively large lateral forces, of the order of 50% of the normal force, are developed by the two and three wing combinations which are about six times those developed on the cruciform combination. The maximum induced rolling moments for the three and four wing combinations are of the same order but are 60% of the maximum value for the two wing combination.

3 It is found possible to synthesise approximately the normal force and side force on the various combinations by deriving the characteristics of a single panel with roll angle and body incidence.

4 The stabiliser and control effectiveness of the in-line rear controls tested show considerable variations over the range of control angle and body incidence of the tests. Analysis shows that these variations can be variously attributed to the losses in the viscous wake from the wing and to the fact

that the control operates at times within the field of the Prandtl-Meyer expansion from the wing trailing edge.

5 In general there is a forward movement of aerodynamic centre for negative control angles and a rearward movement for positive angles.

6 The control when located close behind the wing trailing edge has only about 40% of the effectiveness of that of a control located one or two control chords from the trailing edge.

7 The large variations with body incidence and roll angle of the rolling moment produced by the deflection of a single control panel are attributed to variations in the local kinetic pressure and Mach number produced by the wing flow field. Despite these large variations of the rolling moment produced by the deflection of an individual control, when all the control surfaces are deflected as ailerons it is found, for both the three and four wing panel combinations, that the resulting rolling moment varies very little with roll angle.

Rear controls in line with wings of the type tested introduce non linearities into the aerodynamic characteristics of the slender configuration which do much to offset the otherwise well behaved characteristics of the basic slender wing. Alternative forms of control surface should therefore be explored if improvements are to be made. Such alternatives might be trailing edge controls, wing tip controls or even an interdigitated form of the rear control of the type tested.

Appendix A

NOTES ON THE FORMULAE USED FOR ESTIMATING THE AERODYNAMIC CHARACTERISTICS AT SMALL INCIDENCE

A.1 Normal force for the wing and cone combination as given in Ref.1

$$-\frac{dC_z}{d\alpha} = \frac{2\pi\, t_1}{\bar{\beta}} \frac{1}{E_o \Lambda}\left[1 - \frac{8}{3\pi}\left(\frac{t_o}{t_1}\right)^3 + \frac{3}{2}\left(\frac{t_o}{t_1}\right)^4 - \frac{8}{15\pi}\left(\frac{t_o}{t_1}\right)^5 + \ldots\right]$$

.... (A1)

where $t_1 = \bar{\beta} \tan \gamma$

$t_o = \bar{\beta} \tan \theta_o$

γ is semi apex angle of the wing

θ_o is semi apex angle of the cone

$$\Lambda = 1 - \frac{3}{2}\left(\frac{t_o}{t_1}\right)^4 \frac{t_1}{E_o} I_2 - \frac{5}{16}\left(\frac{t_o}{t_1}\right)^8 \left(\frac{t_1}{E_o}\right) I_4 - \frac{21}{256}\left(\frac{t_o}{t_1}\right)^{12} \frac{t_1}{E_o} I_6$$

$$I_2 = -\frac{t_1}{3} K_o\left(\sqrt{1 - t_1^2}\right) - \frac{1 - 2\,t_1^2}{3t_1} E_o\left(\sqrt{1 - t_1^2}\right)$$

$$I_4 = \left(\frac{16t_1^4 - 16t_1^2 + 1}{15t_1}\right) E_o\left(\sqrt{1 - t_1^2}\right) + \left(\frac{7 - 8\,t_1^2}{15}\right) t_1 K_o\left(\sqrt{1 - t_1^2}\right)$$

$$I_6 = \left(\frac{-256t_1^6 + 384t_1^4 - 134t_1^2 + 3}{105t_1}\right) E_o\left(\sqrt{1 - t_1^2}\right)$$

$$+ \left(\frac{128t_1^4 - 176t_1^2 + 51}{105}\right) t_1 K_o\left(\sqrt{1 - t_1^2}\right)$$

and where K_o and E_o are complete elliptic integrals of the first and second kind respectively both with a modulus of $\sqrt{1 - t_1^2}$.

A.2 Increments of load and moment due to the addition of the controls as derived from Ref.4

$$\Delta C_{z_c} = -(K_{B(C)} + K_{C(B)}) \frac{q_\ell}{q_\infty} \frac{S_C}{S_W} \frac{4\alpha}{\beta_\ell} \left(1 - \frac{1}{2 A_N \beta_\ell}\right) \left(1 - \frac{\bar{\varepsilon}}{\alpha}\right) \quad (A2)$$

$$\Delta C_{m_c} = -(K_{B(C)} + K_{C(B)}) \frac{q_\ell}{q_\infty} \frac{S_C \ell_c}{S_W \bar{c}} \frac{4\alpha}{\beta_\ell} \left(1 - \frac{1}{2 A_N \beta_\ell}\right) \left(1 - \frac{\bar{\varepsilon}}{\alpha}\right) \quad (A3)$$

A_N = net aspect ratio of controls

$K_{B(C)}$ and $K_{C(B)}$ interference factors as given in Ref.4

S_C = net area of the control

$\frac{q_\ell}{q_\infty}(\alpha)$ = ratio of the mean local kinetic pressure at the control to that of the free stream

$\bar{\beta}_\ell$ = local value of $\sqrt{M^2 - 1}$

$\bar{\varepsilon}$ = mean downwash at the controls

ℓ_c = tail arm (taken as distance from the reference point to the centre of pressure of the control).

A.3 Increments of load and moment due to deflecting the controls

$$\Delta C_{z_\eta} = -(k_{B(C)} + k_{C(B)}) \frac{q_\ell}{q_\infty} \frac{S_C}{S_W} \frac{4\eta}{\bar{\beta}_\ell} \left(1 - \frac{1}{2 A_N \bar{\beta}_\ell}\right) \quad (A4)$$

$$\Delta C_{m_\eta} = -(k_{B(C)} + k_{C(B)}) \frac{q_\ell}{q_\infty} \frac{S_C \ell_n}{S_W \bar{c}} \frac{4\eta}{\bar{\beta}_\ell} \left(1 - \frac{1}{2 A_N \bar{\beta}_\ell}\right) \quad (A5)$$

$k_{B(C)}$ and $k_{C(B)}$ interference factors as given in Ref.4.

A.4 Downwash calculation just downstream of the trailing edge of the wing and in the Trefftz plane.

The downwash angle, ε, immediately downstream of the wing trailing edge can readily be calculated from the knowledge of the pressure distribution just upstream of the edge by application of the "lift cancellation" technique. It follows that

$$\frac{4\alpha\left(1-\frac{\varepsilon}{\alpha}\right)}{\bar{\beta}} = \Delta p_{TE} = \frac{p\ (\text{lower surface}) - p\ (\text{upper surface})}{\frac{1}{2}\rho V^2} .$$

For a delta wing with subsonic leading edges

$$\Delta C_{p_{TE}} = \frac{4t_1}{\bar{\beta} E_o} \frac{1}{\sqrt{1-\left(\frac{t}{t_1}\right)^2}}$$

where $t = \frac{y\bar{\beta}}{C_R}$ and C_R is the root chord.

For a conical wing and body $\Delta C_{p_{TE}}$ is found from Ref. 1 to be

$$\Delta C_{p_{TE}} = \frac{4t_1}{\bar{\beta} E_o \Lambda} \frac{1}{\sqrt{1-\left(\frac{t}{t_1}\right)^2}} \left[1 - \frac{3}{2}\left(\frac{t_o}{t_1}\right)^4 \left(\frac{t_1^2}{t^2} - 1\right) - \frac{5}{16}\left(\frac{t_o}{t_1}\right)^8 \left(2\frac{t_1^4}{t^4} - 3\frac{t_1^2}{t} + 1\right) - \frac{21}{768}\left(\frac{t_o}{t_1}\right)^{12} \left(16\frac{t_1^6}{t^6} - 32\frac{t_1^4}{t^4} + 19\frac{t_1^2}{t^2} - 3\right)\right] .$$

The mean value of the downwash over the control can be found from

$$\bar{\varepsilon} = \frac{1}{s-a}\int_a^s \varepsilon\, dy ,$$

where a is the body radius and s the semi span of the wing.

For the plane delta wing with subsonic edges this gives

$$\frac{\bar{\varepsilon}}{\alpha} = 1 - \frac{\bar{\beta}\tan\gamma}{E_o} \frac{\left[\frac{\pi}{2} - \sin^{-1}\left(\frac{a}{s}\right)\right]}{1-\frac{a}{s}} .$$

The downwash in the Trefftz plane can be calculated from the knowledge of the spanwise loading L(y) since

$$L(y) = \rho U \Gamma \quad ,$$

where Γ is the circulation, and ε can be calculated from,

$$\varepsilon = -\frac{1}{2\pi U} \int_{-s}^{+s} \frac{\left(\frac{d\Gamma}{dy}\right)_{y=y_o} dy_o}{y - y_o} \quad .$$

For a delta wing with subsonic leading edges,

$$\Gamma = \frac{2\alpha U s}{E_o} \sqrt{1 - \frac{y^2}{s^2}} \quad ,$$

whence, since the loading is elliptic, we find that ε is a constant across the span, so that

$$\frac{\bar{\varepsilon}}{\alpha} = \frac{1}{E_o} \quad . \tag{A6}$$

A.5 Calculation of the lift of multi-panelled slender wing body combinations.

Applying the method given by A. H. Sacks[6], Dr. A. J. Ross of R.A.E. showed that the normal force developed by a slender thin wing and body combination with N equally spaced panels is given by

$$-\frac{\partial C_z}{\partial \alpha} = \frac{2}{S_r} \left[2\pi r_o^2 - S\right]_{x = C_R} \tag{A7}$$

where

$$r_o^2 = \frac{1}{2}\, 4/N \left[s^{N/2} + \left(\frac{a^2}{s}\right)^{N/2}\right]^{4/N}$$

a is the body radius, S the cross sectional area and S_r is the reference area used in C_z i.e. S_W and provided $N > 3$. The formula holds for all roll attitudes.

This reduces to

$$-\frac{\partial C_z}{\partial \alpha} = \frac{\pi A}{2} \left\{2^{1 - 4/N} \left[1 + \left(\frac{a}{s}\right)^N\right]^{4/N} - \frac{a^2}{s^2}\right\} \tag{A8}$$

when C_z is based on twice the panel area and where A is twice the aspect ratio of a single panel.

For N = 3 we have

$$-\frac{\partial C_z}{\partial \alpha} = \frac{\pi A}{2}\left\{\frac{1}{2^{\frac{1}{3}}}\left[1+\left(\frac{a}{s}\right)^3\right]^{4/3} - \frac{a^2}{s^2}\right\} \qquad (A9)$$

and for N = 4

$$-\frac{\partial C_z}{\partial \alpha} = \frac{\pi A}{2}\left\{1 - \frac{a^2}{s^2} + \frac{s^4}{s^4}\right\} \quad . \qquad (A10)$$

This latter result agrees with that given by Spreiter[7].

It can also be shown by the same method that for N > 3 the rolling moments are zero for all roll attitudes.

In order to generalise the above result, for a delta wing with subsonic leading edges it is suggested that a factor $1/E_o$ should be applied to the right hand sides of equations (A9) and (A10).

Appendix B

Tabulated test results

Tables	1	- 48	W_2
	49	- 100	W_3
	101	- 197	W_4

Note - For wing W_3 the orientation of the model is such that at $\lambda = 30^{\circ}$ one wing is in the -z plane.

In the tables the figures appearing in each column must be multiplied by 10^{-N} for Tables 1 to 29 inclusive and by 10^{+N} for Tables 30 to 197 inclusive where the exponent N appears at the head of each column.

Table 1

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0006
	1354	-0040	+0000	-0406	+0001	+0157	+0511		-0076	+3057
	1355	-0030	+0000	-0302	+0001	+0107	+0391		-0035	+2945
	1356	-0020	+0000	-0204	+0001	+0049	+0255		-0010	+2680
	1357	-0010	+0000	-0101	+0000	-0002	+0119		+0029	+2048
	1358	+0000	+0000	+0001	-0000	-0050	+0017		+0015	+2191
	1359	+0011	+0000	+0107	-0000	-0090	-0102		+0041	+2959
	1360	+0020	+0000	+0203	-0001	-0161	-0222		+0054	+1890
	1361	+0030	+0000	+0304	-0001	-0205	-0356		+0086	+2051
	1362	+0040	+0000	+0405	-0001	-0260	-0475		+0127	+1769
	1363	+0050	+0000	+0510	-0002	-0328	-0628		+0178	+1322
	1364	+0060	+0000	+0609	-0002	-0387	-0764		+0231	+1043
M_2	1365	+0081	+0000	+0818	-0003	-0536	-1088		+0345	+1065
	1366	+0100	+0000	+1017	-0004	-0656	-1430		+0463	+0305
	1367	+0120	+0000	+1224	-0004	-0771	-1768		+0596	+0040
	1368	+0140	+0000	+1429	-0005	-0916	-2142		+0731	-0358
	1369	+0160	+0000	+1630	-0006	-1053	-2499		+0896	+0296
	1380	+0180	+0000	+1835	-0008	-1352	-2926		+1053	-0493
	1381	+0200	+0000	+2043	-0009	-1523	-3385		+1205	-2034
	1382	+0220	+0000	+2243	-0010	-1721	-3862		+1396	-0358
	1383	+0240	+0000	+2448	-0011	-1844	-4254		+1630	-2506
	1384	+0260	+0000	+2654	-0013	-2153	-4883		+1800	-3780
	1385	+0280	+0000	+2862	-0014	-2379	-5445		+2023	-4504
	1386	+0286	+0000	+2923	-0014	-2456	-5619		+2071	-4813

Table 2

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0005	0005	0005
W_2B	0996	-0040	+0000	-0405	+0001	+0191	+0569		+0173	+0183
	0997	-0030	+0000	-0301	+0001	+0144	+0411		+0136	+0150
	0998	-0020	+0000	-0203	+0001	+0110	+0281		+0119	+0137
	0999	-0010	+0000	-0101	+0001	+0068	+0149		+0063	+0166
	1000	+0000	+0000	+0002	+0000	+0032	+0019		+0000	+0116
	1001	+0010	+0000	+0105	+0000	-0016	-0114		-0041	+0126
	1002	+0020	+0000	+0204	-0000	-0040	-0234		-0072	+0104
	1003	+0030	+0000	+0307	-0000	-0094	-0376		-0129	+0069
	1004	+0041	+0000	+0412	-0001	-0135	-0525		-0164	+0116
	1005	+0050	+0000	+0511	-0001	-0198	-0677		-0192	+0122
	1006	+0060	+0000	+0614	-0001	-0270	-0835		-0229	+0108
	1007	+0080	+0000	+0816	-0002	-0399	-1185		-0351	+0085
	1008	+0101	+0000	+1024	-0003	-0493	-1568		-0532	+0101
	1009	+0120	+0000	+1222	-0003	-0598	-1950		-0721	+0118
	1010	+0140	+0000	+1427	-0003	-0667	-2356		-0929	+0104
	1011	+0160	+0000	+1630	-0004	-0766	-2798		-1126	+0151
	1012	+0180	+0000	+1837	-0005	-1048	-3282		-1350	+0185
	1013	+0200	+0000	+2042	-0006	-1128	-3780		-1614	+0040
	1014	+0220	+0000	+2248	-0007	-1320	-4325		-1859	+0484
	1015	+0240	+0000	+2455	-0007	-1300	-4900		-2118	-0124
	1016	+0260	+0000	+2662	-0008	-1569	-5500		-2437	-0057
	1017	+0280	+0000	+2867	-0009	-1740	-6138		-2693	+0162
	1018	+0287	+0000	+2943	-0010	-1851	-6367		-2816	+0300

Table 3

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0005	0005	0006
$W_2\,B\,C^F$	1022	-0040	+0000	-0408	+0001	+0223	+0637		+0557	-0594
	1023	-0030	+0000	-0306	+0001	+0176	+0475		+0460	-1209
	1024	-0020	+0000	-0205	+0001	+0121	+0327		+0320	-0559
	1025	-0010	+0000	-0101	+0000	+0062	+0167		+0185	-0605
	1026	+0000	+0000	-0000	+0000	+0017	+0036		+0078	-0449
	1027	+0010	+0000	+0100	-0000	-0028	-0090		-0014	-0615
	1028	+0020	+0000	+0203	-0000	-0059	-0232		-0102	-0564
	1029	+0030	+0000	+0303	-0001	-0114	-0397		-0252	-0430
	1030	+0040	+0000	+0403	-0001	-0182	-0559		-0379	-0435
	1031	+0050	+0000	+0510	-0001	-0257	-0742		-0501	+0114
	1032	+0060	+0000	+0610	-0002	-0326	-0905		-0613	-0228
	1033	+0080	+0000	+0815	-0003	-0474	-1286		-0898	+0133
	1034	+0100	+0000	+1025	-0003	-0594	-1701		-1210	-0273
	1035	+0120	+0000	+1228	-0004	-0710	-2138		-1556	+0247
	1036	+0140	+0000	+1430	-0004	-0798	-2573		-1909	+0706
	1037	+0160	+0000	+1635	-0005	-0911	-3025		-2280	+2093
	1038	+0180	+0000	+1842	-0006	-1222	-3573		-2680	+2884
	1039	+0200	+0000	+2046	-0007	-1330	-4101		-3127	+1482
	1040	+0220	+0000	+2254	-0008	-1605	-4702		-3649	+7436
	1041	+0240	+0000	+2461	-0008	-1564	-5334		-4117	+1311
	1042	+0260	+0000	+2669	-0010	-1881	-5987		-4681	+2069
	1043	+0280	+0000	+2881	-0011	-2088	-6680		-5237	+4788
$\eta = 0^\circ$	1044	+0286	+0000	+2941	-0011	-2198	-6885		-5390	+5614

Table 4

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0003	0005	0005
$W_2\ B\ C^F$ $\eta = +5^\circ$	1048	-0040	+0000	-0409	+0002	+0299	+0650		+0671	+0154
	1049	-0030	+0000	-0302	+0001	+0238	+0491		+0545	+0170
	1050	-0020	+0000	-0202	+0001	+0177	+0333		+0407	+0126
	1051	-0010	+0000	-0101	+0001	+0128	+0193		+0285	+0168
	1052	-0000	+0000	-0002	+0001	+0076	+0053		+0178	+0200
	1053	+0010	+0000	+0101	+0000	+0033	-0071		+0082	+0214
	1054	+0021	+0000	+0209	+0000	-0029	-0245		-0029	+0208
	1055	+0030	+0000	+0306	-0000	-0059	-0384		-0179	+0248
	1056	+0040	+0000	+0410	-0001	-0180	-0558		-0288	+0115
	1057	+0050	+0000	+0509	-0001	-0222	-0731		-0398	+0170
	1058	+0060	+0000	+0611	-0001	-0286	-0904		-0523	+0187
	1059	+0080	+0000	+0820	-0002	-0422	-1288		-0799	+0284
	1060	+0100	+0000	+1019	-0003	-0526	-1670		-1075	+0270
	1061	+0121	+0000	+1233	-0003	-0644	-2105		-1416	+0315
	1062	+0140	+0000	+1433	-0004	-0765	-2523		-1726	+0332
	1063	+0160	+0000	+1636	-0004	-0856	-3010		-2089	+0405
	1064	+0180	+0000	+1842	-0006	-1187	-3519		-2477	+0580
	1065	+0200	+0000	+2048	-0007	-1268	-4060		-2895	+0392
	1066	+0220	+0000	+2256	-0008	-1560	-4646		-3324	+0937
	1067	+0240	+0000	+2467	-0008	-1534	-5274		-3798	+0496
	1068	+0260	+0000	+2673	-0010	-1832	-5922		-4352	+0439
	1069	+0278	+0000	+2857	-0011	-2000	-6516		-4763	+0558

Table 5

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0006
	1073	-0040	+0000	-0407	+0002	+0328	+0701		+0712	+0131
	1074	-0029	+0000	-0301	+0001	+0257	+0522		+0583	+0144
	1075	-0020	+0000	-0200	+0001	+0193	+0361		+0443	+0231
	1076	-0010	+0000	-0099	+0001	+0134	+0218		+0319	+0069
	1077	+0000	+0000	+0002	+0000	+0083	+0072		+0202	+0171
	1078	+0010	+0000	+0101	+0000	+0039	-0053		+0126	-0008
	1079	+0020	+0000	+0204	-0000	-0005	-0176		+0056	+0144
	1080	+0030	+0000	+0308	-0000	-0056	-0319		-0053	+0241
	1081	+0040	+0000	+0407	-0001	-0142	-0499		-0182	+0698
	1082	+0050	+0000	+0509	-0001	-0208	-0660		-0294	+0772
W_2 B C^F	1083	+0060	+0000	+0611	-0002	-0291	-0840		-0408	+0731
	1084	+0080	+0000	+0817	-0002	-0477	-1217		-0667	+1062
$\eta = +10^\circ$	1085	+0100	+0000	+1022	-0003	-0584	-1614		-0908	+1267
	1086	+0120	+0000	+1224	-0004	-0724	-2011		-1194	+1993
	1087	+0140	+0000	+1429	-0004	-0856	-2451		-1481	+2616
	1088	+0160	+0000	+1635	-0005	-0975	-2925		-1801	+3645
	1089	+0181	+0000	+1847	-0007	-1318	-3434		-2133	+3945
	1090	+0200	+0000	+2048	-0008	-1450	-3965		-2506	+2711
	1091	+0220	+0000	+2255	-0009	-1716	-4539		-2915	+8578
	1092	+0240	+0000	+2461	-0009	-1702	-5128		-3311	+2406
	1093	+0260	+0000	+2670	-0011	-2049	-5784		-3792	+3091
	1094	+0278	+0000	+2859	-0012	-2253	-6377		-4160	+5760

Table 6

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0006
W_2 B C^F	1097	-0049	+0000	-0504	+0002	+0346	+0844		+0920	-1242
	1098	-0040	+0000	-0409	+0001	+0242	+0685		+0782	-2767
$\eta = +15^\circ$	1099	-0030	+0000	-0307	+0001	+0207	+0512		+0677	-2910
	1100	-0020	+0000	-0205	+0001	+0162	+0369		+0563	-2329
	1101	-0010	+0000	-0103	+0000	+0098	+0211		+0454	-2573
	1102	+0000	+0000	-0001	+0000	+0054	+0088		+0408	-2772
	1103	+0010	+0000	+0099	-0000	+0014	-0015		+0357	-2640
	1104	+0020	+0000	+0204	-0000	-0036	-0155		+0295	-2899
	1105	+0030	+0000	+0304	-0001	-0064	-0295		+0187	-2756
	1106	+0040	+0000	+0405	-0001	-0126	-0471		+0090	-2199
	1107	+0050	+0000	+0506	-0001	-0188	-0646		-0051	-1919
	1108	+0060	+0000	+0609	-0002	-0255	-0804		-0175	-1924
	1109	+0080	+0000	+0813	-0002	-0407	-1191		-0433	-1106
	1110	+0101	+0000	+1029	-0003	-0547	-1594		-0648	-1300
	1111	+0120	+0000	+1222	-0004	-0671	-1965		-0881	-0684
	1112	+0140	+0000	+1428	-0005	-0803	-2388		-1121	-0765
	1113	+0160	+0000	+1632	-0005	-0904	-2829		-1380	-0416
	1114	+0180	+0000	+1838	-0007	-1190	-3341		-1661	+0139
	1115	+0200	+0000	+2044	-0007	-1322	-3870		-1988	-1740
	1116	+0220	+0000	+2252	-0009	-1622	-4434		-2339	+4082
	1117	+0240	+0000	+2464	-0009	-1584	-5047		-2682	-1011
	1118	+0260	+0000	+2665	-0011	-1921	-5644		-3086	-0561
	1119	+0278	+0000	+2854	-0011	-2053	-6247		-3439	-0003

Table 7

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0006
W_2 B C^F	1122	-0050	+0000	-0506	+0002	+0375	+0846		+1001	-0591
	1123	-0040	+0000	-0408	+0001	+0303	+0683		+0895	-1683
	1124	-0030	+0000	-0305	+0001	+0237	+0533		+0792	-2387
	1125	-0020	+0000	-0205	+0001	+0170	+0386		+0726	-2132
	1126	-0010	+0000	-0103	+0000	+0097	+0258		+0648	-2208
	1127	+0000	+0000	-0002	+0000	+0053	+0148		+0649	-2450
	1128	+0010	+0000	+0100	-0000	+0004	+0019		+0601	-2420
	1129	+0020	+0000	+0201	-0000	-0039	-0109		+0538	-2182
	1130	+0030	+0000	+0302	-0001	-0113	-0272		+0446	-1722
	1131	+0040	+0000	+0404	-0001	-0165	-0422		+0311	-1618
	1132	+0050	+0000	+0505	-0001	-0249	-0605		+0179	-1297
	1133	+0060	+0000	+0608	-0002	-0321	-0771		+0065	-1407
$\eta = +20^\circ$	1134	+0080	+0000	+0815	-0003	-0538	-1141		-0145	-0694
	1135	+0100	+0000	+1020	-0004	-0687	-1511		-0324	-1086
	1136	+0120	+0000	+1222	-0005	-0846	-1918		-0508	-0888
	1137	+0140	+0000	+1427	-0005	-0985	-2306		-0722	-0454
	1138	+0160	+0000	+1630	-0006	-1125	-2751		-0935	+0010
	1139	+0180	+0000	+1836	-0007	-1421	-3252		-1155	+0690
	1140	+0200	+0000	+2043	-0009	-1577	-3769		-1414	-2083
	1141	+0220	+0000	+2252	-0010	-1918	-4328		-1730	+4186
	1142	+0240	+0000	+2453	-0010	-1907	-4898		-2042	-0971
	1143	+0260	+0000	+2662	-0012	-2257	-5528		-2389	-0066
	1144	+0278	+0000	+2847	-0013	-2470	-6084		-2694	+0813

Table 8

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0006
W_2 B C^F	1148	-0040	+0000	-0407	+0001	+0263	+0568		+0309	-2443
$\eta = -5^\circ$	1149	-0030	+0000	-0307	+0001	+0199	+0409		+0205	-2374
	1150	-0020	+0000	-0204	+0001	+0161	+0265		+0089	-2494
	1151	-0010	+0000	-0102	+0000	+0090	+0125		+0019	-2464
	1152	-0000	+0000	-0001	+0000	+0049	+0000		-0059	-2229
	1153	+0011	+0000	+0106	-0000	+0004	-0124		-0105	-2112
	1154	+0020	+0000	+0205	-0000	-0024	-0264		-0207	-2277
	1155	+0030	+0000	+0304	-0001	-0083	-0424		-0317	-2344
	1156	+0040	+0000	+0408	-0001	-0144	-0585		-0458	-1848
	1157	+0051	+0000	+0514	-0001	-0218	-0763		-0586	-1925
	1158	+0060	+0000	+0613	-0002	-0292	-0941		-0714	-1693
	1159	+0080	+0000	+0817	-0003	-0437	-1215		-1003	-1317
	1160	+0100	+0000	+1022	-0003	-0574	-1724		-1310	-1357
	1161	+0120	+0000	+1226	-0004	-0668	-2141		-1648	-0680
	1162	+0140	+0000	+1432	-0004	-0774	-2572		-2021	-0185
	1163	+0160	+0000	+1637	-0005	-0895	-3064		-2402	+0949
	1164	+0180	+0000	+1844	-0006	-1195	-3576		-2833	+1678
	1165	+0200	+0000	+2049	-0007	-1333	-4144		-3315	+0557
	1166	+0220	+0000	+2256	-0008	-1619	-4725		-3789	+6625
	1167	+0240	+0000	+2464	-0009	-1630	-5340		-4301	+3361
	1168	+0260	+0000	+2671	-0010	-1915	-6003		-4868	+1893
	1169	+0278	+0000	+2862	-0011	-2103	-6612		-5360	+2892

Table 9

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0005	0005	0005
W_2 B C^F	1173	-0040	+0000	-0404	+0002	+0291	+0546		+0093	+0139
	1174	-0030	+0000	-0305	+0001	+0237	+0402		-0003	+0159
$\eta = -10^\circ$	1175	-0020	+0000	-0204	+0001	+0183	+0257		-0113	+0139
	1176	-0010	+0000	-0101	+0001	+0132	+0112		-0193	+0179
	1177	+0000	+0000	+0001	+0000	+0048	-0018		-0263	+0233
	1178	+0010	+0000	+0102	+0000	+0015	-0124		-0271	+0237
	1179	+0020	+0000	+0207	+0000	-0034	-0269		-0336	+0252
	1180	+0030	+0000	+0306	-0000	-0088	-0417		-0439	+0218
	1181	+0040	+0000	+0406	-0001	-0157	-0578		-0530	+0216
	1182	+0050	+0000	+0509	-0001	-0241	-0724		-0640	+0217
	1183	+0060	+0000	+0610	-0002	-0325	-0924		-0788	+0161
	1184	+0081	+0000	+0826	-0003	-0524	-1325		-1085	+0278
	1185	+0100	+0000	+1021	-0003	-0675	-1708		-1381	+0242
	1186	+0120	+0000	+1225	-0004	-0828	-2129		-1733	+0294
	1187	+0140	+0000	+1428	-0005	-0932	-2549		-2102	+0441
	1188	+0160	+0000	+1634	-0005	-1103	-3025		-2488	+0505
	1189	+0180	+0000	+1845	-0007	-1480	-3575		-2935	+0638
	1190	+0200	+0000	+2048	-0008	-1596	-4127		-3413	+0460
	1191	+0220	+0000	+2256	-0009	-1909	-4713		-3929	+0927
	1192	+0240	+0000	+2463	-0010	-1996	-5334		-4445	+0633
	1193	+0261	+0000	+2675	-0012	-2318	-5994		-5014	+0601
	1194	+0281	+0000	+2884	-0013	-2540	-6678		-5644	+0697
	1195	+0287	+0000	+2948	-0013	-2619	-6881		-5831	+0726

Table 10

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0005	0005	0006
W_2 B C^F	1198	-0050	+0000	-0503	+0002	+0288	+0660		-0062	-0111
	1199	-0040	+0000	-0405	+0001	+0218	+0517		-0140	-0659
	1200	-0030	+0000	-0300	+0001	+0165	+0339		-0254	-1020
	1201	-0020	+0000	-0203	+0001	+0118	+0214		-0346	-0954
	1202	-0010	+0000	-0100	+0000	+0067	+0068		-0432	-0892
	1203	+0000	+0000	+0004	+0000	+0022	-0072		-0489	-0323
	1204	+0010	+0000	+0101	-0000	-0008	-0161		-0500	-0624
	1205	+0020	+0000	+0204	-0000	-0073	-0304		-0521	-0860
	1206	+0030	+0000	+0303	-0001	-0123	-0429		-0567	-0431
	1207	+0040	+0000	+0411	-0001	-0186	-0590		-0618	-0319
	1208	+0051	+0000	+0515	-0001	-0260	-0750		-0714	-0838
	1209	+0060	+0000	+0610	-0002	-0339	-0929		-0827	-1429
$\eta = -15^\circ$	1210	+0080	+0000	+0816	-0003	-0520	-1322		-1163	-0776
	1211	+0100	+0000	+1022	-0004	-0681	-1733		-1457	-0648
	1212	+0120	+0000	+1225	-0005	-0818	-2144		-1781	-1009
	1213	+0140	+0000	+1430	-0005	-0955	-2572		-2152	-0900
	1214	+0160	+0000	+1635	-0006	-1099	-3039		-2566	+0529
	1215	+0180	+0000	+1842	-0008	-1461	-3596		-3052	+2218
	1216	+0200	+0000	+2049	-0009	-1599	-4152		-3581	+1019
	1217	+0220	+0000	+2255	-0010	-1872	-4724		-4079	+4476
	1218	+0240	+0000	+2467	-0011	-1980	-5350		-4646	+1600
	1219	+0260	+0000	+2676	-0013	-2392	-6017		-5322	+5320
	1220	+0280	+0000	+2881	-0014	-2625	-6663		-5924	+4600
	1221	+0286	+0000	+2941	-0014	-2601	-6883		-6077	+2611

Table 11

W_2 B C^F

$\eta = -20°$

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\ C_n$
		0001	0001	0002	0002	0005	0004	0005	0005	0006
	1224	-0050	+0000	-0502	+0002	+0286	+0604		-0417	+9992
	1225	-0040	+0000	-0404	+0002	+0164	+0453		-0489	+7517
	1226	-0030	+0000	-0303	+0001	+0147	+0305		-0571	+7424
	1227	-0019	+0000	-0196	+0001	+0090	+0152		-0652	+7387
	1228	-0010	+0000	-0100	+0001	+0038	-0001		-0734	+7538
	1229	+0000	+0000	+0003	+0001	-0008	-0130		-0798	+7673
	1230	+0010	+0000	+0103	+0001	-0037	-0222		-0749	+8080
	1231	+0020	+0000	+0206	+0000	-0084	-0351		-0766	+7838
	1232	+0030	+0000	+0306	-0000	-0148	-0499		-0817	+7524
	1233	+0040	+0000	+0408	-0000	-0203	-0650		-0844	+7195
	1234	+0050	+0000	+0509	-0001	-0279	-0779		-0876	+6409
	1235	+0060	+0000	+0610	-0001	-0348	-0964		-0947	+5207
	1236	+0080	+0000	+0815	-0002	-0496	-1336		-1296	+4924
	1237	+0100	+0000	+1023	-0003	-0605	-1744		-1621	+4503
	1238	+0120	+0000	+1224	-0003	-0680	-2153		-1946	+4190
	1239	+0140	+0000	+1433	-0004	-0798	-2598		-2344	+4425
	1240	+0160	+0000	+1636	-0005	-0950	-3083		-2840	+4195
	1241	+0180	+0000	+1842	-0006	-1255	-3625		-3284	+6261
	1242	+0200	+0000	+2048	-0007	-1429	-4167		-3857	+5412
	1243	+0220	+0000	+2254	-0008	-1575	-4766		-4332	+7311
	1244	+0240	+0000	+2462	-0009	-1740	-5367		-4987	+3656
	1245	+0260	+0000	+2673	-0011	-2101	-6032		-5608	+6952
	1246	+0280	+0000	+2877	-0012	-2260	-6686		-6213	+5701
	1247	+0286	+0000	+2941	-0012	-2330	-6901		-6423	+5639

Table 12

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0005
W_2 B C^M	1251	-0040	+0000	-0406	+0002	+0343	+0617		+0499	-0275
	1252	-0030	+0000	-0306	+0001	+0290	+0477		+0368	-0249
	1253	-0020	+0000	-0203	+0001	+0195	+0320		+0251	-0215
	1254	-0010	+0000	-0101	+0001	+0149	+0178		+0098	-0162
	1255	+0000	+0000	+0001	+0000	+0101	+0036		-0010	-0144
	1256	+0010	+0000	+0101	+0000	+0018	-0104		-0111	-0087
	1257	+0020	+0000	+0206	-0000	-0028	-0246		-0279	-0063
	1258	+0030	+0000	+0306	-0001	-0102	-0406		-0419	-0024
	1259	+0040	+0000	+0406	-0001	-0194	-0584		-0562	+0005
	1260	+0050	+0000	+0510	-0001	-0258	-0744		-0687	-0020
	1261	+0060	+0000	+0614	-0002	-0349	-0919		-0823	+0073
	1262	+0080	+0000	+0815	-0003	-0558	-1313		-1135	+0202
$\eta = 0^\circ$	1263	+0100	+0000	+1021	-0004	-0711	-1719		-1494	+0207
	1264	+0120	+0000	+1225	-0004	-0863	-2131		-1870	+0315
	1265	+0140	+0000	+1432	-0005	-1039	-2576		-2271	+0399
	1266	+0160	+0000	+1639	-0006	-1195	-3073		-2695	+0496
	1267	+0180	+0000	+1843	-0008	-1561	-3590		-3121	+0617
	1268	+0200	+0000	+2053	-0009	-1699	-4146		-3655	+0465
	1269	+0220	+0000	+2256	-0010	-2045	-4718		-4158	+1079
	1270	+0240	+0000	+2463	-0011	-2119	-5541		-4664	+0708
	1271	+0260	+0000	+2677	-0013	-2496	-6040		-5306	+0681
	1272	+0279	+0000	+2865	-0014	-2747	-6649		-5806	+0928

Table 13

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0005	0005	0006
$W_2\ B\ C^M$	1275	-0050	+0000	-0506	+0002	+0375	+0807		+0939	-0187
$\eta = +5^\circ$	1276	-0040	+0000	-0408	+0002	+0300	+0637		+0832	-0610
	1277	-0030	+0000	-0304	+0001	+0247	+0480		+0695	-1143
	1278	-0020	+0000	-0206	+0001	+0191	+0323		+0560	-0873
	1279	-0010	+0000	-0102	+0001	+0142	+0181		+0412	-0417
	1280	+0000	+0000	-0001	+0001	+0098	+0055		+0290	-0235
	1281	+0010	+0000	+0100	+0000	+0051	-0086		+0172	-0936
	1282	+0020	+0000	+0204	-0000	-0021	-0248		+0016	+0145
	1283	+0030	+0000	+0303	-0000	-0068	-0392		-0139	+0683
	1284	+0040	+0000	+0408	-0001	-0134	-0572		-0284	+1201
	1285	+0050	+0000	+0510	-0001	-0227	-0716		-0393	+1522
	1286	+0060	+0000	+0611	-0002	-0304	-0896		-0522	+1341
	1287	+0080	+0000	+0816	-0003	-0518	-1293		-0859	+0358
	1288	+0100	+0000	+1019	-0003	-0649	-1707		-1201	+1177
	1289	+0120	+0000	+1223	-0004	-0734	-2102		-1526	+2404
	1290	+0141	+0000	+1437	-0005	-0883	-2571		-1892	+2754
	1291	+0160	+0000	+1637	-0005	-1005	-3025		-2254	+3534
	1292	+0180	+0000	+1842	-0007	-1375	-3551		-2632	+4478
	1293	+0201	+0000	+2054	-0008	-1481	-4111		-3105	+2744
	1294	+0220	+0000	+2256	-0009	-1836	-4675		-3560	+8644
	1295	+0240	+0000	+2462	-0009	-1847	-5285		-4018	+5554
	1296	+0260	+0000	+2669	-0011	-2204	-5939		-4602	+5323
	1297	+0280	+0000	+2881	-0013	-2458	-6640		-5115	+7171
	1298	+0286	+0000	+2938	-0013	-2572	-6808		-5272	+6653

Table 14

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0006
	1301	-0049	+0000	-0506	+0002	+0383	+0905		+1307	+1547
	1302	-0040	+0000	-0408	+0002	+0331	+0744		+1181	+1088
	1303	-0029	+0000	-0302	+0001	+0257	+0562		+1030	+0694
	1304	-0020	+0000	-0206	+0001	+0207	+0434		+0886	+1023
	1305	-0010	+0000	-0104	+0001	+0152	+0291		+0717	+1313
	1306	+0000	+0000	+0000	+0001	+0095	+0127		+0597	+1653
	1307	+0010	+0000	+0100	+0000	+0041	+0002		+0490	+2123
	1308	+0020	+0000	+0205	+0000	-0009	-0160		+0318	+2690
	1309	+0030	+0000	+0306	-0000	-0057	-0321		+0161	+3012
	1310	+0040	+0000	+0404	-0000	-0108	-0467		+0030	+3435
W_2 B C^M	1311	+0050	+0000	+0509	-0001	-0188	-0648		-0106	+3490
	1312	+0060	+0000	+0612	-0001	-0268	-0828		-0250	+2923
$\eta = +10^\circ$	1313	+0080	+0000	+0819	-0002	-0434	-1225		-0640	+3798
	1314	+0100	+0000	+1019	-0003	-0577	-1624		-0961	+3477
	1315	+0120	+0000	+1225	-0003	-0697	-2036		-1257	+3705
	1316	+0140	+0000	+1432	-0004	-0818	-2468		-1577	+4044
	1317	+0160	+0000	+1635	-0005	-0946	-2923		-1893	+3972
	1318	+0180	+0000	+1843	-0007	-1301	-3449		-2233	+5054
	1319	+0200	+0000	+2050	-0007	-1411	-3971		-2654	+3242
	1320	+0220	+0000	+2253	-0009	-1734	-4533		-3077	+8860
	1321	+0240	+0000	+2458	-0009	-1761	-5126		-3478	+5756
	1322	+0260	+0000	+2668	-0011	-2093	-5798		-4040	+4844
	1323	+0281	+0000	+2889	-0012	-2365	-6502		-4511	+7429
	1324	+0288	+0000	+2954	-0013	-2465	-6704		-4689	+7964

Table 15

W_2 B C^M

$\eta = +15°$

Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\ C_n$
Exponent / Configuration	~~0001~~	0001	0002	0002	0005	0004	0005	0005	0006
1329	-0030	+0000	-0309	+0002	+0243	+0578		+1350	+3269
1330	-0019	+0000	-0201	+0001	+0188	+0434		+1210	+3534
1331	-0010	+0000	-0106	+0001	+0131	+0290		+1010	+3748
1332	-0000	+0000	-0004	+0001	+0087	+0164		+0918	+3906
1333	+0010	+0000	+0098	+0001	+0045	+0041		+0848	+3826
1334	+0020	+0000	+0199	+0000	-0009	-0124		+0684	+3647
1335	+0031	+0000	+0308	-0000	-0081	-0288		+0474	+4496
1336	+0040	+0000	+0404	-0000	-0156	-0450		+0333	+4901
1337	+0050	+0000	+0511	-0001	-0229	-0633		+0181	+4919
1338	+0060	+0000	+0607	-0001	-0314	-0813		+0022	+4503
1339	+0080	+0000	+0814	-0002	-0536	-1212		-0384	+5507
1340	+0101	+0000	+1026	-0003	-0707	-1629		-0687	+5367
1341	+0120	+0000	+1223	-0004	-0843	-2011		-0963	+4848
1342	+0140	+0000	+1430	-0005	-1002	-2428		-1236	+5185
1343	+0160	+0000	+1633	-0006	-1150	-2882		-1492	+5685
1344	+0180	+0000	+1838	-0008	-1517	-3372		-1776	+6437
1345	+0200	+0000	+2048	-0009	-1684	-3932		-2143	+4323
1346	+0220	+0000	+2250	-0010	-1982	-4462		-2480	+9898
1347	+0240	+0000	+2457	-0011	-2052	-5079		-2856	+5570
1348	+0260	+0000	+2667	-0013	-2431	-5716		-3363	+5452
1349	+0280	+0000	+2873	-0014	-2707	-6372		-3740	+5616
1350	+0287	+0000	+2946	-0015	-2858	-6619		-3933	+6488

Table 16

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0005	0005	0006
$W_2\ B\ C^M$	1389	-0050	+0000	-0509	+0006	+1055	+0984		+1883	+2831
	1390	-0040	+0000	-0411	+0002	+0385	+0800		+1716	+3298
	1391	-0030	+0000	-0306	+0002	+0316	+0641		+1592	+2900
	1392	-0020	+0000	-0204	+0002	+0237	+0500		+1486	+2996
	1393	-0010	+0000	-0105	+0001	+0159	+0340		+1254	+4543
	1394	+0000	+0000	-0002	+0001	+0127	+0215		+1217	+3810
	1395	+0010	+0000	+0099	+0001	+0060	+0086		+1141	+3250
	1396	+0020	+0000	+0204	+0000	+0029	-0054		+1034	+2988
	1397	+0030	+0000	+0302	+0000	-0044	-0216		+0799	+3755
	1398	+0040	+0000	+0405	-0000	-0142	-0394		+0620	+4447
$\eta = +20^\circ$	1399	+0050	+0000	+0507	-0001	-0215	-0558		+0453	+3642
	1400	+0060	+0000	+0608	-0001	-0300	-0753		+0273	+3342
	1401	+0080	+0000	+0816	-0002	-0483	-1159		-0135	+4597
	1402	+0100	+0000	+1018	-0003	-0638	-1550		-0407	+4450
	1403	+0120	+0000	+1223	-0004	-0793	-1957		-0659	+4721
	1404	+0140	+0000	+1431	-0005	-0947	-2369		-0897	+4723
	1405	+0160	+0000	+1631	-0006	-1092	-2811		-1111	+5252
	1406	+0180	+0000	+1837	-0007	-1460	-3292		-1380	+6036
	1407	+0201	+0000	+2052	-0009	-1649	-3860		-1689	+4192
	1408	+0220	+0000	+2250	-0010	-1959	-4375		-1982	+9351
	1409	+0240	+0000	+2458	-0011	-2011	-4976		-2265	+4998
	1410	+0260	+0000	+2664	-0013	-2397	-5601		-2739	+5898
	1411	+0280	+0000	+2873	-0014	-2685	-6257		-3108	+7207
	1412	+0287	+0000	+2945	-0015	-2836	-6495		-3270	+6905

Table 17

W_2 B C^M

$\eta = -5°$

Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\ C_n$
Exponent / Configuration	0001	0001	0002	0002	0005	0004	0005	0005	0005
1415	-0049	+0000	-0505	+0002	+0352	+0725		+0280	+0226
1416	-0040	+0000	-0406	+0002	+0276	+0560		+0182	+0140
1417	-0030	+0000	-0304	+0001	+0207	+0395		+0067	+0139
1418	-0020	+0000	-0202	+0001	+0158	+0256		-0022	+0150
1419	-0010	+0000	-0102	+0001	+0110	+0111		-0158	+0138
1420	+0000	+0000	+0002	+0001	+0049	-0018		-0299	+0303
1421	+0010	+0000	+0101	+0000	-0002	-0157		-0394	+0307
1422	+0020	+0000	+0204	-0000	-0055	-0305		-0583	+0280
1423	+0030	+0000	+0306	-0001	-0163	-0472		-0729	+0288
1424	+0040	+0000	+0406	-0001	-0229	-0620		-0856	+0288
1425	+0051	+0000	+0516	-0001	-0308	-0804		-1004	+0272
1426	+0060	+0000	+0613	-0002	-0422	-0990		-1106	+0176
1427	+0080	+0000	+0819	-0003	-0573	-1361		-1403	+0204
1428	+0100	+0000	+1019	-0003	-0714	-1768		-1783	+0320
1429	+0120	+0000	+1224	-0004	-0849	-2193		-2196	+0341
1430	+0140	+0000	+1434	-0005	-0994	-2660		-2656	+0424
1431	+0160	+0000	+1636	-0006	-1155	-3123		-3100	+0573
1432	+0181	+0000	+1849	-0008	-1558	-3686		-3612	+0703
1433	+0200	+0000	+2049	-0009	-1718	-4227		-4171	+0582
1434	+0220	+0000	+2259	-0010	-2094	-4826		-4724	+1120
1435	+0240	+0000	+2466	-0011	-2180	-5446		-5321	+0984
1436	+0260	+0000	+2678	-0013	-2509	-6139		-6013	+0821
1437	+0280	+0000	+2879	-0014	-2821	-6825		-6540	+0967
1438	+0286	+0000	+2945	-0015	-2919	-7006		-6762	+1037

Table 18

W_2 B C^M

$\eta = -10°$

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0005	0005	0005
	1441	-0050	+0000	-0504	+0002	+0339	+0691		+0025	+0634
	1442	-0040	+0000	-0405	+0002	+0264	+0526		-0080	+0581
	1443	-0030	+0000	-0304	+0001	+0194	+0364		-0161	+0479
	1444	-0020	+0000	-0202	+0001	+0136	+0217		-0340	+0531
	1445	-0010	+0000	-0101	+0001	+0080	+0054		-0528	+0539
	1446	+0000	+0000	+0002	+0001	+0036	-0072		-0635	+0621
	1447	+0010	+0000	+0105	+0000	-0022	-0201		-0721	+0657
	1448	+0020	+0000	+0206	+0000	-0070	-0346		-0846	+0645
	1449	+0030	+0000	+0306	-0000	-0154	-0509		-1003	+0659
	1450	+0040	+0000	+0410	-0001	-0224	-0671		-1145	+0651
	1451	+0050	+0000	+0511	-0001	-0298	-0834		-1287	+0601
	1452	+0060	+0000	+0612	-0002	-0385	-1017		-1424	+0557
	1453	+0080	+0000	+0817	-0002	-0539	-1397		-1777	+0572
	1454	+0100	+0000	+1022	-0003	-0705	-1812		-2104	+0578
	1455	+0120	+0000	+1227	-0004	-0870	-2246		-2509	+0601
	1456	+0140	+0000	+1435	-0005	-0998	-2700		-2984	+0597
	1457	+0160	+0000	+1639	-0006	-1176	-3187		-3473	+0684
	1458	+0180	+0000	+1844	-0008	-1593	-3718		-4026	+0859
	1459	+0200	+0000	+2051	-0009	-1791	-4301		-4601	+0695
	1460	+0220	+0000	+2262	-0011	-2174	-4901		-5159	+1292
	1461	+0240	+0000	+2467	-0011	-2260	-5537		-5772	+1048
	1462	+0260	+0000	+2677	-0013	-2603	-6211		-6465	+0931
	1463	+0280	+0000	+2880	-0015	-2893	-6887		-7031	+0985
	1464	+0285	+0000	+2937	-0015	-3010	-7057		-7211	+0926

Table 19

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0005	0005	0005
W_2 B C^M	1468	-0040	+0000	-0404	+0002	+0268	+0477		-0422	+0911
$\eta = -15^\circ$	1469	-0030	+0000	-0304	+0002	+0221	+0311		-0528	+0790
	1470	-0020	+0000	-0200	+0002	+0166	+0167		-0676	+0721
	1471	-0010	+0000	-0097	+0001	+0096	-0015		-0931	+0727
	1472	+0000	+0000	+0003	+0001	+0033	-0139		-0997	+0775
	1473	+0010	+0000	+0103	+0001	-0022	-0265		-1131	+0937
	1474	+0020	+0000	+0207	+0000	-0076	-0421		-1254	+0909
	1475	+0030	+0000	+0308	-0000	-0158	-0581		-1399	+0922
	1476	+0040	+0000	+0410	-0000	-0232	-0737		-1478	+0924
	1477	+0050	+0000	+0512	-0001	-0324	-0913		-1609	+0855
	1478	+0060	+0000	+0613	-0001	-0398	-1089		-1784	+0811
	1479	+0080	+0000	+0824	-0002	-0574	-1489		-2171	+0888
	1480	+0100	+0000	+1025	-0003	-0734	-1889		-2471	+0924
	1481	+0120	+0000	+1228	-0004	-0867	-2305		-2846	+0872
	1482	+0140	+0000	+1440	-0005	-1031	-2774		-3287	+0884
	1483	+0160	+0000	+1640	-0006	-1197	-3265		-3801	+0910
	1484	+0180	+0000	+1847	-0008	-1597	-3791		-4387	+1124
	1485	+0200	+0000	+2053	-0009	-1801	-4369		-4985	+0936
	1486	+0220	+0000	+2262	-0011	-2218	-4983		-5592	+1569
	1487	+0240	+0000	+2468	-0012	-2324	-5601		-6194	+1423
	1488	+0260	+0000	+2678	-0014	-2722	-6286		-6881	+1393
	1489	+0278	+0000	+2861	-0015	-3000	-6891		-7454	+1416

Table 20

W_2 B C^M

$\eta = -20°$

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0005	0005	0005
	1492	-0049	+0000	-0501	+0002	+0302	+0584		-0560	+0640
	1493	-0040	+0000	-0403	+0002	+0247	+0420		-0694	+0553
	1494	-0030	+0000	-0300	+0002	+0188	+0255		-0874	+0551
	1495	-0020	+0000	-0200	+0001	+0136	+0111		-1058	+0525
	1496	-0010	+0000	-0097	+0001	+0043	-0055		-1215	+0641
	1497	+0000	+0000	+0005	+0000	-0020	-0181		-1278	+0659
	1498	+0010	+0000	+0107	+0000	-0081	-0310		-1348	+0717
	1499	+0020	+0000	+0208	-0000	-0155	-0471		-1430	+0762
	1500	+0030	+0000	+0308	-0000	-0212	-0614		-1579	+0749
	1501	+0040	+0000	+0413	-0001	-0279	-0776		-1615	+0686
	1502	+0050	+0000	+0514	-0001	-0352	-0920		-1724	+0657
	1503	+0060	+0000	+0617	-0002	-0441	-1118		-1870	+0615
	1504	+0080	+0000	+0821	-0003	-0637	-1515		-2329	+0735
	1505	+0100	+0000	+1023	-0004	-0785	-1895		-2608	+0772
	1506	+0120	+0000	+1228	-0004	-0952	-2327		-3027	+0787
	1507	+0140	+0000	+1435	-0005	-1106	-2775		-3457	+0823
	1508	+0160	+0000	+1645	-0006	-1337	-3301		-3972	+0959
	1509	+0180	+0000	+1850	-0008	-1709	-3830		-4598	+1085
	1510	+0200	+0000	+2053	-0010	-1951	-4392		-5207	+1050
	1511	+0220	+0000	+2262	-0011	-2321	-5008		-5812	+1572
	1512	+0240	+0000	+2468	-0012	-2509	-5661		-6470	+1496
	1513	+0260	+0000	+2677	-0014	-2813	-6336		-7199	+1309
	1514	+0280	+0000	+2884	-0016	-3185	-7005		-7843	+1350
	1515	+0284	+0000	+2925	-0016	-3248	-7158		-7966	+1199

Table 21

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0005	0005	0005
W_2 B C^R	1520	-0049	+0000	-0504	+0003	+0537	+0766		+0717	+0001
	1521	-0040	+0000	-0407	+0003	+0450	+0609		+0609	-0006
	1522	-0030	+0000	-0307	+0002	+0349	+0452		+0456	+0004
	1523	-0020	+0000	-0201	+0002	+0277	+0295		+0290	+0076
	1524	-0010	+0000	-0102	+0001	+0196	+0158		+0148	+0104
	1525	+0000	+0000	-0000	+0001	+0112	+0019		+0013	+0186
	1526	+0010	+0000	+0103	+0000	+0021	-0138		-0110	+0196
	1527	+0020	+0000	+0203	+0000	-0042	-0274		-0257	+0249
	1528	+0030	+0000	+0306	-0000	-0107	-0414		-0406	+0297
	1529	+0040	+0000	+0406	-0001	-0235	-0593		-0536	+0355
	1530	+0050	+0000	+0511	-0001	-0328	-0768		-0690	+0355
	1531	+0060	+0000	+0612	-0002	-0444	-0943		-0829	+0360
$\eta = 0^\circ$	1532	+0080	+0000	+0821	-0003	-0675	-1346		-1223	+0449
	1533	+0100	+0000	+1023	-0004	-0863	-1730		-1609	+0538
	1534	+0120	+0000	+1226	-0005	-1044	-2148		-2001	+0610
	1535	+0140	+0000	+1436	-0006	-1239	-2604		-2418	+0730
	1536	+0160	+0000	+1636	-0007	-1477	-3077		-2809	+0879
	1537	+0180	+0000	+1844	-0010	-1926	-3605		-3294	+1060
	1538	+0200	+0000	+2050	-0011	-2153	-4145		-3817	+0985
	1539	+0220	+0000	+2258	-0013	-2581	-4742		-4344	+1509
	1540	+0240	+0000	+2465	-0014	-2710	-5358		-4915	+1130
	1541	+0260	+0000	+2674	-0017	-3198	-6028		-5602	+1202
	1542	+0280	+0000	+2883	-0019	-3601	-6713		-6229	+1467
	1543	+0285	+0000	+2937	-0019	-3737	-6891		-6406	+1439

Table 22

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0005
$W_2\ B\ C^R$	1548	-0049	+0000	-0505	+0003	+0443	+0834		+1141	+0824
	1549	-0040	+0000	-0406	+0003	+0368	+0668		+0996	+0806
	1550	-0030	+0000	-0305	+0002	+0294	+0503		+0852	+0756
	1551	-0020	+0000	-0202	+0002	+0228	+0337		+0691	+0767
	1552	-0010	+0000	-0100	+0002	+0155	+0189		+0517	+0810
	1553	+0000	+0000	+0000	+0001	+0110	+0058		+0385	+0795
	1554	+0011	+0000	+0106	+0001	+0065	-0071		+0274	+0846
	1555	+0020	+0000	+0203	+0001	-0005	-0219		+0101	+0897
	1556	+0030	+0000	+0304	+0001	-0054	-0366		-0012	+0916
	1557	+0040	+0000	+0407	+0000	-0114	-0514		-0139	+0933
	1558	+0050	+0000	+0510	-0000	-0198	-0703		-0286	+0871
	1559	+0060	+0000	+0611	-0001	-0279	-0869		-0416	+0868
$\eta = +5^\circ$	1560	+0080	+0000	+0815	-0002	-0446	-1277		-0846	+0871
	1561	+0100	+0000	+1019	-0002	-0575	-1670		-1207	+0918
	1562	+0120	+0000	+1224	-0003	-0705	-2096		-1565	+0984
	1563	+0140	+0000	+1430	-0003	-0836	-2522		-1921	+1019
	1564	+0160	+0000	+1634	-0004	-1003	-3005		-2279	+1173
	1565	+0180	+0000	+1841	-0006	-1385	-3508		-2662	+1298
	1566	+0200	+0000	+2049	-0007	-1577	-4063		-3159	+1199
	1567	+0220	+0000	+2252	-0008	-1882	-4603		-3603	+1737
	1568	+0240	+0000	+2461	-0009	-1981	-5238		-4105	+1444
	1569	+0260	+0000	+2670	-0011	-2380	-5888		-4739	+1430
	1570	+0280	+0000	+2878	-0012	-2658	-6578		-5288	+1779
	1571	+0286	+0000	+2936	-0013	-2781	-6768		-5483	+1786

Table 23

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\ C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0005
W_2 B C^R	1681	-0050	+0000	-0507	+0003	+0479	+0878		+1487	+0741
	1682	-0040	+0000	-0410	+0003	+0393	+0740		+1359	+0662
	1683	-0030	+0000	-0307	+0002	+0318	+0563		+1167	+0650
	1684	-0020	+0000	-0201	+0002	+0248	+0388		+0984	+0615
	1685	-0010	+0000	-0104	+0001	+0133	+0248		+0820	+0570
	1686	+0000	+0000	-0002	+0001	+0090	+0124		+0709	+0555
	1687	+0010	+0000	+0099	+0001	+0024	-0015		+0588	+0600
	1688	+0020	+0000	+0202	+0000	-0031	-0172		+0436	+0605
	1689	+0030	+0000	+0302	+0000	-0095	-0311		+0301	+0628
	1690	+0041	+0000	+0410	-0000	-0170	-0489		+0162	+0674
	1691	+0050	+0000	+0509	-0000	-0214	-0645		+0039	+0774
	1692	+0060	+0000	+0609	-0001	-0294	-0822		-0121	+0742
$\eta = +10^\circ$	1693	+0080	+0000	+0814	-0002	-0484	-1227		-0610	+0783
	1694	+0100	+0000	+1022	-0003	-0620	-1613		-0937	+0823
	1695	+0120	+0000	+1224	-0004	-0771	-2018		-1222	+0829
	1696	+0140	+0000	+1429	-0004	-0908	-2469		-1521	+0820
	1697	+0160	+0000	+1634	-0005	-1088	-2927		-1835	+0958
	1698	+0180	+0000	+1840	-0007	-1499	-3436		-2186	+1089
	1699	+0200	+0000	+2046	-0009	-1787	-3964		-2596	+1082
	1700	+0220	+0000	+2254	-0010	-2030	-4527		-2999	+1494
	1701	+0240	+0000	+2461	-0012	-2274	-5142		-3447	+0956
	1702	+0260	+0000	+2668	-0014	-2663	-5793		-4049	+1084
	1703	+0278	+0000	+2860	-0015	-2915	-6397		-4448	+1157

Table 24

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0006
W_2 B C^R	1700	-0049	+0000	-0508	+0003	+0449	+0969		+2021	-0079
$\eta = +15^\circ$	1707	-0040	+0000	-0410	+0002	+0362	+0797		+1855	-0933
	1708	-0030	+0000	-0308	+0002	+0289	+0623		+1682	-1385
	1709	-0020	+0000	-0207	+0001	+0217	+0485		+1490	-0852
	1710	-0010	+0000	-0104	+0001	+0144	+0328		+1347	-0443
	1711	+0000	+0000	-0003	+0001	+0104	+0209		+1288	-0231
	1712	+0010	+0000	+0099	+0000	+0024	+0071		+1126	+0374
	1713	+0020	+0000	+0199	-0000	-0044	-0086		+0912	+0886
	1714	+0030	+0000	+0303	-0001	-0113	-0240		+0776	+1047
	1715	+0040	+0000	+0406	-0001	-0171	-0397		+0648	+0988
	1716	+0050	+0000	+0507	-0001	-0257	-0571		+0489	+1659
	1717	+0060	+0000	+0609	-0002	-0354	-0762		+0314	+1486
	1718	+0080	+0000	+0818	-0003	-0555	-1176		-0235	+2472
	1719	+0100	+0000	+1020	-0004	-0684	-1557		-0557	+3042
	1720	+0120	+0000	+1224	-0004	-0816	-1956		-0795	+2715
	1721	+0140	+0000	+1431	-0005	-0974	-2386		-1060	+2692
	1722	+0160	+0000	+1636	-0006	-1135	-2853		-1329	+4383
	1723	+0180	+0000	+1841	-0008	-1567	-3339		-1607	+5627
	1724	+0200	+0000	+2048	-0010	-1850	-3875		-1949	+4144
	1725	+0220	+0000	+2255	-0011	-2137	-4430		-2304	+8520
	1726	+0240	+0000	+2461	-0012	-2278	-5012		-2667	+6533
	1727	+0260	+0000	+2669	-0015	-2693	-5674		-3213	+7223
	1728	+0280	+0000	+2876	-0016	-3018	-6331		-3635	+8602
	1729	+0284	+0000	+2922	-0017	-3121	-6473		-3739	+8770

Table 25

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0006
W_2 B C^R	1732	-0049	+0000	-0507	+0002	+0475	+1002		+2323	-3875
	1733	-0040	+0000	-0408	+0002	+0394	+0823		+2181	-3888
	1734	-0030	+0000	-0306	+0001	+0314	+0683		+2004	-3487
	1735	-0020	+0000	-0208	+0001	+0239	+0538		+1874	-3217
	1736	-0010	+0000	-0104	+0001	+0182	+0377		+1808	-3553
	1737	+0000	+0000	-0004	+0000	+0128	+0270		+1749	-3204
	1738	+0010	+0000	+0098	-0000	+0024	+0127		+1610	-2343
	1739	+0020	+0000	+0200	-0000	-0028	-0033		+1365	-2127
	1740	+0030	+0000	+0303	-0001	-0093	-0178		+1175	-1535
	1741	+0040	+0000	+0404	-0001	-0170	-0339		+1049	-1241
	1742	+0050	+0000	+0506	-0002	-0257	-0519		+0899	-1424
$\eta = +20^\circ$	1743	+0060	+0000	+0609	-0002	-0353	-0718		+0658	-1055
	1744	+0080	+0000	+0815	-0003	-0562	-1132		+0075	+0445
	1745	+0100	+0000	+1018	-0004	-0709	-1526		-0223	+0909
	1746	+0120	+0000	+1222	-0005	-0852	-1903		-0415	+1047
	1747	+0140	+0000	+1427	-0005	-1005	-2332		-0644	+1572
	1748	+0160	+0000	+1634	-0006	-1198	-2798		-0862	+3313
	1749	+0180	+0000	+1837	-0008	-1630	-3269		-1102	+4254
	1750	+0200	+0000	+2044	-0010	-1927	-3806		-1425	+3708
	1751	+0220	+0000	+2251	-0011	-2212	-4343		-1715	+8383
	1752	+0240	+0000	+2457	-0012	-2353	-4952		-2063	+6211
	1753	+0260	+0000	+2668	-0015	-2827	-5600		-2537	+7135
	1754	+0280	+0000	+2871	-0016	-3141	-6236		-2897	+8708
	1755	+0284	+0000	+2916	-0017	-3266	-6386		-2997	+8991

Table 26

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0005
$W_2\ B\ C^R$	1570	-0050	+0000	-0505	+0002	+0357	+0752		+0382	+0135
$\eta = -5^\circ$	1577	-0040	+0000	-0405	+0002	+0276	+0570		+0253	+0077
	1578	-0030	+0000	-0304	+0001	+0222	+0430		+0130	+0070
	1579	-0020	+0000	-0204	+0001	+0171	+0285		-0009	+0082
	1580	-0010	+0000	-0101	+0001	+0115	+0122		-0201	+0120
	1581	+0000	+0000	+0001	+0000	+0030	-0018		-0330	+0170
	1582	+0010	+0000	+0101	+0000	-0013	-0141		-0435	+0220
	1583	+0020	+0000	+0206	-0000	-0065	-0300		-0618	+0235
	1584	+0030	+0000	+0307	-0000	-0121	-0459		-0774	+0273
	1585	+0040	+0000	+0409	-0001	-0194	-0637		-0916	+0234
	1586	+0050	+0000	+0510	-0001	-0278	-0781		-1085	+0264
	1587	+0060	+0000	+0612	-0002	-0370	-0980		-1209	+0212
	1588	+0080	+0000	+0820	-0003	-0511	-1356		-1559	+0206
	1589	+0100	+0000	+1022	-0003	-0627	-1767		-1988	+0271
	1590	+0120	+0000	+1227	-0004	-0786	-2200		-2438	+0315
	1591	+0140	+0000	+1432	-0005	-0914	-2668		-2928	+0323
	1592	+0160	+0000	+1637	-0005	-1077	-3140		-3423	+0541
	1593	+0180	+0000	+1845	-0007	-1484	-3685		-3969	+0720
	1594	+0200	+0000	+2052	-0009	-1706	-4232		-4579	+0649
	1595	+0220	+0000	+2257	-0010	-2020	-4831		-5153	+1082
	1596	+0240	+0000	+2464	-0011	-2113	-5452		-5775	+0718
	1597	+0260	+0000	+2673	-0013	-2512	-6153		-6585	+0826
	1598	+0278	+0000	+2862	-0014	-2745	-6773		-7196	+0912

Table 27

W_2 B C^R

$\eta = -10°$

Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\ C_n$
Exponent / Configuration	0001	0001	0002	0002	0005	0004	0005	0005	0005
1601	-0049	+0000	-0501	+0003	+0404	+0672		-0036	+0443
1602	-0040	+0000	-0402	+0002	+0332	+0506		-0149	+0400
1603	-0030	+0000	-0303	+0002	+0273	+0263		-0259	+0383
1604	-0020	+0000	-0202	+0002	+0222	+0216		-0408	+0426
1605	-0010	+0000	-0099	+0001	+0154	+0073		-0571	+0445
1606	+0000	+0000	+0004	+0001	+0082	-0091		-0730	+0496
1607	+0010	+0000	+0104	+0001	+0040	-0217		-0839	+0555
1608	+0020	+0000	+0205	+0000	-0026	-0363		-1009	+0582
1609	+0030	+0000	+0308	+0000	-0090	-0526		-1229	+0598
1610	+0040	+0000	+0412	-0000	-0194	-0686		-1397	+0606
1611	+0050	+0000	+0513	-0001	-0274	-0859		-1537	+0601
1612	+0060	+0000	+0617	-0001	-0368	-1062		-1694	+0552
1613	+0080	+0000	+0817	-0002	-0510	-1413		-1991	+0724
1614	+0100	+0000	+1025	-0003	-0623	-1834		-2436	+0875
1615	+0120	+0000	+1232	-0003	-0780	-2288		-2937	+0942
1616	+0140	+0000	+1436	-0004	-0991	-2740		-3475	+0897
1617	+0160	+0000	+1640	-0005	-1180	-3233		-4019	+1084
1618	+0180	+0000	+1844	-0007	-1568	-3762		-4636	+1294
1619	+0200	+0000	+2052	-0009	-1864	-4344		-5319	+1135
1620	+0221	+0000	+2265	-0010	-2189	-4964		-6004	+1688
1621	+0240	+0000	+2467	-0011	-2283	-5583		-6671	+1534
1622	+0260	+0000	+2680	-0013	-2715	-6277		-7438	+1501
1623	+0280	+0000	+2884	-0015	-3066	-6945		-8087	+1685
1624	+0285	+0000	+2933	-0015	-3159	-7113		-8246	+1768

Table 28

W_2 B C^R

$\eta = -15°$

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0005	0005	0005
	1627	-0050	+0000	-0503	+0003	+0321	+0652		-0299	+0731
	1628	-0040	+0000	-0405	+0002	+0251	+0498		-0405	+0650
	1629	-0030	+0000	-0302	+0002	+0215	+0344		-0526	+0650
	1630	-0019	+0000	-0196	+0002	+0156	+0188		-0683	+0669
	1631	-0010	+0000	-0098	+0001	+0088	+0034		-0875	+0688
	1632	+0000	+0000	+0002	+0001	+0020	-0121		-1067	+0739
	1633	+0010	+0000	+0106	+0001	-0040	-0243		-1162	+0789
	1634	+0020	+0000	+0206	+0000	-0111	-0397		-1326	+0798
	1635	+0030	+0000	+0308	-0000	-0180	-0568		-1534	+0796
	1636	+0040	+0000	+0409	-0001	-0247	-0737		-1721	+0834
	1637	+0051	+0000	+0518	-0001	-0346	-0926		-1890	+0809
	1638	+0060	+0000	+0613	-0002	-0442	-1081		-2025	+0802
	1639	+0080	+0000	+0824	-0003	-0613	-1477		-2370	+0766
	1640	+0100	+0000	+1024	-0003	-0738	-1868		-2788	+0843
	1641	+0120	+0000	+1228	-0004	-0895	-2315		-3341	+0986
	1642	+0140	+0000	+1436	-0005	-1052	-2795		-3920	+1058
	1643	+0160	+0000	+1641	-0006	-1249	-3294		-4524	+1262
	1644	+0180	+0000	+1849	-0008	-1713	-3830		-5160	+1478
	1645	+0200	+0000	+2061	-0010	-1906	-4431		-5890	+1371
	1647	+0220	+0000	+2264	-0011	-2252	-5006		-6496	+1604
	1648	+0240	+0000	+2474	-0013	-2443	-5663		-7160	+1245
	1649	+0260	+0000	+2680	-0015	-2799	-6324		-7890	+1201
	1650	+0280	+0000	+2888	-0016	-3085	-6993		-8508	+1331
	1652	+0284	+0000	+2931	-0017	-3226	-7146		-8688	+1175

Table 29

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
		0001	0001	0002	0002	0005	0004	0006	0005	0005
$W_2\ B\ C^R$	1656	-0050	+0000	-0502	+0002	+0297	+0591		-0691	+0088
	1657	-0040	+0000	-0405	+0001	+0227	+0429		-0837	-0016
	1658	-0030	+0000	-0300	+0001	+0169	+0270		-0963	+0009
	1659	-0019	+0000	-0195	+0001	+0113	+0109		-1111	-0019
	1660	-0010	+0000	-0095	+0000	+0066	-0033		-1381	+0003
	1661	+0000	+0000	+0007	+0000	-0005	-0197		-1610	+0088
	1662	+0010	+0000	+0104	-0000	-0076	-0304		-1683	+0126
	1663	+0020	+0000	+0208	-0001	-0134	-0463		-1823	+0121
	1664	+0030	+0000	+0309	-0001	-0196	-0622		-2069	+0298
	1665	+0040	+0000	+0414	-0001	-0289	-0801		-2256	+0258
$\eta = -20^\circ$	1666	+0050	+0000	+0515	-0002	-0376	-0979		-2427	+0241
	1667	+0060	+0000	+0619	-0002	-0463	-1173		-2601	+0235
	1668	+0080	+0000	+0821	-0003	-0633	-1546		-2976	+0222
	1669	+0100	+0000	+1026	-0004	-0771	-1933		-3272	+0295
	1670	+0120	+0000	+1231	-0005	-0933	-2374		-3798	+0360
	1671	+0140	+0000	+1437	-0005	-1063	-2837		-4386	+0486
	1672	+0160	+0000	+1646	-0006	-1311	-3374		-5017	+0761
	1673	+0180	+0000	+1851	-0009	-1755	-3911		-5703	+0994
	1674	+0200	+0000	+2056	-0010	-1970	-4464		-6376	+0811
	1675	+0220	+0000	+2265	-0011	-2280	-5085		-7039	+1137
	1676	+0240	+0000	+2470	-0012	-2428	-5708		-7692	+0942
	1677	+0260	+0000	+2690	-0015	-2872	-6389		-8463	+0937
	1678	+0278	+0000	+2863	-0016	-3181	-6997		-9005	+1155

Table 30

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0006	-0004	-0006	-0006	-0006
	2528	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	2523	+0052	-1800	-0521	-0000	+0324	+0633	+3571	+0627	+4150
†	2524	+0041	-1800	-0410	-0000	+0163	+0492	+0000	+0292	+0291
†	2525	+0030	-1800	-0303	-0000	+0033	+0349	+0000	+0563	+0675
†	2526	+0021	-1800	-0209	-0000	-0022	+0238	+0000	+0409	+1295
†	2527	+0011	-1800	-0107	-0000	+0389	+0119	+0000	+0086	+1054
	2529	+0010	+0000	+0099	+0000	-0165	-0102	+0000	-0177	-1305
	2530	+0020	-0000	+0204	-0000	+0059	-0238	-0148	+0199	+0119
	2531	+0032	+0000	+0316	+0000	-0085	-0380	-0148	+0236	-1308
	2532	+0042	+0000	+0423	+0000	-0291	-0514	-0148	+0388	+0288
	2533	+0050	+0000	+0501	+0000	-0060	-0616	-0298	+0226	-2387
	2534	+0061	-0000	+0606	-0000	+0314	-0767	-0298	+0537	-1430
W_2	2535	+0082	+0000	+0818	+0000	-0247	-1082	-0285	+1616	+0333
	2536	+0101	-0000	+1012	-0000	+0112	-1384	-0136	+2892	+0708
	2537	+0122	-0000	+1216	-0000	+0127	-1718	+0321	+3894	+2382
	2538	+0142	-0000	+1421	-0000	+0313	-2084	+0470	+3746	+4364
	2539	+0163	-0000	+1628	-0000	+0522	-2482	+0768	+5614	+6689
	2540	+0183	+0000	+1832	+0000	-1204	-2892	+1807	+6721	+5612
	2541	+0203	-0000	+2034	-0000	-0644	-3330	+1958	+7502	+7809
	2542	+0224	+0000	+2240	+0000	-0946	-3806	+2697	+8252	+1801
	2543	+0245	+0000	+2447	+0000	-0566	-4307	+2697	+8710	+1584
	2544	+0265	+0000	+2655	+0000	-1101	-4839	+3737	+9056	-1455
	2545	+0286	+0000	+2861	+0000	-1079	-5369	+4047	+9904	-1948
	2546	+0294	+0000	+2940	+0000	-1249	-5590	+4640	+9050	-2172
	2550	+0001	-1800	-0007	+0000	+0211	+0023	-0608	-1819	-1403
	2550	+0018	-1014	-0035	-0176	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 31

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0006	-0006	-0005
	2557	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	≠2552	+0051	-1751	-0506	-0044	+0058	+0616	-0452	+0013	+0290
	≠2553	+0040	-1751	-0402	-0035	+0037	+0480	-0451	+0475	+0279
	≠2554	+0030	-1751	-0302	-0026	+0039	+0360	-0301	+0676	+0171
	≠2555	+0020	-1751	-0202	-0017	+0005	+0232	+0000	+0094	+0058
	≠2556	+0010	-1751	-0101	-0009	+0000	+0120	+0000	+0141	+0121
	2558	+0010	+0049	+0101	+0009	-0007	-0113	+0000	-0227	-0071
	2559	+0020	+0050	+0203	+0018	-0045	-0232	+0000	+0197	-0093
	2560	+0030	+0049	+0303	+0026	-0033	-0361	-0301	+0045	+0026
	2561	+0041	+0049	+0406	+0035	-0022	-0490	-0452	+0438	-0074
W_2	2562	+0051	+0049	+0507	+0044	-0031	-0626	-0591	+0336	-0034
	2563	+0061	+0049	+0606	+0052	-0056	-0762	-0892	+0181	-0195
	2565	+0102	+0049	+1012	+0087	-0019	-1397	-1773	+1769	-0310
	2566	+0122	+0049	+1215	+0104	-0029	-1719	-1911	+3162	+0219
	2567	+0143	+0049	+1420	+0121	-0084	-2089	-2213	+5063	+0266
	2568	+0163	+0049	+1623	+0138	-0276	-2474	-2199	+6372	+0439
	2569	+0183	+0049	+1827	+0155	-0413	-2892	-1596	+6693	+0274
	2570	+0204	+0049	+2032	+0172	-0543	-3341	-1283	+7636	+0057
	2571	+0224	+0049	+2235	+0188	-0627	-3808	-0981	+8415	-0066
	2572	+0245	+0049	+2441	+0204	-0687	-4299	-1433	+9013	-0066
	2573	+0266	+0049	+2646	+0220	-0866	-4819	-0818	+9734	-0250
	2574	+0286	+0049	+2850	+0236	-0943	-5366	-0654	+9485	-0492
	2575	+0294	+0049	+2932	+0242	-1074	-5582	-0178	+7792	-1215
	2577	+0000	-1770	-0001	-0000	+0072	-0002	-0255	-1079	-0151

≠ For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 32

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0006	-0006	-0005
	2584	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	2579	+0051	-1701	-0501	-0087	+0185	+0609	-1191	+1142	+0884
†	2580	+0040	-1701	-0398	-0070	+0195	+0482	-1041	+1260	+0657
†	2581	+0030	-1701	-0299	-0052	+0122	+0356	-0446	+0972	+0514
†	2582	+0020	-1701	-0201	-0035	+0083	+0237	-0148	+0885	+0413
†	2583	+0010	-1700	-0100	-0018	+0081	+0118	+0000	+0173	+0333
	2585	+0010	+0099	+0099	+0017	-0056	-0102	+0000	-0193	+0004
	2586	+0020	+0099	+0200	+0035	-0085	-0229	+0000	-0091	-0090
	2587	+0030	+0099	+0299	+0052	-0122	-0347	-0298	+0093	-0067
	2589	+0041	+0099	+0400	+0070	-0175	-0479	-0731	+0072	-0187
W_2	2591	+0061	+0099	+0599	+0104	-0202	-0747	-1760	+0463	+0011
	2592	+0081	+0099	+0801	+0139	-0157	-1057	-2652	+1561	+0166
	2593	+0102	+0099	+1000	+0173	-0206	-1382	-2936	+2358	-0037
	2594	+0122	+0099	+1202	+0207	-0298	-1713	-3973	+3242	+0003
	2595	+0142	+0099	+1403	+0241	-0441	-2070	-4567	+4730	+0232
	2596	+0163	+0099	+1603	+0275	-0759	-2455	-5162	+5364	+0230
	2597	+0183	+0099	+1805	+0309	-0905	-2851	-5459	+6354	+0247
	2598	+0204	+0099	+2007	+0342	-1151	-3293	-5595	+7238	+0432
	2599	+0224	+0099	+2208	+0374	-1282	-3752	-5743	+6975	-0078
	2600	+0245	+0099	+2411	+0407	-1528	-4250	-6040	+7788	-0707
	2601	+0266	+0099	+2613	+0439	-1783	-4740	-6487	+7875	-1131
	2602	+0286	+0099	+2815	+0470	-1975	-5286	-6326	+7163	-1580
	2603	+0294	+0099	+2896	+0483	-2110	-5499	-6165	+6494	-2277
	2604	+0000	-1672	-0002	-0000	+0029	+0002	-0624	-0375	+0449

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 33

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0006	-0006
	2611	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
✓	2606	+0051	-1652	-0491	-0130	+0236	+0595	+0031	+0374	+4550
✓	2607	+0040	-1651	-0391	-0104	+0249	+0469	-0131	+0526	+3845
✓	2608	+0030	-1651	-0294	-0078	+0207	+0343	-0088	+0612	+2833
✓	2609	+0020	-1651	-0195	-0052	+0125	+0226	-0044	+0140	+1284
✓	2610	+0010	-1651	-0097	-0026	+0085	+0109	-0015	+0020	-1515
	2612	+0010	+0149	+0098	+0026	-0055	-0101	+0000	-0192	+0045
	2613	+0020	+0149	+0197	+0052	-0125	-0226	-0015	-0140	-1367
	2614	+0030	+0149	+0295	+0078	-0204	-0343	-0015	-0276	-2869
W_2	2615	+0041	+0148	+0393	+0104	-0230	-0468	-0029	+0128	-0714
	2616	+0051	+0148	+0491	+0130	-0250	-0602	-0177	+0116	-0060
	2617	+0061	+0148	+0588	+0155	-0310	-0734	-0235	+0286	-0221
	2618	+0081	+0148	+0786	+0207	-0267	-1041	-0324	+1106	+0007
	2619	+0102	+0148	+0982	+0258	-0375	-1354	-0530	+1912	-1652
	2620	+0122	+0148	+1178	+0309	-0585	-1682	-0618	+3010	-0706
	2621	+0142	+0148	+1377	+0360	-0885	-2033	-0677	+4354	+3317
	2622	+0163	+0148	+1573	+0410	-1124	-2424	-0708	+5219	+2429
	2623	+0183	+0148	+1770	+0460	-1348	-2815	-0899	+6135	+3247
	2625	+0204	+0148	+1969	+0510	-1655	-3244	-0958	+7024	+0829
	2626	+0224	+0148	+2165	+0559	-1900	-3690	-0987	+8105	+4405
	2627	+0245	+0148	+2363	+0607	-2258	-4150	-1061	+8368	-0147
	2628	+0266	+0148	+2561	+0655	-2538	-4644	-1150	+9831	+1208
	2629	+0286	+0148	+2758	+0701	-2865	-5174	-1209	+9642	-2244
	2630	+0294	+0148	+2837	+0720	-2974	-5377	-1224	+9595	-2065
	2631	+0000	-1669	-0001	-0000	+0095	-0006	-0101	-2312	-5914
	2631	+0017	-1024	-0036	-0166	+0000	+0000	+0000	+0000	+0000

✓ For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 34

Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
Exponent	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0006	-0005
	2640	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	2633 †	+0051	-1602	-0477	-0172	+0321	+0580	-0014	+0657	+0286
	2635 †	+0040	-1602	-0380	-0137	+0275	+0450	-0167	+0054	+0130
	2636 †	+0030	-1602	-0285	-0103	+0271	+0337	-0107	+0377	+0338
	2637 †	+0020	-1602	-0190	-0069	+0179	+0225	-0061	+0044	+0178
	2639 †	+0010	-1602	-0093	-0034	+0099	+0104	-0015	+0179	+0165
	2641	+0010	+0198	+0095	+0034	-0057	-0104	-0018	-0126	-0121
	2643	+0020	+0198	+0191	+0069	-0143	-0214	-0030	-0145	-0050
	2644	+0030	+0198	+0286	+0103	-0217	-0333	-0075	+0434	+0076
	2645	+0041	+0198	+0381	+0137	-0246	-0460	-0134	+0537	-0027
W_2	2646	+0051	+0198	+0477	+0172	-0318	-0587	-0239	+0013	-0145
	2647	+0061	+0198	+0573	+0206	-0347	-0714	-0313	+0116	-0250
	2648	+0081	+0197	+0764	+0273	-0372	-0999	-0363	+2611	+1041
	2649	+0101	+0197	+0954	+0341	-0537	-1305	-0650	+3835	+1058
	2650	+0122	+0197	+1147	+0409	-0829	-1634	-0698	+4761	+0952
	2651	+0142	+0197	+1338	+0476	-1192	-1986	-0834	+5518	+1101
	2652	+0163	+0197	+1528	+0542	-1469	-2349	-1077	+6161	+0960
	2653	+0183	+0197	+1720	+0609	-1758	-2737	-1169	+7363	+1013
	2654	+0204	+0197	+1912	+0674	-2121	-3148	-1202	+7989	+0966
	2655	+0224	+0197	+2102	+0739	-2493	-3574	-1384	+8647	+1060
	2656	+0245	+0197	+2294	+0803	-2919	-4031	-1444	+8862	+0720
	2657	+0265	+0197	+2486	+0866	-3321	-4505	-1535	+9879	+0779
	2658	+0286	+0197	+2676	+0929	-3741	-5010	-1778	+9780	+0204
	2659	+0294	+0197	+2752	+0953	-3872	-5216	-1825	+8756	-0508
	2660	+0000	-1715	-0002	-0000	+0144	-0010	-0092	-7655	-2894
	2660	+0017	-1026	-0037	-0165	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 35

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	=0001	-0001	=0002	=0002	=0005	=0004	=0005	=0005	=0005
	2673	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
✓	2662	+0051	-1552	=0460	=0212	+0350	+0552	=0248	+0178	+1351
✓	2663	+0040	-1552	-0367	-0170	+0303	+0440	-0248	+0178	+1368
✓	2664	+0030	-1552	-0275	-0127	+0223	+0320	-0142	+0192	+1364
✓	2665	+0020	-1552	-0184	-0085	+0047	+0210	-0081	+0144	+0928
✓	2666	+0010	-1552	-0091	-0042	-0013	+0105	-0021	+0070	+0672
	2667	+0000	+0253	+0001	+0000	-0072	+0000	=0021	+0030	+0419
	2668	+0010	+0248	+0094	+0043	-0164	-0112	=0036	=0031	+0116
	2669	+0020	+0248	+0184	+0085	-0223	-0217	-0080	-0235	-0804
	2670	+0030	+0248	+0275	+0127	-0375	-0328	-0123	-0306	-1361
	2671	+0041	+0248	+0368	+0170	-0447	-0450	-0167	-0374	-1777
	2672	+0051	+0247	+0460	+0211	-0419	-0554	-0183	+0662	+3242
	2674	+0010	+0248	+0094	+0043	-0101	-0104	-0030	-0052	-0182
	2676	+0020	+0248	+0185	+0086	-0175	-0212	-0024	-0074	-0483
	2677	+0030	+0248	+0275	+0127	-0281	-0324	-0022	-0082	-0533
W_2	2678	+0041	+0248	+0368	+0170	-0368	-0436	-0189	-0053	-0576
	2679	+0051	+0248	+0460	+0212	-0419	-0566	-0247	-0110	-1032
	2680	+0061	+0248	+0552	+0254	-0524	-0695	-0338	-0171	-1368
	2681	+0081	+0247	+0736	+0339	-0586	-0971	-0594	-0210	-1751
	2682	+0101	+0247	+0921	+0422	-0765	-1271	-0776	-0130	-2175
	2683	+0122	+0247	+1105	+0506	-1115	-1593	-0927	-0121	-2322
	2684	+0142	+0247	+1289	+0589	-1529	-1930	-0941	-0049	-2509
	2685	+0162	+0247	+1472	+0672	-1887	-2286	-1078	+0022	-2718
	2686	+0183	+0247	+1657	+0754	-2282	-2648	-1366	-0018	-3277
	2687	+0203	+0247	+1841	+0835	-2746	-3051	-1563	+0093	-2893
	2688	+0224	+0247	+2026	+0915	-3133	-3450	-1714	+1233	+1859
	2689	+0244	+0247	+2209	+0994	-3666	-3876	-1895	+1245	+1272
	2690	+0265	+0247	+2392	+1073	-4171	-4335	-2063	+1277	+1439
	2691	+0285	+0247	+2574	+1150	-4741	-4788	-2256	+1225	+0645
	2692	+0294	+0247	+2646	+1180	-4942	-4981	-2331	+1194	+0180
	2693	+0000	-1658	-0001	-0000	+0074	-0006	+0034	-0297	-1385
	2693	+0010	-1004	-0029	-0161	+0000	+0000	+0000	+0000	+0000

✓ For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 36

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0005	-0005
	2847	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	2842	+0051	-1503	-0441	-0252	+0586	+0525	-0372	+0065	+0394
†	2843	+0041	-1503	-0352	-0201	+0459	+0416	-0268	+0062	+0212
†	2844	+0031	-1502	-0265	-0151	+0382	+0298	-0164	+0085	+0268
†	2845	+0020	-1502	-0177	-0101	+0245	+0196	-0090	+0066	+0251
†	2846	+0010	-1502	-0088	-0051	+0148	+0094	-0045	+0072	+0044
	2848	+0010	+0297	+0087	+0050	-0076	-0095	-0031	+0001	-0136
	2849	+0020	+0297	+0175	+0100	-0171	-0198	-0061	-0013	-0122
	2850	+0030	+0297	+0263	+0150	-0299	-0308	-0151	-0020	-0030
	2851	+0040	+0297	+0349	+0199	-0384	-0418	-0241	+0008	-0062
	2852	+0050	+0297	+0438	+0250	-0451	-0545	-0345	+0075	-0073
	2853	+0061	+0297	+0528	+0301	-0571	-0663	-0495	+0053	+0011
	2854	+0081	+0297	+0704	+0400	-0733	-0933	-0780	+0093	-0031
	2855	+0101	+0297	+0877	+0498	-0919	-1209	-0990	+0269	+0191
	2856	+0121	+0296	+1053	+0597	-1327	-1517	-1169	+0253	-0030
	2857	+0142	+0296	+1231	+0697	-1748	-1848	-1348	+0261	-0396
	2858	+0162	+0296	+1405	+0794	-2202	-2187	-1557	+0276	-0680
	2859	+0183	+0296	+1580	+0891	-2685	-2532	-1737	+0359	-0728
	2860	+0203	+0296	+1757	+0988	-3218	-2910	-1961	+0382	-0815
	2861	+0224	+0296	+1931	+1084	-3732	-3304	-2171	+0443	-0877
	2862	+0244	+0296	+2104	+1177	-4375	-3707	-2455	+0817	+0170
	2863	+0265	+0296	+2279	+1272	-4981	-4130	-2739	+0823	+0214
	2864	+0285	+0296	+2452	+1364	-5595	-4568	-3038	+0944	+0158
	2865	+0293	+0296	+2520	+1400	-5902	-4738	-3138	+1170	+1153
	2866	+0000	-1485	-0004	-0002	+0101	-0002	-0128	-0090	+0853
	2866	+0017	-0976	-0022	-0166	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 37

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0006	-0005
	2206	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
≠	2201	+0051	-1453	-0417	-0288	+0550	+0506	-0359	+1072	+0478
≠	2202	+0040	-1453	-0331	-0229	+0463	+0395	-0269	+1120	+0520
≠	2203	+0030	-1453	-0249	-0172	+0352	+0292	-0165	+0927	+0356
≠	2204	+0020	-1453	-0166	-0115	+0220	+0182	-0090	+0545	+0156
≠	2205	+0010	-1453	-0083	-0058	+0147	+0094	-0030	+0382	+0035
	2207	+0010	+0347	+0084	+0058	-0103	-0095	+0000	+0010	+0018
	2208	+0020	+0359	+0165	+0119	-3471	-0144	-0030	-3787	-3701
	2209	+0030	+0347	+0249	+0172	-0391	-0283	-0120	+0134	+0201
	2210	+0041	+0347	+0334	+0231	-0514	-0393	-0210	+0745	+0316
W_2	2211	+0051	+0347	+0415	+0287	-0600	-0505	-0315	+1101	+0159
	2212	+0061	+0347	+0499	+0344	-0710	-0631	-0450	+1069	+0257
	2213	+0081	+0347	+0665	+0459	-0940	-0877	-0751	+1261	+0021
	2214	+0101	+0346	+0831	+0573	-1311	-1137	-1051	+1971	+0120
	2215	+0121	+0346	+0997	+0687	-1781	-1420	-1246	+2824	-0005
	2216	+0142	+0346	+1164	+0801	-2254	-1736	-1426	+3775	+0214
	2217	+0162	+0347	+1328	+0914	-2842	-2033	-1427	+3330	-6793
	2218	+0183	+0346	+1493	+1026	-3341	-2369	-1923	+4413	-8157
	2219	+0203	+0346	+1658	+1137	-3951	-2721	-2164	+5105	-9748
	2220	+0223	+0346	+1822	+1245	-4538	-3100	-2524	+7488	+0264
	2221	+0244	+0346	+1987	+1355	-5229	-3478	-2840	+8614	+0377
	2222	+0275	+0346	+2232	+1517	-6330	-4083	-3411	+9688	+0551
	2223	+0285	+0346	+2311	+1570	-6755	-4273	-3624	+8742	+0118
	2224	+0293	+0346	+2375	+1612	-6957	-4436	-3822	+7696	-0687

≠ For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 38

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0006	-0005
	2233	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	2228	+0051	-1404	-0390	-0323	+0668	+0469	-0421	-3047	-1205
†	2229	+0040	-1404	-0311	-0257	+0531	+0368	-0302	-3053	-1455
†	2230	+0030	-1404	-0233	-0193	+0397	+0265	-0181	-2562	-1445
†	2231	+0020	-1404	-0155	-0128	+0254	+0170	-0106	-2293	-1144
†	2232	+0010	-1403	-0078	-0064	+0120	+0080	-0030	-0008	-0196
	2234	+0010	+0398	+0077	+0064	-0163	-0079	+0000	-0079	-0040
	2235	+0020	+0397	+0156	+0130	-0306	-0174	-0030	+0223	-0061
	2236	+0030	+0397	+0233	+0193	-0418	-0262	-0121	+0387	-0056
	2237	+0040	+0397	+0311	+0258	-0599	-0365	-0227	-0131	-0281
W_2	2238	+0050	+0397	+0388	+0322	-0746	-0460	-0348	-0207	-0511
	2239	+0061	+0397	+0466	+0386	-0861	-0580	-0499	+0055	-0169
	2240	+0081	+0397	+0621	+0515	-1159	-0803	-0786	+0072	-0414
	2241	+0101	+0396	+0776	+0643	-1591	-1048	-1088	+0766	-0496
	2242	+0121	+0396	+0932	+0770	-2118	-1317	-1315	+1607	-0317
	2243	+0142	+0396	+1087	+0898	-2702	-1609	-1527	+2882	-0379
	2244	+0162	+0396	+1241	+1024	-3257	-1896	-1815	+3714	-0244
	2245	+0182	+0396	+1395	+1150	-3910	-2203	-2103	+4274	-0238
	2246	+0203	+0396	+1548	+1275	-4613	-2535	-2420	+5687	-0100
	2247	+0223	+0396	+1701	+1399	-5305	-2873	-2781	+6633	+0205
	2248	+0243	+0396	+1853	+1523	-6112	-3226	-3204	+7397	+0002
	2249	+0264	+0396	+2004	+1644	-6908	-3589	-3643	+8080	+0167
	2250	+0284	+0396	+2154	+1765	-7822	-3957	-4156	+8727	-0178
	2251	+0292	+0396	+2212	+1813	-8168	-4099	-4368	+7946	-0753

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 39

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0006	-0005
	2261	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	✓ 2256	+0051	-1353	-0360	-0356	+0773	+0435	-0439	-0619	+0068
	✓ 2257	+0040	-1353	-0287	-0283	+0576	+0349	-0303	-0597	-0173
	✓ 2258	+0030	-1353	-0216	-0213	+0442	+0246	-0182	+0413	-0076
	✓ 2259	+0020	-1353	-0143	-0142	+0276	+0167	-0106	-0012	-0117
	✓ 2260	+0010	-1353	-0072	-0072	+0153	+0088	-0045	-0148	-0163
	2262	+0010	+0448	+0071	+0071	-0177	-0071	-0015	-0654	-0250
	2263	+0020	+0447	+0142	+0141	-0327	-0158	-0061	+0080	-0139
	2264	+0030	+0447	+0214	+0212	-0491	-0237	-0137	-0310	-0016
W_2	2265	+0040	+0447	+0287	+0283	-0635	-0332	-0228	+0236	-0096
	2266	+0050	+0447	+0357	+0354	-0833	-0419	-0350	-0049	-0201
	2267	+0060	+0447	+0429	+0424	-1019	-0513	-0502	+0065	-0039
	2268	+0081	+0447	+0572	+0566	-1361	-0728	-0821	+1117	+0131
	2269	+0101	+0446	+0716	+0707	-1896	-0958	-1157	+1710	+0123
	2270	+0121	+0446	+0860	+0849	-2508	-1207	-1415	+0411	-0844
	2271	+0141	+0446	+1001	+0988	-3132	-1468	-1659	+1271	-0945
	2272	+0161	+0446	+1142	+1126	-3769	-1755	-1995	+2663	-0578
	2273	+0182	+0446	+1285	+1267	-4391	-2027	-2286	+3097	-0823
	2274	+0202	+0446	+1426	+1405	-5127	-2335	-2668	+4217	-0591
	2275	+0223	+0446	+1566	+1542	-5939	-2652	-3094	+4911	-0535
	2276	+0243	+0446	+1705	+1679	-6799	-2970	-3570	+5728	-0459
	2277	+0263	+0446	+1843	+1814	-7672	-3311	-4104	+6167	-0688
	2278	+0284	+0446	+1980	+1948	-8646	-3644	-4672	+6246	-0903
	2279	+0292	+0446	+2033	+2001	-8959	-3779	-4916	+6251	-1479

✓ For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 40

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0005	-0005
	2288	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	2282	+0041	-1303	-0264	-0311	+0655	+0299	-0254	+0068	+0129
†	2283	+0051	-1303	-0327	-0386	+0866	+0386	-0438	+0030	+0185
†	2284	+0040	-1303	-0260	-0306	+0708	+0299	-0302	+0003	-0020
†	2285	+0030	-1303	-0195	-0230	+0497	+0229	-0197	+0009	+0092
†	2286	+0020	-1303	-0130	-0154	+0378	+0149	-0106	+0040	+0124
†	2287	+0010	-1303	-0065	-0077	+0173	+0071	-0030	+0027	+0047
	2289	+0010	+0497	+0065	+0077	-0137	-0063	+0000	+0028	+0007
	2290	+0020	+0497	+0130	+0154	-0296	-0143	-0030	+0058	+0158
	2291	+0030	+0497	+0195	+0230	-0448	-0220	-0121	+0191	+0964
	2292	+0040	+0497	+0261	+0308	-0658	-0299	-0151	+0126	+0295
	2293	+0050	+0497	+0326	+0384	-0807	-0380	-0336	+0069	+0162
W_2	2294	+0071	+0497	+0456	+0537	-1257	-0563	-0610	+0247	+0860
	2295	+0081	+0497	+0522	+0614	-1566	-0656	-0807	+0260	+0811
	2296	+0101	+0496	+0651	+0767	-2128	-0853	-1111	+0353	+1166
	2297	+0121	+0496	+0781	+0919	-2751	-1091	-1385	+0371	+0676
	2298	+0141	+0496	+0910	+1072	-3398	-1327	-1400	+0472	+0780
	2299	+0162	+0496	+1039	+1223	-4092	-1573	-1985	+0572	+1086
	2300	+0182	+0496	+1168	+1375	-4869	-1856	-2023	+0749	+1367
	2301	+0202	+0496	+1295	+1525	-5642	-2125	-2793	+0769	+1283
	2302	+0222	+0496	+1422	+1675	-6517	-2418	-3281	+0914	+1295
	2303	+0243	+0496	+1547	+1824	-7438	-2715	-3813	+0960	+1339
	2304	+0263	+0495	+1672	+1971	-8373	-3017	-4385	+0994	+1219
	2305	+0284	+0495	+1795	+2118	-9344	-3330	-4976	+1070	+1198
	2306	+0292	+0495	+1843	+2176	-9712	-3446	-5234	+1061	+1058
	2306	+0289	+0430	+2070	+1926	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 41

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0005
	2315	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
✓	2310	+0051	-1253	-0292	-0412	+0090	+0341	-0469	-0211	-0001
✓	2311	+0040	-1253	-0252	-0328	+0071	+0272	-0333	+0097	+0080
✓	2312	+0030	-1253	-0174	-0245	+0054	+0201	-0213	+0134	-0126
✓	2313	+0020	-1253	-0116	-0164	+0041	+0131	-0138	+0529	+0025
✓	2314	+0010	-1252	-0058	-0082	+0021	+0062	-0061	+0461	-0097
	2316	+0010	+0548	+0059	+0083	-0022	-0053	+0016	-0107	-0142
	2317	+0020	+0547	+0117	+0165	-0034	-0124	-0029	+0017	-0142
	2318	+0031	+0547	+0181	+0255	-0054	-0200	-0118	-0545	-0298
	2319	+0040	+0547	+0233	+0329	-0075	-0260	-0192	-0293	-0369
	2320	+0050	+0547	+0290	+0410	-0094	-0330	-0236	+0326	+0004
	2321	+0060	+0547	+0347	+0491	-0120	-0414	-0460	+0573	-0049
W_2	2322	+0081	+0547	+0464	+0657	-0179	-0567	-0549	+1032	+0192
	2323	+0101	+0547	+0581	+0821	-0247	-0752	-1014	+1932	+0211
	2324	+0121	+0547	+0697	+0985	-0319	-0943	-1300	+2851	+0146
	2325	+0141	+0547	+0811	+1147	-0394	-1151	-1615	+3212	+0262
	2326	+0161	+0546	+0926	+1310	-0469	-1384	-1960	+4488	+0571
	2327	+0182	+0546	+1039	+1472	-0549	-1635	-1975	+4296	-0160
	2328	+0202	+0546	+1153	+1634	-0638	-1083	-2894	+5108	+0064
	2329	+0222	+0546	+1266	+1795	-0730	-2151	-3418	+6340	-0051
	2330	+0243	+0546	+1378	+1956	-0825	-2421	-3973	+6892	-0041
	2331	+0263	+0546	+1488	+2116	-0920	-2704	-4601	+7084	-0239
	2332	+0283	+0546	+1597	+2273	-1019	-2986	-5272	+6883	-0501
	2333	+0290	+0545	+1635	+2329	-1053	-3092	-5431	+6021	-1242
	2334	+0000	-1402	-0002	-0001	+0012	-0012	+0050	-5723	-3926
	2334	+0010	-1055	-0042	-0152	+0000	+0000	+0000	+0000	+0000

✓ For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 42

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0005
	2341	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	2336	+0050	-1203	-0254	-0436	+0097	+0288	-0354	-0374	-0167
†	2337	+0040	-1203	-0202	-0346	+0078	+0235	-0293	-0169	-0136
†	2338	+0030	-1203	-0152	-0260	+0059	+0171	-0185	-0290	-0173
†	2339	+0020	-1203	-0101	-0173	+0037	+0109	-0093	-0221	-0310
†	2340	+0010	-1203	-0051	-0087	+0015	+0055	-0031	-0295	-0262
	2342	+0010	+0598	+0051	+0088	-0019	-0055	+0000	-0352	-0251
	2343	+0020	+0598	+0102	+0174	-0037	-0110	+0001	-0264	-0102
	2344	+0030	+0598	+0151	+0260	-0059	-0164	-0059	-0373	-0258
	2345	+0040	+0598	+0202	+0346	-0082	-0227	-0167	-0617	-0248
W_2	2346	+0050	+0598	+0253	+0434	-0105	-0281	-0243	-0355	-0222
	2347	+0060	+0597	+0303	+0520	-0133	-0349	-0304	+0694	+0147
	2348	+0081	+0597	+0405	+0695	-0197	-0490	-0627	+0901	+0072
	2349	+0101	+0597	+0506	+0869	-0279	-0635	-0918	+1652	+0249
	2350	+0121	+0597	+0605	+1040	-0355	-0816	-1196	+1996	+0400
	2351	+0141	+0597	+0707	+1215	-0440	-0987	-1366	+2740	+0481
	2352	+0161	+0597	+0806	+1388	-0523	-1199	-1949	+3724	+0505
	2353	+0181	+0597	+0905	+1558	-0597	-1415	-2320	+6487	+1298
	2354	+0202	+0596	+1003	+1730	-0685	-1643	-2830	+6353	+1059
	2355	+0222	+0596	+1101	+1901	-0778	-1889	-3386	+7299	+1155
	2356	+0242	+0596	+1198	+2073	-0872	-2141	-3989	+7648	+0842
	2357	+0262	+0596	+1294	+2242	-0973	-2401	-4592	+8368	+0582
	2358	+0283	+0596	+1388	+2411	-1072	-2668	-5256	+8561	+0631
	2359	+0290	+0596	+1421	+2470	-1108	-2753	-5487	+8249	+0407
	2360	+0001	+0576	+0005	+0008	+0022	+0001	+0101	+2491	+1188
	2360	+0015	-1036	-0034	-0141	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 43

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	2367	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	2362	+0050	-1152	-0215	-0456	+0108	+0248	-0338	+0053	+0360
†	2363	+0040	-1152	-0170	-0362	+0089	+0194	-0262	+0077	+0579
†	2364	+0030	-1152	-0128	-0273	+0066	+0148	-0154	+0058	+0498
†	2365	+0020	-1152	-0085	-0182	+0043	+0093	-0093	+0067	+0469
†	2366	+0010	-1152	-0043	-0091	+0020	+0047	-0015	-0019	+0050
	2368	+0010	+0648	+0043	+0091	-0016	-0047	+0015	-0045	-0025
	2369	+0020	+0648	+0086	+0183	-0039	-0093	+0001	-0096	-0446
	2370	+0030	+0648	+0128	+0273	-0059	-0140	-0045	-0140	-0652
	2371	+0040	+0648	+0171	+0364	-0085	-0194	-0119	-0207	-0943
W_2	2372	+0050	+0648	+0214	+0454	-0107	-0234	-0196	+0104	+0566
	2373	+0060	+0648	+0257	+0546	-0140	-0294	-0271	+0194	+0933
	2374	+0080	+0648	+0342	+0727	-0211	-0400	-0530	+0236	+0808
	2375	+0101	+0648	+0427	+0909	-0295	-0528	-0789	+0253	+0876
	2376	+0121	+0647	+0512	+1091	-0392	-0671	-0985	+0319	+0952
	2377	+0141	+0647	+0597	+1271	-0475	-0816	-1382	+0918	+3756
	2378	+0161	+0647	+0681	+1452	-0566	-0992	-1794	+1001	+3718
	2379	+0181	+0647	+0765	+1633	-0656	-1178	-2313	+1111	+4049
	2380	+0201	+0647	+0848	+1814	-0749	-1388	-2818	+1235	+4175
	2381	+0222	+0646	+0931	+1994	-0840	-1607	-3383	+1386	+4673
	2382	+0242	+0646	+1012	+2174	-0941	-1831	-3962	+1538	+4867
	2383	+0262	+0646	+1093	+2353	-1041	-2081	-4588	+1677	+5050
	2384	+0283	+0646	+1172	+2531	-1143	-2322	-5245	+1724	+5010
	2385	+0290	+0646	+1200	+2592	-1174	-2416	-5474	+1707	+5131
	2386	+0001	+0593	+0005	+0008	+0012	+0013	+0040	+0881	+4363
	2386	+0015	-1031	-0033	-0143	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 44

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	2393	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	2388	+0050	-1102	-0174	-0473	+0105	+0201	-0293	+0037	+0161
†	2389	+0040	-1102	-0138	-0377	+0081	+0156	-0235	+0049	+0059
†	2390	+0030	-1102	-0104	-0283	+0063	+0119	-0177	+0018	+0026
	0050	+0003	+0003	+0500	+0500	+ 250	+ 1	- 175	- 175	- 175
	0050	+0003	+0003	+0500	+0500	+ 1	+ 1	- 175	- 175	- 175
	2394	+0010	+0698	+0035	+0094	-0020	-0037	+0000	+0033	-0051
	2395	+0020	+0698	+0069	+0188	-0040	-0074	-0015	+0003	+0055
	2396	+0030	+0698	+0104	+0282	-0061	-0111	-0075	+0001	-0030
	2397	+0040	+0698	+0138	+0377	-0088	-0155	-0119	-0025	-0190
	2398	+0050	+0698	+0173	+0471	-0118	-0183	-0193	-0081	-0497
	2399	+0060	+0698	+0207	+0566	-0153	-0227	-0237	-0102	-0508
W_2	2400	+0080	+0698	+0276	+0754	-0226	-0321	-0489	-0109	-0638
	2401	+0101	+0698	+0345	+0943	-0310	-0422	-0695	-0074	-0698
	2402	+0121	+0698	+0415	+1132	-0414	-0529	-0902	+0430	+1586
	2403	+0141	+0698	+0482	+1320	-0514	-0635	-1271	+0460	+1632
	2404	+0161	+0698	+0551	+1508	-0612	-0782	-1640	+0582	+1867
	2405	+0181	+0697	+0618	+1696	-0706	-0945	-2144	+0714	+2387
	2406	+0201	+0697	+0686	+1884	-0802	-1124	-2646	+0817	+2415
	2407	+0222	+0697	+0752	+2071	-0903	-1326	-3207	+0935	+2685
	2408	+0242	+0697	+0819	+2259	-1003	-1526	-3705	+0768	+1657
	2409	+0262	+0696	+0884	+2445	-1100	-1738	-4349	+1085	+2967
	2410	+0282	+0696	+0948	+2631	-1209	-1965	-4961	+1147	+2907
	2411	+0289	+0696	+0970	+2698	-1246	-2046	-5152	+1016	+2247
	2412	+0000	-0971	-0000	-0002	+0013	+0004	-0032	+0475	+2231
	2412	+0016	-1045	-0039	-0152	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 45

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0005
	2420	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	2415	+0051	-1051	-0132	-0488	+0111	+0156	-0286	+0962	+0732
†	2416	+0040	-1051	-0106	-0390	+0088	+0120	-0211	+1087	+0721
†	2417	+0030	-1051	-0079	-0293	+0063	+0092	-0152	+0740	+0550
†	2418	+0020	-1052	-0053	-0196	+0040	+0065	-0075	+0389	+0230
†	2419	+0010	-1052	-0027	-0100	+0017	+0028	-0015	-0023	-0047
	2421	+0010	+0749	+0026	+0097	-0021	-0020	+0031	-0503	-0306
	2422	+0020	+0749	+0053	+0195	-0040	-0056	+0032	-0326	-0281
	2423	+0030	+0749	+0079	+0291	-0064	-0084	+0018	-0656	-0447
	2424	+0050	+0749	+0131	+0483	-0116	-0139	-0098	-0637	-0470
	2425	+0060	+0749	+0157	+0581	-0152	-0164	-0156	-0918	-0528
	2426	+0080	+0749	+0209	+0775	-0232	-0230	-0300	-0931	-0571
W_2	2427	+0101	+0749	+0261	+0970	-0329	-0312	-0476	-0329	-0557
	2428	+0121	+0748	+0313	+1164	-0437	-0393	-0681	+0528	-0315
	2429	+0141	+0748	+0365	+1358	-0545	-0474	-1004	+0886	-0172
	2430	+0161	+0748	+0416	+1551	-0659	-0579	-1357	+1704	-0092
	2431	+0181	+0748	+0467	+1746	-0762	-0708	-1752	+2474	-0094
	2432	+0201	+0748	+0518	+1939	-0868	-0845	-2163	+3118	+0215
	2433	+0222	+0748	+0569	+2134	-0971	-1015	-2648	+4843	+0569
	2434	+0242	+0747	+0618	+2325	-1067	-1177	-3090	+6095	+0805
	2435	+0262	+0747	+0668	+2519	-1174	-1353	-3516	+6915	+0920
	2436	+0272	+0747	+0692	+2614	-1223	-1442	-3737	+7200	+1009
	0050	+0003	+0003	+0500	+0500	+0339	+0339	+4521	+8477	+4521
	0050	-0000	+0747	+0692	+2614	+0339	+0339	+4521	+8477	+4521

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 46

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0005
	2446	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	2441	+0051	-1001	-0088	-0499	+0127	+0083	-0187	+1279	+0351
†	2442	+0040	-1001	-0070	-0394	+0093	+0072	-0143	+0578	+0129
†	2443	+0030	-1001	-0053	-0297	+0064	+0053	-0100	+0338	-0082
†	2444	+0020	-1001	-0035	-0195	+0046	+0040	-0057	+0098	+0003
†	2445	+0010	-1000	-0017	-0099	+0026	+0012	-0014	+0237	-0050
	2447	+0010	+0799	+0018	+0100	-0021	-0020	+0014	+0218	+0059
	2448	+0020	+0799	+0035	+0196	-0042	-0040	+0029	+0177	-0010
	2449	+0030	+0799	+0053	+0297	-0063	-0061	+0014	-0190	-0094
	2450	+0040	+0799	+0070	+0395	-0093	-0072	-0029	-0216	+0032
	2451	+0050	+0799	+0088	+0496	-0117	-0099	-0058	+0136	+0051
	2452	+0061	+0799	+0106	+0597	-0154	-0111	-0101	+0113	+0146
W_2	2453	+0081	+0799	+0141	+0795	-0242	-0161	-0187	+0431	+0259
	2454	+0101	+0799	+0175	+0990	-0338	-0203	-0216	+0342	+0386
	2455	+0121	+0799	+0210	+1188	-0450	-0244	-0491	+0386	+0309
	2456	+0141	+0799	+0244	+1385	-0572	-0292	-0708	+1520	+0502
	2457	+0161	+0799	+0279	+1584	-0693	-0363	-0925	+1924	+0860
	2458	+0181	+0799	+0314	+1785	-0807	-0450	-1243	+3365	+1116
	2459	+0201	+0798	+0348	+1980	-0913	-0557	-1548	+5363	+1872
	2460	+0221	+0798	+0381	+2178	-1023	-0655	-1856	+5301	+2113
	2461	+0241	+0798	+0415	+2373	-1126	-0775	-2159	+6383	+2499
	2462	+0262	+0798	+0448	+2574	-1230	-0896	-2494	+7232	+2641
	2463	+0282	+0798	+0480	+2768	-1333	-1025	-2784	+7620	+2793
	2464	+0290	+0798	+0493	+2847	-1375	-1077	-2887	+8193	+2894
	2465	+0001	-0959	-0001	-0007	+0017	-0008	+0041	+3857	+1752
	2465	+0016	-1045	-0039	-0150	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 47

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0005	-0005	-0006	-0005
	2472	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	2467	+0052	-0950	-0045	-0514	+0126	+0431	-0150	+0173	-0165
†	2468	+0040	-0950	-0035	-0401	+0095	+0336	-0136	+0206	-0016
†	2469	+0030	-0951	-0026	-0299	+0069	+0296	-0105	+0024	-0008
†	2470	+0020	-0951	-0017	-0196	+0043	+0256	-0075	-0159	+0001
†	2471	+0010	-0950	-0009	-0100	+0023	+0051	-0029	+0380	-0088
	2473	+0010	+0849	+0009	+0100	-0018	-0127	+0000	+0053	-0086
	2474	+0020	+0850	+0018	+0201	-0042	-0176	+0015	-0027	-0168
	2475	+0030	+0849	+0026	+0300	-0064	-0308	+0029	-0220	-0071
	2476	+0040	+0850	+0035	+0400	-0090	-0253	+0045	-0335	-0184
	2477	+0050	+0850	+0044	+0501	-0124	-0457	+0031	+0154	-0134
	2478	+0060	+0850	+0053	+0601	-0154	-0573	+0001	+0128	-0003
W_2	2479	+0081	+0850	+0071	+0803	-0242	-0776	-0012	+0175	+0029
	2480	+0101	+0850	+0088	+1002	-0338	-0972	-0056	+0511	+0321
	2481	+0121	+0850	+0106	+1206	-0464	-1129	-0129	+0832	+0448
	2482	+0141	+0850	+0123	+1403	-0583	-1382	-0276	+1825	+0544
	2483	+0161	+0850	+0140	+1604	-0712	-1465	-0408	+2048	+0696
	2484	+0181	+0849	+0157	+1802	-0828	-1959	-0540	+2966	+0985
	2485	+0201	+0849	+0174	+2006	-0945	-2376	-0643	+3733	+1445
	2486	+0221	+0849	+0191	+2204	-1053	-2689	-0805	+4519	+1869
	2487	+0242	+0849	+0208	+2407	-1161	-3490	-0966	+4625	+2031
	2488	+0262	+0849	+0224	+2606	-1262	-4025	-1025	+4677	+1989
	2489	+0282	+0849	+0241	+2808	-1361	-4645	-1158	+5669	+2491
	2490	+0290	+0849	+0247	+2884	-1398	-4961	-1320	+6249	+2744
	2493	+0000	+0654	+0000	+0001	+0016	-0066	+0067	+2332	+0970
	2493	+0015	-1044	-0036	-0142	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 48

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0006	-0006	-0006	-0005
	2500	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
✓	2495	+0050	-0900	+0000	-0500	+0123	+0033	+0591	+0641	+0318
✓	2496	+0040	-0900	-0000	-0396	+0091	+0472	-0738	+0275	+0112
✓	2497	+0030	-0900	-0000	-0299	+0067	+0752	-0591	+0042	+0199
✓	2498	+0020	-0900	-0000	-0197	+0047	+0197	-0296	+0012	+0165
✓	2499	+0010	-0900	-0000	-0097	+0023	+0497	-0147	+0081	+0082
	2501	+0010	+0900	-0000	+0102	-0020	+0209	+0294	+0153	+0145
	2502	+0020	+0900	-0000	+0202	-0040	+0463	+0442	-0063	+0098
	2503	+0030	+0900	-0000	+0301	-0068	+0025	+0592	-0195	-0030
	2504	+0041	+0900	-0000	+0405	-0096	+0364	+0593	-0478	+0009
	2505	+0050	+0900	-0000	+0502	-0124	+0775	+0890	-0528	+0003
W_2	2506	+0060	+0900	-0000	+0603	-0160	+0408	+1037	-0388	-0085
	2507	+0080	+0900	-0000	+0803	-0244	+0697	+1025	-0496	+0050
	2508	+0101	+0900	-0000	+1008	-0343	+0263	+1174	-0127	+0221
	2509	+0121	+0900	-0000	+1207	-0459	+0866	+1620	+0494	+0525
	2510	+0141	+0900	-0000	+1409	-0586	+0786	+2364	+0883	+0574
	2511	+0161	+0900	-0000	+1608	-0711	+2193	+2664	+1694	+1025
	2512	+0181	+0900	-0000	+1809	-0836	+3642	+2811	+2131	+1282
	2513	+0201	+0900	-0000	+2013	-0956	+4175	+3557	+2539	+1473
	2514	+0221	+0900	-0000	+2213	-1066	+5304	+3843	+2320	+1807
	2515	+0241	+0900	-0000	+2413	-1161	+6243	+4116	+2592	+2142
	2516	+0261	+0900	-0001	+2614	-1263	+7094	+4253	+2682	+2203
	2517	+0282	+0900	-0000	+2815	-1362	+6249	+4390	+3557	+2660
	2521	+0001	-0903	-0000	-0006	+0024	+0093	-0095	-0240	+0581

✓ For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 49

Note:- For wing W_3 the orientation of the model is such that at $\lambda = 30^\circ$ one wing is in the -z plane.

Configuration / Exponent	Serial No.	σ°	$\lambda + 90^\circ$	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0006	-0006	-0006	-0005
	3505	+0000	+0900	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3500	-0050	+0900	+0000	-0507	+0559	-0910	-0463	+1589	+0318
	3501	-0040	+0900	+0000	-0405	+0435	-0419	-0463	+1354	+0233
	3502	-0030	+0900	+0000	-0305	+0326	-0593	-0464	+1146	+0203
	3503	-0020	+0900	+0000	-0202	+0207	-0621	-0159	+0803	+0056
	3504	-0010	+0900	+0000	-0101	+0102	-0113	+0000	+0204	-0055
	3506	+0010	+0900	-0000	+0101	-0098	+0425	+0306	-0536	-0198
	3507	+0020	+0900	-0000	+0202	-0192	+0881	+0307	+0169	-0084
	3508	+0030	+0900	-0000	+0302	-0284	+0790	+0774	+0161	-0024
	3509	+0040	+0900	-0000	+0404	-0379	+1224	+0922	-0072	-0061
	3510	+0050	+0900	-0000	+0504	-0468	+0776	+1083	-0054	-0027
	3511	+0060	+0900	-0000	+0607	-0563	+1245	+1084	+0317	+0076
	3512	+0080	+0900	-0000	+0808	-0766	+1380	+1554	+0978	-0047
W_3	3513	+0100	+0900	-0000	+1010	-0964	+1352	+2001	+0839	+0101
	3514	+0120	+0900	-0000	+1214	-1185	+1296	+2151	+1099	+0119
	3515	+0140	+0900	-0000	+1415	-1418	+1357	+2759	+0615	-0123
	3516	+0160	+0900	-0000	+1619	-1657	+1451	+3355	+0440	-0233
	3517	+0180	+0900	-0000	+1821	-1910	+0974	+3653	-0089	-0531
	3518	+0190	+0900	-0000	+1923	-2039	+1341	+4251	-0495	-0683
	3519	+0200	+0900	-0000	+2025	-2181	+1144	+3953	-0607	-0705
	3520	+0210	+0900	-0000	+2127	-2317	+0832	+3808	-1266	-0959
	3521	+0220	+0900	-0000	+2229	-2470	+0283	+5301	-1658	-1176
	3522	+0230	+0900	-0000	+2329	-2615	+0443	+5753	-2138	-1327
	3523	+0240	+0900	-0000	+2432	-2762	+0595	+4847	-1593	-1159
	3524	+0250	+0900	-0000	+2534	-2921	+0864	+6032	-1829	-1076
	3525	+0260	+0900	-0000	+2635	-3093	+0805	+6168	-2304	-1077
	3526	+0270	+0900	-0000	+2738	-3268	+0736	+6162	-2439	-1069
	3528	+0280	+0900	-0000	+2840	-3435	+0790	+5937	-1973	-1004
	3529	+0288	+0900	-0000	+2923	-3560	+0479	+5915	-1594	-0965
	3530	-0000	+0900	+0000	-0001	+0007	-0528	+0538	-0047	+0539

Table 50

Configuration / Exponent	Serial No.	σ°	$\lambda+90^\circ$	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0005	-0005	-0006	-0006
	3537	+0000	+0950	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3532	-0050	+0950	+0044	-0505	+0561	-0372	-0032	+1290	+4789
	3533	-0040	+0950	+0035	-0404	+0434	-0274	-0047	+1192	+3360
	3534	-0030	+0950	+0027	-0303	+0321	-0250	-0031	+0886	+4509
	3535	-0020	+0950	+0018	-0202	+0210	-0190	-0031	+1161	+4318
	3536	-0010	+0950	+0009	-0101	+0103	-0058	+0000	+0370	+3111
	3538	+0010	+0950	-0009	+0101	-0090	+0125	+0016	+0180	+2747
	3539	+0020	+0950	-0018	+0200	-0184	+0257	+0033	+0291	+3372
	3540	+0030	+0950	-0027	+0302	-0275	+0380	+0049	-0135	-0122
	3541	+0040	+0950	-0035	+0403	-0376	+0520	+0081	-0091	+1415
	3542	+0050	+0950	-0044	+0504	-0475	+0656	+0082	-0314	+0109
	3543	+0060	+0950	-0053	+0603	-0557	+0769	+0099	+0304	+3882
	3544	+0080	+0950	-0071	+0805	-0752	+1090	+0129	+0353	+3416
W_3	3545	+0100	+0950	-0088	+1007	-0958	+1433	+0235	+0500	+1338
	3546	+0120	+0950	-0106	+1208	-1175	+1863	+0309	+0434	+3329
	3547	+0140	+0950	-0124	+1411	-1413	+2428	+0474	+0664	+0943
	3548	+0160	+0950	-0141	+1613	-1647	+2995	+0637	+0522	-0031
	3549	+0180	+0950	-0159	+1814	-1899	+3693	+0874	+0036	-0490
	3550	+0190	+0950	-0167	+1915	-2020	+3998	+0992	-0249	-1166
	3551	+0200	+0950	-0176	+2017	-2159	+4403	+1066	-0549	-1926
	3552	+0210	+0950	-0185	+2118	-2296	+4696	+1215	-1010	-3124
	3553	+0220	+0950	-0193	+2219	-2434	+5023	+1422	-1496	-5502
	3554	+0230	+0950	-0201	+2320	-2588	+5404	+1703	-1533	-5824
	3555	+0240	+0950	-0210	+2422	-2734	+5861	+1703	-2026	-7659
	3556	+0250	+0950	-0219	+2524	-2889	+6284	+1941	-2493	-8211
	3557	+0260	+0950	-0227	+2625	-3051	+6755	+2015	-2442	-7935
	3558	+0270	+0950	-0236	+2725	-3210	+7345	+2060	-3318	-9301
	3560	+0280	+0950	-0244	+2828	-3378	+7823	+2152	-2933	-7411
	3560	+0288	+0950	-0251	+2911	-3520	+8310	+2183	-3420	-6859
	3561	+0000	+0950	+0000	-0000	+0019	-0039	+0125	-0023	+2042

Table 51

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda+90°$	$\alpha°$	$\beta°$	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0005
	3568	+0000	+1000	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3564	-0050	+1000	+0087	-0498	+0557	-0071	-0047	-3391	-2111
	3564	-0040	+1000	+0070	-0398	+0428	-0057	-0032	-3547	-1928
	3565	-0030	+1000	+0052	-0298	+0300	-0049	-0030	-3509	-2159
	3566	-0020	+1000	+0035	-0198	+0189	-0035	-0030	-4021	-2330
	3567	-0010	+1000	+0017	-0099	+0087	-0013	-0015	+0838	+0165
	3569	+0010	+1000	-0018	+0100	-0088	+0023	+0000	-0229	-0263
	3570	+0020	+1000	-0035	+0200	-0179	+0041	+0016	-0597	-0323
	3571	+0030	+1000	-0053	+0299	-0270	+0067	+0032	-1184	-0573
	3572	+0040	+1000	-0071	+0399	-0366	+0091	+0032	-1809	-0758
	3573	+0050	+1000	-0089	+0499	-0464	+0115	+0046	-4582	-2109
	3574	+0060	+1000	-0106	+0598	-0571	+0140	+0077	-4745	-2271
	3575	+0080	+1000	-0141	+0797	-0758	+0203	+0151	-4436	-2288
W_3	3576	+0100	+1000	-0176	+0997	-0952	+0267	+0269	-3665	-1952
	3577	+0120	+1000	-0211	+1196	-1163	+0351	+0400	-3881	-2112
	3578	+0140	+1000	-0247	+1396	-1393	+0454	+0620	-3767	-1867
	3579	+0160	+1000	-0282	+1596	-1624	+0571	+0898	-4886	-2052
	3580	+0180	+1000	-0316	+1794	-1863	+0702	+1263	-4821	-2336
	3581	+0190	+1000	-0334	+1895	-2002	+0771	+1467	-4869	-2457
	3582	+0200	+1000	-0351	+1994	-2126	+0842	+1686	-5612	-2660
	3583	+0210	+1000	-0368	+2095	-2260	+0909	+1921	-5596	-2718
	3584	+0220	+1000	-0385	+2196	-2400	+0982	+2227	-6734	-2863
	3585	+0230	+1000	-0402	+2295	-2543	+1061	+2477	-6062	-2815
	3586	+0240	+1000	-0419	+2393	-2684	+1146	+2550	-6510	-2680
	3588	+0250	+1000	-0436	+2493	-2835	+1228	+2828	-7001	-2631
	3588	+0260	+1000	-0453	+2594	-2993	+1323	+2979	-7776	-2949
	3590	+0270	+1000	-0470	+2693	-3130	+1420	+3097	-8277	-3169
	3590	+0280	+1000	-0486	+2794	-3278	+1521	+3262	-8773	-3364
	3591	+0288	+1000	-0500	+2876	-3396	+1600	+3338	-8344	-3349
	3592	+0000	+1000	-0001	+0001	+0006	+0000	+0026	-4538	-2310

Table 52

Configuration / Exponent	Serial No.	σ°	$\lambda+90^\circ$	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0005
	3599	+0000	+1050	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3594	-0050	+1050	+0130	-0488	+0537	-0096	+0107	+3119	+0968
	3595	-0040	+1050	+0104	-0390	+0415	-0081	+0016	+2244	+0583
	3596	-0030	+1050	+0079	-0293	+0305	-0068	+0016	+1801	+0291
	3597	-0020	+1050	+0052	-0194	+0182	-0041	+0001	+0897	+0007
	3598	-0010	+1050	+0026	-0098	+0086	-0022	+0001	+0794	-0104
	3600	+0010	+1050	-0026	+0099	-0088	+0026	+0000	-0287	-0090
	3601	+0020	+1050	-0053	+0196	-0180	+0057	+0016	-0367	-0204
	3602	+0030	+1050	-0079	+0293	-0261	+0093	+0016	-0993	-0291
	3603	+0040	+1050	-0105	+0391	-0366	+0133	+0016	-1421	-0566
	3604	+0050	+1050	-0131	+0488	-0447	+0166	+0016	-1460	-0566
	3605	+0060	+1050	-0158	+0586	-0553	+0211	+0060	-1385	-0700
	3606	+0080	+1050	-0210	+0781	-0741	+0297	+0147	-1833	-0672
W_3	3607	+0100	+1050	-0263	+0978	-0934	+0404	+0266	-0078	-0105
	3608	+0120	+1050	-0315	+1173	-1140	+0522	+0441	-0260	-0285
	3609	+0140	+1050	-0367	+1368	-1360	+0671	+0691	-0257	-0284
	3610	+0160	+1050	-0419	+1563	-1578	+0834	+1014	-0190	-0373
	3611	+0180	+1050	-0471	+1759	-1818	+1017	+1442	-0426	-0372
	3612	+0190	+1050	-0497	+1857	-1934	+1114	+1647	-0817	-0502
	3613	+0200	+1050	-0522	+1954	-2053	+1212	+1898	-2217	-0512
	3614	+0210	+1050	-0548	+2052	-2183	+1315	+2181	-1495	-0569
	3616	+0220	+1050	-0573	+2148	-2320	+1418	+2432	-1543	-0742
	3616	+0230	+1050	-0598	+2246	-2452	+1543	+2685	-1122	-0759
	3618	+0240	+1050	-0624	+2343	-2576	+1669	+2877	-1969	-0863
	3618	+0250	+1050	-0650	+2442	-2716	+1805	+3128	-3842	-0994
	3620	+0260	+1050	-0675	+2540	-2851	+1947	+3249	-3192	-1390
	3620	+0270	+1050	-0699	+2636	-2984	+2090	+3441	-4211	-1296
	3622	+0280	+1050	-0725	+2734	-3113	+2240	+3637	-4695	-1816
	3622	+0288	+1050	-0745	+2815	-3229	+2369	+3761	-5287	-1922
	3623	+0000	+1050	+0000	-0000	+0013	+0001	-0098	+1574	-0043

Table 55

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda+90°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0005
	3630	+0000	+1100	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3625	-0050	+1100	+0172	-0475	+0526	-0133	-0049	+0906	+0033
	3626	-0040	+1100	+0138	-0381	+0423	-0111	-0033	+0866	+0086
	3627	-0030	+1100	+0104	-0285	+0315	-0089	-0033	+0795	+0262
	3628	-0020	+1100	+0069	-0189	+0203	-0060	-0017	-0542	-0273
	3629	-0010	+1100	+0035	-0095	+0104	-0030	-0017	+0510	+0094
	3631	+0010	+1100	-0035	+0096	-0088	+0036	+0001	-0463	-0231
	3632	+0020	+1100	-0070	+0191	-0165	+0069	+0001	-0680	-0273
	3633	+0030	+1100	-0104	+0285	-0253	+0114	+0018	-0156	-0093
	3634	+0040	+1100	-0139	+0381	-0351	+0168	+0034	-0796	-0116
	3635	+0050	+1100	-0174	+0476	-0443	+0217	+0051	-3282	-1497
	3636	+0060	+1100	-0208	+0570	-0523	+0274	+0068	-0347	-0007
	3637	+0080	+1100	-0277	+0760	-0715	+0380	+0161	+0149	+0045
W_3	3638	+0100	+1100	-0347	+0950	-0912	+0519	+0315	-0794	-0275
	3639	+0120	+1100	-0415	+1139	-1111	+0683	+0515	-0504	-0192
	3640	+0140	+1100	-0484	+1329	-1316	+0855	+0791	-0752	-0308
	3641	+0160	+1100	-0553	+1519	-1533	+1062	+1127	-0871	-0210
	3642	+0180	+1100	-0622	+1709	-1771	+1287	+1527	-1201	-0462
	3643	+0190	+1100	-0655	+1803	-1883	+1399	+1773	-1840	-0708
	3644	+0200	+1100	-0689	+1898	-2002	+1529	+2003	-1609	-0371
	3645	+0210	+1100	-0723	+1992	-2125	+1659	+2264	-2043	-0708
	3646	+0220	+1100	-0757	+2087	-2237	+1796	+2417	-2252	-0809
	3647	+0230	+1100	-0790	+2182	-2358	+1942	+2585	-3034	-0652
	3648	+0240	+1100	-0824	+2275	-2500	+2100	+2816	-4014	-1268
	3649	+0250	+1100	-0857	+2370	-2618	+2264	+2971	-4010	-1525
	3650	+0260	+1100	-0890	+2465	-2735	+2428	+3018	-4317	-1623
	3652	+0270	+1100	-0923	+2557	-2854	+2599	+3218	-5026	-1972
	3652	+0280	+1100	-0956	+2652	-2985	+2783	+3314	-6179	-2193
	3653	+0288	+1100	-0983	+2730	-3085	+2937	+3438	-7167	-2301
	3654	+0000	+1100	-0000	+0001	+0023	-0003	+0048	-0764	-0570

Table 54

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda+90°$	$\alpha°$	$\beta°$	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0005
	3661	+0000	+1150	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3656	-0050	+1150	+0213	-0458	+0501	-0155	-0045	+2617	+1006
	3657	-0040	+1150	+0170	-0366	+0383	-0129	-0045	+1811	+0617
	3658	-0030	+1150	+0128	-0274	+0279	-0105	-0015	+1493	+0389
	3659	-0020	+1150	+0085	-0183	+0177	-0070	-0015	+0875	+0289
	3660	-0010	+1150	+0042	-0091	+0090	-0037	-0015	+0772	+0374
	3662	+0010	+1150	-0042	+0092	-0084	+0058	+0015	+9683	+4797
	3663	+0020	+1150	-0085	+0182	-0164	+0105	+0015	+9601	+4783
	3664	+0030	+1150	-0129	+0275	-0256	+0154	+0015	+4627	+2403
	3665	+0040	+1150	-0171	+0367	-0344	+0211	+0015	+4535	+2421
	3666	+0050	+1150	-0214	+0459	-0436	+0275	+0031	+3970	+2271
	3667	+0060	+1150	-0257	+0550	-0525	+0339	+0045	+4278	+2417
	3668	+0080	+1150	-0343	+0734	-0706	+0483	+0130	+4088	+2327
W_3	3669	+0100	+1150	-0429	+0917	-0891	+0647	+0315	+4612	+2641
	3670	+0120	+1150	-0514	+1099	-1086	+0841	+0500	+4234	+2501
	3671	+0140	+1150	-0599	+1282	-1291	+1060	+0770	+3864	+2273
	3672	+0160	+1150	-0685	+1465	-1505	+1298	+1126	+3695	+2483
	3674	+0180	+1150	-0769	+1647	-1730	+1554	+1482	+3360	+2421
	3674	+0190	+1150	-0811	+1739	-1844	+1694	+1697	+3231	+2303
	3676	+0200	+1150	-0853	+1830	-1967	+1844	+1912	+2825	+2088
	3676	+0210	+1150	-0895	+1921	-2073	+1993	+2068	+2844	+2043
	3678	+0220	+1150	-0937	+2012	-2188	+2151	+2197	+2296	+2058
	3678	+0230	+1150	-0979	+2102	-2305	+2322	+2353	+1669	+1841
	3680	+0240	+1150	-1020	+2192	-2423	+2494	+2512	+1500	+1867
	3680	+0260	+1150	-1103	+2375	-2677	+2873	+2712	+0281	+1251
	3682	+0280	+1150	-1184	+2554	-2917	+3256	+2886	-1191	+0939
	3682	+0288	+1150	-1217	+2628	-3025	+3418	+3047	-2275	+0716
	3683	+0000	+1150	-0000	+0000	+0006	+0010	-0003	+4020	+2121

Table 55

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda+90°$	$\alpha°$	$\beta°$	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0005
	3690	+0000	+1200	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3685	-0050	+1200	+0252	-0439	+0488	-0196	-0032	+1106	+0216
	3686	-0040	+1200	+0202	-0351	+0384	-0167	-0032	+1255	+0266
	3687	-0030	+1200	+0151	-0263	+0277	-0126	-0032	+0791	+0287
	3688	-0020	+1200	+0102	-0176	+0182	-0086	+0000	+0754	+0263
	3689	-0010	+1200	+0051	-0089	+0091	-0047	+0000	+0754	+0118
	3691	+0010	+1200	-0051	+0088	-0086	+0051	+0016	-0215	-0100
	3692	+0020	+1200	-0101	+0175	-0163	+0107	+0016	-0043	-0020
	3693	+0030	+1200	-0151	+0262	-0239	+0168	+0016	-0067	-0006
	3694	+0040	+1200	-0202	+0349	-0316	+0233	+0016	+0453	+0325
	3695	+0050	+1200	-0253	+0437	-0412	+0304	+0032	+0043	+0297
	3696	+0060	+1200	-0304	+0525	-0499	+0386	+0032	-0175	+0384
	3697	+0080	+1200	-0406	+0700	-0684	+0551	+0121	-0681	+0327
W_3	3698	+0100	+1200	-0507	+0875	-0852	+0745	+0269	-0494	+0253
	3699	+0120	+1200	-0608	+1050	-1048	+0974	+0460	-0542	+0129
	3700	+0140	+1200	-0709	+1223	-1251	+1218	+0757	-0930	-0006
	3701	+0160	+1200	-0810	+1398	-1465	+1480	+1095	-1148	+0225
	3702	+0180	+1200	-0909	+1571	-1675	+1768	+1434	-1514	+0399
	3703	+0190	+1200	-0959	+1659	-1785	+1923	+1581	-1565	-0008
	3704	+0200	+1200	-1009	+1745	-1904	+2087	+1713	-2131	+0008
	3705	+0210	+1200	-1058	+1831	-2014	+2247	+1831	-0836	+0306
	3706	+0220	+1200	-1108	+1917	-2127	+2426	+1964	-1410	+0042
	3707	+0230	+1200	-1157	+2004	-2241	+2608	+2068	-2019	-0405
	3708	+0240	+1200	-1206	+2089	-2358	+2795	+2187	-3414	-0376
	3710	+0250	+1200	-1255	+2176	-2481	+2992	+2261	-4795	-0772
	3710	+0260	+1200	-1303	+2261	-2603	+3184	+2394	-5445	-0833
	3712	+0270	+1200	-1352	+2347	-2724	+3394	+2425	-5940	-1299
	3712	+0280	+1200	-1400	+2433	-2864	+3598	+2573	-6847	-1658
	3713	+0288	+1200	-1439	+2502	-2962	+3766	+2647	-7016	-1330
	3714	+0000	+1200	+0000	-0000	+0009	+0001	-0013	+0365	+0547

Table 112

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0006	-0004	-0006	-0005	-0005
	4901	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4892	-0040	+0000	-0406	+0000	-0841	+0600	+0404	+0404	-1145
	4892	+0000	+0000	+0001	+0000	-1847	+0027	+0404	-0347	-1565
	4893	+0040	+0000	+0406	+0001	-2672	-0554	+1012	-0983	-1314
$W_4\ B\ C^R$	4894	+0080	+0000	+0814	+0001	-3182	-1256	+1618	-1790	-1625
	4895	+0120	+0000	+1222	+0001	-4201	-2080	+2377	-2868	-1886
$\xi_{-z} = 0$	4896	+0160	+0000	+1632	+0001	-2427	-3012	+3438	-3868	-1492
	4897	+0200	+0000	+2042	+0001	-8404	-4067	+4352	-5038	-1455
	4898	+0240	+0000	+2455	+0001	-6712	-5258	+6931	-6527	-1800
	4900	+0280	+0000	+2868	+0002	-9501	-6586	+9361	-8368	-2848
	4900	-0000	+0000	-0002	+0001	-2299	+0020	-0304	-0652	-2381
	4900	-0000	+0000	-0062	+0047	+0000	+0000	+0000	+0000	+0000

Table 113

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	4919	+0000	+0150	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4909	-0040	+0150	-0391	-0105	+0131	+0583	-0083	+0785	-0225
	4910	+0000	+0150	+0001	+0000	-0004	+0025	-0054	+0076	+0128
	4911	+0040	+0150	+0393	+0105	-0142	-0535	+0033	-0560	+1171
$W_4\ B\ C^R$	4912	+0080	+0150	+0786	+0210	-0288	-1204	+0106	-1445	+1135
	4913	+0120	+0150	+1181	+0314	-0451	-1997	+0457	-2431	+1221
$\xi_{-z} = 0^\circ$	4914	+0160	+0150	+1575	+0417	-0682	-2858	+1090	-3428	+1802
	4916	+0200	+0150	+1971	+0519	-0978	-3823	+2262	-4351	+3021
	4916	+0240	+0150	+2366	+0619	-1325	-4865	+3668	-5434	+4740
	4918	+0280	+0150	+2761	+0717	-1749	-5965	+4901	-6543	+6897
	4918	+0000	+0150	-0000	+0000	-0008	+0022	-0184	-0211	-0824
	4918	+0000	+0150	-0054	+0038	+0000	+0000	+0000	+0000	+0000

Table 57

W_3

Configuration \ Exponent	Serial No.	σ°	$\lambda + 90^\circ$	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0068	-0068	-0069	-0070	-0069
	3756	+0000	+1300	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3751	-0050	+1300	+0324	-0388	+0405	-0265	+0000	+1585	+0277
	3752	-0040	+1300	+0260	-0310	+0313	-0214	+0000	+0734	+0152
	3753	-0030	+1300	+0195	-0232	+0229	-0163	+0000	+0888	+0093
	3754	-0020	+1300	+0130	-0155	+0137	-0112	+0000	+0606	-0069
	3755	-0010	+1300	+0065	-0077	+0069	-0056	+0000	+0472	+0211
	3757	+0010	+1300	-0065	+0077	-0071	+0056	+0016	-0136	-0050
	3758	+0020	+1300	-0130	+0155	-0142	+0136	+0001	+0177	+0228
	3759	+0030	+1300	-0195	+0232	-0220	+0209	+0001	-0130	+0226
	3760	+0040	+1300	-0260	+0310	-0299	+0290	-0014	+0049	+0233
	3761	+0050	+1300	-0326	+0387	-0383	+0389	+0002	-0588	-0181
	3762	+0060	+1300	-0390	+0464	-0461	+0469	+0002	-0375	+0007
	3763	+0080	+1300	-0521	+0619	-0633	+0688	+0047	-0384	+0075
	3764	+0100	+1300	-0652	+0774	-0801	+0922	+0195	-0635	+0074
	3765	+0120	+1300	-0782	+0928	-0976	+1180	+0357	-0772	-0115
	3766	+0140	+1300	-0912	+1082	-1180	+1481	+0593	-1470	-0121
	3767	+0160	+1300	-1041	+1234	-1392	+1783	+0829	-1828	-0147
	3768	+0180	+1300	-1171	+1388	-1598	+2108	+1021	-2345	-0291
	3769	+0190	+1300	-1234	+1463	-1710	+2279	+1095	-2740	-0552
	3770	+0200	+1300	-1298	+1540	-1824	+2467	+1183	-3474	-0654
	3771	+0210	+1300	-1363	+1616	-1929	+2653	+1257	-3842	-1016
	3772	+0220	+1300	-1427	+1692	-2043	+2841	+1345	-4308	-0986
	3774	+0230	+1300	-1490	+1766	-2157	+3037	+1419	-4660	-1139
	3774	+0240	+1300	-1554	+1842	-2282	+3251	+1478	-5184	-1576
	3776	+0250	+1300	-1617	+1917	-2408	+3456	+1553	-5822	-1682
	3776	+0260	+1300	-1680	+1992	-2532	+3670	+1641	-6948	-1777
	3778	+0270	+1300	-1742	+2066	-2650	+3888	+1715	-7657	-2041
	3778	+0280	+1300	-1805	+2141	-2775	+4109	+1759	-7694	-1989
	3780	+0288	+1300	-1856	+2201	-2882	+4282	+1790	-8668	-2387
	3780	+0000	+1300	-0000	+0000	-0006	+0000	-0062	-2371	-0726

Table 58

Configuration \ Exponent	Serial No.	σ°	$\lambda+90^\circ$	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0068	-0068	-0069	-0070	-0069
	3787	+0000	+1350	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3782	-0050	+1350	+0356	-0357	+0368	-0305	+0018	+1657	+0236
	3783	-0040	+1350	+0286	-0286	+0286	-0240	+0002	+1206	+0053
	3784	-0030	+1350	+0215	-0215	+0212	-0176	+0016	+0889	+0144
	3785	-0020	+1350	+0144	-0144	+0135	-0119	+0016	+0689	+0033
	3786	-0010	+1350	+0071	-0071	+0069	-0063	+0000	+0253	-0148
	3788	+0010	+1350	-0072	+0071	-0062	+0070	+0000	-0039	+0060
	3790	+0020	+1350	-0143	+0143	-0132	+0142	+0000	+0158	+0039
	3790	+0030	+1350	-0215	+0215	-0209	+0230	-0016	-0083	-0065
	3792	+0040	+1350	-0286	+0286	-0281	+0318	-0016	-0328	+0013
	3792	+0050	+1350	-0357	+0357	-0362	+0416	-0016	-0188	+0010
	3794	+0060	+1350	-0430	+0429	-0442	+0513	-0016	-0048	+0008
	3794	+0080	+1350	-0573	+0572	-0598	+0737	+0043	-0244	-0003
W_3	3796	+0100	+1350	-0717	+0714	-0757	+0985	+0146	-0027	+0292
	3796	+0120	+1350	-0860	+0856	-0944	+1277	+0294	-0640	+0156
	3798	+0140	+1350	-1003	+0998	-1143	+1581	+0450	-0958	+0170
	3798	+0160	+1350	-1146	+1140	-1348	+1910	+0615	-1767	+0014
	3800	+0180	+1350	-1289	+1280	-1554	+2252	+0733	-2522	-0071
	3800	+0200	+1350	-1430	+1420	-1771	+2619	+0835	-3068	-0490
	3802	+0220	+1350	-1571	+1559	-2000	+3011	+0968	-3938	-0870
	3802	+0240	+1350	-1711	+1697	-2239	+3420	+1072	-4947	-1356
	3804	+0260	+1350	-1851	+1834	-2502	+3862	+1207	-7435	-1779
	3804	+0280	+1350	-1990	+1971	-2752	+4299	+1295	-8301	-1998
	3806	+0288	+1350	-2046	+2027	-2857	+4480	+1310	-8690	-2477
	3806	-0000	+1350	+0000	-0001	+0015	+0003	-0141	-1931	-0313
	3806	-0000	+1350	+0013	-0133	+0000	+0000	+0000	+0000	+0000

Table 59

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda+90°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0006	-0005
	3813	+0000	+1400	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3808	-0050	+1400	+0385	-0324	+0334	-0337	-0136	+1161	+0243
	3809	-0040	+1400	+0310	-0260	+0271	-0274	-0136	+0595	+0110
	3810	-0030	+1400	+0232	-0195	+0196	-0208	-0149	+0203	-0163
	3811	-0020	+1400	+0154	-0129	+0133	-0137	-0149	-0515	-0126
	3812	-0010	+1400	+0077	-0065	+0071	-0074	+0000	-0365	-0052
	3814	+0010	+1400	-0078	+0066	-0056	+0079	+0000	-0503	-0052
	3816	+0020	+1400	-0155	+0130	-0110	+0149	+0000	-0101	+0111
	3816	+0030	+1400	-0233	+0195	-0176	+0245	-0149	-0402	-0035
	3818	+0040	+1400	-0311	+0261	-0249	+0342	-0149	-0500	+0043
	3818	+0050	+1400	-0388	+0325	-0323	+0439	-0149	-0292	-0049
	3820	+0060	+1400	-0466	+0390	-0404	+0537	-0149	-0761	-0196
	3820	+0080	+1400	-0621	+0520	-0556	+0780	+0000	-1000	-0192
W_3	3822	+0100	+1400	-0776	+0649	-0717	+1039	+0746	-0666	-0080
	3822	+0120	+1400	-0933	+0779	-0899	+1341	+1343	-0797	-0188
	3824	+0140	+1400	-1088	+0908	-1098	+1659	+2682	-1673	-0079
	3824	+0160	+1400	-1242	+1036	-1299	+1994	+3576	-1605	-0136
	3826	+0180	+1400	-1397	+1163	-1511	+2355	+4470	-2578	-0512
	3826	+0190	+1400	-1474	+1227	-1615	+2526	+4768	-2127	-0305
	3828	+0200	+1400	-1551	+1290	-1721	+2731	+5353	-3109	-0310
	3828	+0210	+1400	-1627	+1353	-1844	+2921	+5799	-3648	-0682
	3830	+0220	+1400	-1704	+1416	-1960	+3127	+6246	-4087	-0792
	3830	+0230	+1400	-1781	+1479	-2069	+3332	+6395	-5176	-1199
	3832	+0240	+1400	-1858	+1542	-2200	+3538	+7134	-5848	-1669
	3832	+0250	+1400	-1933	+1603	-2319	+3760	+7432	-6734	-1681
	3834	+0260	+1400	-2009	+1665	-2444	+3976	+7730	-6957	-1812
	3834	+0270	+1400	-2084	+1727	-2577	+4205	+7872	-7653	-2058
	3836	+0280	+1400	-2160	+1788	-2704	+4429	+8021	-8406	-2697
	3836	+0288	+1400	-2222	+1839	-2810	+4620	+8170	-9051	-2585
	3838	+0000	+1400	-0000	+0000	+0010	-0006	-1141	-4712	-1799

Table 60

W_3

Exponent / Configuration	Serial No.	σ°	$\lambda + 90^\circ$	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0006	-0005
	3844	+0000	+1450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3839	-0050	+1450	+0413	-0289	+0291	-0370	+0297	+1630	+0329
	3840	-0040	+1450	+0331	-0232	+0227	-0291	+0148	+0658	-0008
	3842	-0030	+1450	+0248	-0174	+0173	-0221	+0148	+0346	-0049
	3842	-0020	+1450	+0165	-0116	+0117	-0142	+0148	+0185	-0089
	3844	-0010	+1450	+0083	-0058	+0056	-0078	+0000	+0500	+0052
	3845	+0010	+1450	-0084	+0058	-0047	+0077	+0000	+0505	+0013
	3846	+0020	+1450	-0167	+0117	-0112	+0169	+0000	-1425	-0615
	3847	+0030	+1450	-0249	+0174	-0168	+0260	+0000	+0165	+0131
	3848	+0040	+1450	-0333	+0233	-0235	+0352	+0000	-2290	-1070
	3849	+0050	+1450	-0416	+0291	-0302	+0464	+0000	-3001	-1417
	3850	+0060	+1450	-0498	+0348	-0377	+0567	+0000	-3756	-1736
	3851	+0080	+1450	-0664	+0464	-0517	+0812	+0000	+0282	+0097
	3852	+0100	+1450	-0831	+0580	-0695	+1089	+0148	-0333	-0197
	3853	+0120	+1450	-0997	+0695	-0859	+1378	+0444	-0309	-0065
	3854	+0140	+1450	-1163	+0810	-1059	+1711	+0890	-0916	-0151
	3855	+0160	+1450	-1329	+0924	-1253	+2054	+1039	-1273	-0149
	3856	+0180	+1450	-1494	+1038	-1463	+2413	+1484	-1869	-0337
	3857	+0200	+1450	-1660	+1151	-1692	+2790	+2523	-2333	-0519
	3858	+0210	+1450	-1742	+1207	-1808	+2995	+3116	-2806	-0807
	3859	+0220	+1450	-1826	+1264	-1924	+3200	+3265	-3547	-0751
	3860	+0230	+1450	-1907	+1319	-2039	+3410	+3410	-3902	-1225
	3862	+0240	+1450	-1989	+1374	-2156	+3623	+3410	-4898	-1061
	3862	+0250	+1450	-2070	+1429	-2271	+3834	+3407	-5051	-1284
	3864	+0260	+1450	-2153	+1485	-2406	+4066	+3556	-6728	-1865
	3864	+0270	+1450	-2234	+1539	-2531	+4302	+3556	-4637	-0702
	3866	+0280	+1450	-2316	+1594	-2665	+4524	+3704	-6560	-1476
	3866	+0288	+1450	-2382	+1638	-2776	+4712	+3716	-8585	-2540
	3867	+0000	+1450	-0000	+0000	+0009	-0001	-0679	-1973	-0619
	3867	+0000	+1450	+0015	-0131	+0000	+0000	+0000	+0000	+0000

Table 61

Configuration \ Exponent	Serial No.	σ°	$\lambda+90^\circ$	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0007	-0005	-0005
	3880	+0000	+1500	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3876	-0050	+1500	+0438	-0252	+0232	-0399	+2613	+0072	+0204
	3876	-0040	+1500	+0351	-0202	+0182	-0312	-0372	-0065	-0339
	3878	-0030	+1500	+0263	-0152	+0141	-0242	+1249	+0025	+0123
	3878	-0020	+1500	+0176	-0102	+0090	-0155	+1364	+0020	+0082
	3880	-0010	+1500	+0087	-0050	+0042	-0077	+1364	-0024	-0060
	3881	+0010	+1500	-0088	+0051	-0051	+0079	+1621	-0020	-0039
	3882	+0020	+1500	-0174	+0101	-0102	+0165	+1736	+0009	-0069
	3883	+0030	+1500	-0262	+0151	-0153	+0276	+1736	-0016	-0101
	3884	+0040	+1500	-0351	+0202	-0220	+0365	+3357	-0010	-0009
	3885	+0050	+1500	-0437	+0253	-0290	+0470	+3471	-0039	-0246
	3886	+0060	+1500	-0525	+0303	-0351	+0588	+3576	-0062	-0400
	3887	+0080	+1500	-0702	+0405	-0495	+0840	+2203	-0093	-0410
W_3	3888	+0100	+1500	-0878	+0506	-0653	+1114	+2327	-0131	-0644
	3889	+0120	+1500	-1055	+0607	-0840	+1416	-1974	-0139	-0705
	3890	+0140	+1500	-1229	+0706	-1023	+1740	-1850	-0189	-1001
	3891	+0160	+1500	-1405	+0806	-1219	+2089	-1850	-0200	-0911
	3892	+0180	+1500	-1581	+0906	-1430	+2449	-0257	-0281	-1143
	3893	+0190	+1500	-1670	+0956	-1537	+2634	-1602	-0340	-1319
	3894	+0200	+1500	-1757	+1004	-1651	+2836	-1602	-0357	-1777
	3895	+0210	+1500	-1844	+1053	-1765	+3030	-3071	-0448	-1904
	3896	+0220	+1500	-1931	+1102	-1900	+3225	+0105	-0519	-2019
	3897	+0230	+1500	-2018	+1150	-2017	+3438	-1364	-0622	-2991
	3898	+0240	+1500	-2104	+1198	-2137	+3651	-1249	-0751	-3470
	3900	+0250	+1500	-2193	+1247	-2264	+3873	-2708	-0928	-3973
	3900	+0260	+1500	-2280	+1295	-2396	+4096	-1001	-1089	-4584
	3901	+0270	+1500	-2366	+1342	-2517	+4335	-1001	-0233	-0169
	3902	+0280	+1500	-2453	+1389	-2650	+4559	+2165	-0420	-0907
	3903	+0288	+1500	-2523	+1427	-2756	+4752	+2289	-0672	-2016
	3904	-0000	+1500	+0001	-0000	+0010	-0008	+4759	-0274	-1869

Table 62

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5053	+0000	+0300	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5043	-0040	+0300	-0351	-0202	+0226	+0414	-0022	+0390	-0189
	5044	+0000	+0300	+0000	+0000	+0018	+0027	+0020	-0113	-0042
	5045	+0040	+0300	+0351	+0203	-0239	-0409	+0091	-0522	+0146
W_3 B C^R	5046	+0080	+0300	+0703	+0405	-0553	-0963	+0165	-1050	+0280
	5048	+0120	+0300	+1057	+0608	-0969	-1673	+0298	-1778	+0513
$\xi_{-z} = 0^\circ$	5048	+0160	+0300	+1409	+0808	-1449	-2502	+0459	-2580	+0792
	5050	+0200	+0300	+1759	+1006	-1976	-3412	+0620	-3546	+1075
	5050	+0240	+0300	+2111	+1202	-2560	-4424	+0812	-4759	+1387
	5052	+0280	+0300	+2458	+1392	-3197	-5527	+1018	-6122	+1748
	5052	+0000	+0300	+0000	+0001	+0024	+0001	-0072	-0823	-0342
	5052	+0000	+0300	+0042	-0175	+0000	+0000	+0000	+0000	+0000

Table 63

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	5064	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5054	-0040	+0450	-0286	-0286	+0343	+0323	-0231	+0165	-0300
	5055	+0000	+0450	+0000	+0001	+0001	+0025	+0342	-0295	-0122
	5056	+0040	+0450	+0286	+0286	-0310	-0340	+1651	-0678	+0089
W_3 B C^R	5058	+0080	+0450	+0574	+0573	-0713	-0826	+1798	-1107	+0302
	5058	+0120	+0450	+0861	+0858	-1132	-1475	-0401	-1799	+0538
$\xi_{-z} = 0^\circ$	5060	+0160	+0450	+1149	+1142	-1617	-2242	-2892	-2573	+0798
	5060	+0200	+0450	+1434	+1423	-2138	-3128	-4211	-3610	+1055
	5062	+0240	+0450	+1716	+1702	-2712	-4096	-5092	-4601	+1404
	5062	+0280	+0450	+1994	+1975	-3327	-5175	-5080	-5907	+1713
	5063	+0000	+0450	+0000	+0001	+0000	+0017	-0206	-0501	-0204
	5063	+0000	+0450	+0042	-0171	+0000	+0000	+0000	+0000	+0000

Table 64

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5077	+0000	+0600	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5068	-0040	+0600	-0202	-0351	+0421	+0238	-0011	+0296	-0169
	5068	+0000	+0600	-0000	-0000	-0003	+0043	+0065	+0002	+0076
	5070	+0040	+0600	+0203	+0352	-0405	-0213	+0201	-0317	+0308
W_3 B C^R	5070	+0080	+0600	+0406	+0703	-0845	-0585	+0217	-0682	+0557
	5072	+0120	+0600	+0608	+1052	-1306	-1061	-0027	-1138	+0826
$\xi_{-z} = 0^\circ$	5072	+0160	+0600	+0810	+1401	-1817	-1677	-0650	-1654	+1134
	5073	+0200	+0600	+1010	+1748	-2351	-2422	-1350	-2359	+1440
	5074	+0240	+0600	+1208	+2093	-2913	-3289	-1758	-3384	+1703
	5075	+0280	+0600	+1402	+2436	-3508	-4258	-1924	-4469	+2004
	5076	+0000	+0600	-0001	+0000	+0005	+0034	+0090	-0310	-0068
	5076	+0000	+0600	+0042	-0166	+0000	+0000	+0000	+0000	+0000

Table 65

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5088	+0000	+0750	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5078	-0040	+0750	-0104	-0391	+0494	+0125	-0053	+0313	-0168
	5079	+0000	+0750	+0000	+0002	+0002	+0031	+0036	+0210	+0126
	5080	+0040	+0750	+0105	+0391	-0429	-0103	+0153	+0056	+0406
W_3 B C^R	5082	+0080	+0750	+0210	+0783	-0899	-0295	+0138	-0275	+0619
	5082	+0120	+0750	+0315	+1174	-1406	-0547	-0055	-0461	+0974
$\xi_{-z} = 0^\circ$	5084	+0160	+0750	+0419	+1566	-1988	-0895	-0635	-0753	+1315
	5084	+0200	+0750	+0522	+1956	-2576	-1330	-1512	-1125	+1703
	5086	+0240	+0750	+0625	+2348	-3227	-1868	-2525	-1683	+2084
	5086	+0280	+0750	+0725	+2739	-3927	-2555	-3214	-2363	+2527
	5087	+0000	+0750	-0000	-0000	+0009	+0027	-0050	+0001	+0043
	5088	+0000	+0750	+0042	-0161	+0000	+0000	+0000	+0000	+0000

Table 66

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0006	-0006	-0006	-0004
	5099	+0000	+0900	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5090	-0040	+0900	-0000	-0406	+0521	+2993	+0095	+2614	-0126
	5090	+0000	+0900	-0000	+0001	+0009	+3449	+0664	+2192	+0174
	5091	+0040	+0900	-0000	+0406	-0449	+4785	+1505	+1651	+0421
W_3 B C^R	5092	+0080	+0900	-0001	+0811	-0926	+5679	+2216	+0968	+0689
	5093	+0120	+0900	-0000	+1217	-1451	+5358	+3350	+1700	+1081
$\xi_{-z} = 0^\circ$	5094	+0160	+0900	-0001	+1622	-2062	+6707	+4629	+1241	+1519
	5095	+0200	+0900	-0001	+2031	-2745	+6787	+6471	+0363	+2010
	5096	+0240	+0900	-0001	+2439	-3481	+6507	+7323	-0571	+2528
	5098	+0280	+0900	-0001	+2848	-4346	+7446	+9311	+1309	+3205
	5098	+0000	+0900	-0000	+0001	-0003	+3271	+0234	+2213	+0191
	5098	+0000	+0900	+0058	-0157	+0000	+0000	+0000	+0000	+0000

Table 67

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5110	+0000	+1050	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5100	-0040	+1050	+0104	-0392	+0514	-0054	-0025	-0107	-0185
	5101	+0000	+1050	-0001	+0001	+0021	+0033	+0004	-0115	+0060
	5102	+0040	+1050	-0106	+0392	-0405	+0188	+0031	-0036	+0295
W_3 B C^R	5103	+0080	+1050	-0211	+0783	-0878	+0388	+0232	+0067	+0555
	5104	+0120	+1050	-0316	+1175	-1392	+0658	+0587	+0287	+0871
$\xi_{-z} = 0^\circ$	5106	+0160	+1050	-0421	+1567	-1961	+1025	+1340	+0505	+1250
	5106	+0200	+1050	-0525	+1957	-2538	+1476	+2363	+0981	+1655
	5107	+0240	+1050	-0628	+2349	-3175	+2033	+3501	+1524	+2038
	5108	+0280	+1050	-0729	+2740	-3862	+2730	+4505	+2187	+2467
	5109	+0000	+1050	-0001	-0000	+0025	+0035	-0089	-0302	-0035
	5109	+0000	+1050	+0063	-0154	+0000	+0000	+0000	+0000	+0000

Table 68

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5131	+0000	+1200	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5111	-0040	+1200	+0201	-0352	+0467	-0156	+0008	-0420	-0265
	5112	+0000	+1200	-0001	-0000	+0026	+0027	+0021	-0221	-0020
	5113	+0040	+1200	-0204	+0351	-0369	+0315	+0035	+0045	+0194
W_3 B C^R	5114	+0080	+1200	-0408	+0702	-0817	+0684	+0201	+0287	+0456
	5116	+0120	+1200	-0611	+1053	-1277	+1180	+0617	+0677	+0735
$\xi_{-z} = 0^\circ$	5116	+0160	+1200	-0814	+1402	-1773	+1782	+1302	+1390	+1058
	5118	+0200	+1200	-1014	+1749	-2305	+2526	+2039	+2118	+1332
	5118	+0240	+1200	-1213	+2095	-2871	+3388	+2585	+2947	+1627
	5120	+0280	+1200	-1408	+2439	-3478	+4358	+3013	+3897	+1954
	5130	+0000	+1200	-0001	+0001	+0034	+0030	-0060	-0375	-0083
	5130	+0000	+1200	+0063	-0150	+0000	+0000	+0000	+0000	+0000

Table 69

	5143	+0000	+1350	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5132	-0040	+1350	+0285	-0287	+0386	-0261	-0053	-0638	-0269
	5133	+0000	+1350	-0001	+0000	+0044	+0019	-0040	-0301	-0042
	5134	+0040	+1350	-0288	+0286	-0280	+0406	-0040	+0101	+0159
	5135	+0080	+1350	-0576	+0573	-0677	+0890	+0048	+0481	+0393
W_3 B C^R	5136	+0120	+1350	-0864	+0859	-1105	+1541	+0355	+1068	+0602
	5137	+0160	+1350	-1150	+1142	-1591	+2314	+0750	+1841	+0835
$\xi_{-z} = 0^\circ$	5138	+0200	+1350	-1434	+1422	-2109	+3179	+1028	+2734	+1111
	5139	+0240	+1350	-1717	+1701	-2667	+4146	+1217	+3724	+1370
	5140	+0240	+1350	-1717	+1701	-2671	+4144	+1234	+3711	+1352
	5141	+0280	+1350	-1996	+1975	-3301	+5218	+1456	+4719	+1706
	5142	+0000	+1350	-0001	+0000	+0049	+0022	-0106	-0508	-0114

Table 70

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	5154	+0000	+1500	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5144	-0040	+1500	+0350	-0203	+0266	-0353	+0014	-0646	-0228
	5145	+0000	+1500	-0000	-0000	+0033	+0017	-0130	-0245	-0112
	5146	+0040	+1500	-0351	+0202	-0213	+0451	+0014	+0289	+0056
W_3 B C^R	5147	+0080	+1500	-0704	+0405	-0533	+1001	-0273	+0723	+0162
	5148	+0120	+1500	-1056	+0607	-0958	+1707	-0846	+1438	+0414
$\xi_{-z} = 0^\circ$	5149	+0160	+1500	-1409	+0808	-1430	+2516	-1132	+2316	+0697
	5150	+0200	+1500	-1761	+1006	-1963	+3427	-1265	+3156	+0973
	5151	+0240	+1500	-2113	+1202	-2565	+4439	-1539	+4142	+1249
	5152	+0280	+1500	-2462	+1394	-3209	+5538	-1372	+5197	+1572
	5153	+0000	+1500	-0000	-0000	+0047	+0016	-1029	-0271	-0165
	5154	+0000	+1500	+0065	-0139	+0000	+0000	+0000	+0000	+0000

Table 71

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5165	+0000	+1650	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5156	-0040	+1650	+0390	-0105	+0152	-0412	+0032	-0305	-0004
	5156	+0000	+1650	-0000	-0001	+0052	+0017	+0016	+0111	+0075
	5158	+0040	+1650	-0393	+0105	-0109	+0483	+0030	+0504	+0070
W_3 B C^R	5158	+0080	+1650	-0785	+0211	-0344	+1061	-0086	+0878	+0034
	5160	+0120	+1650	-1179	+0317	-0689	+1759	-0463	+1385	+0161
$\xi_{-z} = 0^\circ$	5160	+0160	+1650	-1572	+0422	-1119	+2543	-0927	+2155	+0387
	5161	+0200	+1650	-1967	+0526	-1626	+3422	-1275	+3042	+0682
	5162	+0240	+1650	-2363	+0629	-2203	+4395	-1548	+3952	+0972
	5163	+0280	+1650	-2758	+0730	-2840	+5469	-1721	+4983	+1304
	5164	+0000	+1650	-0002	+0000	+0054	+0015	-0078	-0498	-0244
	5164	+0000	+1650	+0061	-0128	+0000	+0000	+0000	+0000	+0000

Table 72

W_3 B C^R

$\xi_{-z} = 0°$

Exponent / Configuration	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	5176	+0000	+1800	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5166	-0040	+1800	+0405	+0000	-0006	-0463	+0091	-0612	-0730
	5167	+0000	+1800	-0002	-0000	+0034	+0004	+0033	-0164	-1190
	5168	+0040	+1800	-0405	+0000	-0003	+0472	+0062	+0363	-0931
	5169	+0080	+1800	-0813	+0001	-0095	+1033	-0109	+0912	-1018
	5170	+0120	+1800	-1220	+0004	-0287	+1679	-0493	+1508	-0523
	5171	+0160	+1800	-1628	+0007	-0568	+2419	-1318	+2355	+0904
	5172	+0200	+1800	-2036	+0011	-0941	+3239	-2131	+3226	+3382
	5173	+0240	+1800	-2447	+0016	-1426	+4162	-2771	+4091	+5558
	5174	+0280	+1800	-2858	+0022	-1970	+5162	-3097	+5086	+8284
	5175	+0000	+1800	-0001	+0000	+0034	+0000	-0032	-0478	-2731
	5176	+0000	+1800	+0060	-0119	+0000	+0000	+0000	+0000	+0000

Table 73

W_3 B C^R

$\xi_{-z} = 0°$

0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0005	-0005
5187	+0000	+1950	+0000	+0000	+0000	+0000	+0000	+0000	+0000
5177	-0040	+1950	+0390	+0104	-1119	-0441	+0049	-0370	+1410
5178	+0000	+1950	-0001	-0001	+0406	+0015	+0006	+0119	+0305
5179	+0040	+1950	-0392	-0105	+1483	+0462	+0035	+0564	-0785
5180	+0080	+1950	-0784	-0209	+2065	+0954	-0151	+1027	-1332
5181	+0120	+1950	-1175	-0311	+2424	+1523	-0508	+1664	-2127
5182	+0160	+1950	-1569	-0412	+2241	+2191	-1264	+2482	-2559
5183	+0200	+1950	-1961	-0509	+1478	+2911	-2335	+3287	-2397
5184	+0240	+1950	-2355	-0604	+0006	+3739	-3448	+4184	-1798
5185	+0280	+1950	-2749	-0695	-2600	+4671	-4259	+5301	-0510
5186	+0000	+1950	-0001	-0001	+0474	+0015	-0058	+0095	+0217
5186	+0000	+1950	+0059	-0110	+0000	+0000	+0000	+0000	+0000

Table 74

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	5198	+0000	+2100	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5188	-0040	+2100	+0352	+0202	-0217	-0408	+0656	-0032	+0286
	5189	+0000	+2100	-0001	-0001	+0037	+0016	+0084	+0380	+0128
	5190	+0040	+2100	-0351	-0204	+0273	+0403	-0202	+0887	-0002
W_3 B C^R	5191	+0080	+2100	-0701	-0405	+0514	+0806	-0631	+1197	-0167
	5192	+0120	+2100	-1052	-0606	+0790	+1258	-1204	+1848	-0345
$\xi_{-z} = 0^\circ$	5193	+0160	+2100	-1400	-0804	+1097	+1775	-1204	+2502	-0553
	5194	+0200	+2100	-1748	-1001	+1445	+2333	-0917	+3273	-0801
	5195	+0240	+2100	-2094	-1194	+1826	+2958	-1775	+4145	-1032
	5196	+0280	+2100	-2439	-1383	+2245	+3673	-2062	+5322	-1208
	5197	+0000	+2100	-0001	-0001	+0038	+0027	-0773	+0544	+0215
	5197	+0000	+2100	+0057	-0101	+0000	+0000	+0000	+0000	+0000

Table 75

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	5209	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5199	+0040	-1499	-0348	-0202	+0333	+0366	+7233	+0448	-0488
	5200	+0000	+0089	+0002	+0000	+0102	-0011	+6321	-0006	-0270
	5201	+0041	+0299	+0354	+0203	-0175	-0437	+6021	-0387	-0035
W_3 B C^R	5202	+0081	+0300	+0704	+0405	-0500	-0993	+6158	-0909	+0131
	5203	+0122	+0300	+1057	+0607	-0894	-1701	+8710	-1713	+0287
$\xi_{-z} = -20^\circ$	5204	+0163	+0300	+1409	+0808	-1402	-2512	+8409	-2361	+0697
	5205	+0204	+0300	+1760	+1006	-1951	-3414	+7659	-3287	+1098
	5206	+0246	+0300	+2110	+1201	-2553	-4427	+8110	-4299	+1440
	5207	+0287	+0300	+2459	+1392	-3197	-5519	+9914	-5654	+1781
	5208	+0000	-0063	+0001	-0000	+0108	-0021	+5153	-0257	-0385
	5208	+0018	-0744	+0049	-0176	+0000	+0000	+0000	+0000	+0000

Table 76

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	5220	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5210	+0041	-1349	-0286	-0287	+0457	+0287	+6707	+0155	-0538
	5211	+0000	+0153	+0001	+0000	+0095	-0012	+6846	-0240	-0325
	5212	+0041	+0449	+0286	+0287	-0244	-0363	+6834	-0660	-0038
W_3 B C^R	5213	+0081	+0449	+0573	+0572	-0638	-0851	+7590	-1145	+0159
$\xi_{-z} = -20^\circ$	5214	+0122	+0449	+0862	+0858	-1069	-1505	+4855	-1794	+0437
	5215	+0163	+0448	+1148	+1141	-1573	-2249	+0620	-2549	+0762
	5216	+0204	+0448	+1433	+1422	-2106	-3124	-1952	-3532	+1084
	5217	+0245	+0448	+1715	+1700	-2685	-4100	-3464	-4522	+1411
	5218	+0287	+0447	+1993	+1974	-3307	-5166	-3603	-5772	+1724
	5219	+0000	+0401	+0000	+0000	+0096	-0019	+5963	-0625	-0413
	5219	+0018	-0741	+0049	-0172	+0000	+0000	+0000	+0000	+0000

Table 77

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5231	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5221	+0041	-1199	-0202	-0352	+0536	+0181	+0561	+0096	-0535
	5222	+0000	+0089	+0001	+0000	+0112	-0020	+0710	-0158	-0300
	5223	+0040	+0599	+0203	+0350	-0301	-0272	+0710	-0435	+0037
W_3 B C^R	5224	+0081	+0599	+0406	+0700	-0743	-0632	+0710	-0715	+0313
$\xi_{-z} = -20^\circ$	5225	+0122	+0598	+0608	+1050	-1222	-1108	+0440	-1098	+0657
	5226	+0163	+0598	+0810	+1399	-1750	-1723	-0267	-1602	+1026
	5227	+0204	+0597	+1011	+1748	-2282	-2455	-0957	-2431	+1318
	5228	+0245	+0596	+1209	+2093	-2847	-3311	-1316	-3367	+1598
	5229	+0286	+0596	+1403	+2435	-3441	-4283	-1405	-4475	+1906
	5230	+0000	+0070	+0001	+0000	+0115	-0031	+0671	-0236	-0311
	5230	+0018	-0736	+0050	-0169	+0000	+0000	+0000	+0000	+0000

Table 78

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5242	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5232	+0041	-1049	-0104	-0392	+0595	+0075	+0534	+0164	-0467
	5233	+0000	-0000	+0000	-0000	+0118	-0016	+0745	-0071	-0227
	5234	+0040	+0749	+0105	+0391	-0336	-0144	+0744	-0243	+0103
W_3 B C^R	5235	+0081	+0749	+0210	+0782	-0813	-0335	+0638	-0376	+0451
	5236	+0121	+0749	+0315	+1172	-1334	-0593	+0426	-0594	+0816
$\xi_{-z} = -20^\circ$	5237	+0162	+0748	+0419	+1565	-1913	-0943	-0044	-0833	+1229
	5238	+0203	+0748	+0523	+1956	-2499	-1379	-0819	-1319	+1523
	5239	+0244	+0747	+0624	+2346	-3125	-1925	-1656	-1913	+1848
	5240	+0285	+0746	+0725	+2737	-3806	-2604	-2234	-2703	+2277
	5241	+0000	-0073	+0000	-0000	+0128	-0032	+0660	-0193	-0256
	5241	+0017	-0731	+0049	-0162	+0000	+0000	+0000	+0000	+0000

Table 79

	0000	-0001	-0001	-0002	-0002	-0004	-0006	-0005	-0006	-0004
	5253	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5243	+0041	-0900	+0000	-0406	+0595	-2779	+0658	+0185	-0565
	5244	+0000	+0067	+0000	+0000	+0113	-3212	+0834	+1393	-0216
	5245	+0041	+0900	+0000	+0405	-0363	-1936	+0810	+0996	+0131
W_3 B C^R	5246	+0081	+0900	+0000	+0810	-0852	-0692	+0741	+1298	+0526
	5247	+0122	+0900	+0000	+1215	-1385	+0375	+0844	+1552	+0936
$\xi_{-z} = -20^\circ$	5248	+0162	+0900	+0000	+1622	-1976	+0470	+1156	+1311	+1343
	5249	+0203	+0900	+0000	+2028	-2638	-0909	+1513	-1160	+1738
	5250	+0244	+0900	-0000	+2435	-3360	-1661	+1902	-2845	+2149
	5251	+0284	+0900	+0000	+2845	-4177	-2351	+2363	-2033	+2774
	5252	+0000	-0518	+0001	-0001	+0106	-4372	+0798	+3675	-0094
	5252	+0016	-0677	+0061	-0149	+0000	+0000	+0000	+0000	+0000

Table 80

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5264	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5254	+0041	-0751	+0104	-0393	+0611	-0104	+0587	-0294	-0595
	5255	+0000	+1707	-0000	+0000	+0133	-0027	+0747	-0282	-0369
	5256	+0041	+1051	-0106	+0392	-0320	+0131	+0674	-0141	-0020
$W_3\ B\ C^R$	5257	+0081	+1051	-0211	+0783	-0818	+0350	+0689	+0047	+0392
	5258	+0122	+1051	-0315	+1173	-1305	+0606	+1154	+0281	+0708
$\xi_{-z} = -20^\circ$	5259	+0162	+1052	-0420	+1563	-1855	+0955	+2055	+0551	+1067
	5260	+0203	+1053	-0524	+1956	-2410	+1401	+3258	+0755	+1355
	5261	+0244	+1053	-0627	+2348	-3040	+1958	+4597	+1195	+1672
	5262	+0285	+1054	-0728	+2738	-3682	+2631	+5778	+1796	+2001
	5263	+0000	-1027	-0000	-0000	+0138	-0029	+0683	-0145	-0319
	5263	+0017	-0660	+0068	-0153	+0000	+0000	+0000	+0000	+0000

Table 81

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5275	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5265	+0040	-0601	+0201	-0351	+0539	-0189	+0577	-0304	-0506
	5266	+0000	-1742	-0001	-0000	+0130	-0019	+0735	-0268	-0356
	5267	+0041	+1201	-0203	+0351	-0287	+0260	+0662	-0042	-0074
$W_3\ B\ C^R$	5268	+0081	+1202	-0407	+0701	-0754	+0645	+0660	+0274	+0327
	5269	+0122	+1202	-0609	+1051	-1203	+1123	+1214	+0565	+0520
$\xi_{-z} = -20^\circ$	5270	+0163	+1203	-0812	+1400	-1687	+1729	+2117	+1079	+0780
	5271	+0204	+1203	-1012	+1747	-2197	+2433	+3049	+1736	+0998
	5272	+0245	+1204	-1210	+2094	-2736	+3281	+3821	+2499	+1203
	5273	+0286	+1205	-1404	+2436	-3307	+4226	+4432	+3346	+1442
	5274	+0000	+1779	-0001	+0000	+0129	-0007	+0649	-0345	-0390
	5274	+0016	-0655	+0067	-0146	+0000	+0000	+0000	+0000	+0000

Table 82

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5286	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5276	+0041	-0452	+0286	-0288	+0463	-0293	+0590	-0466	-0449
	5277	+0000	-0894	+0000	-0001	+0139	-0022	+0744	-0273	-0341
	5278	+0041	+1352	-0288	+0286	-0209	+0355	+0688	+0120	-0059
W_3 B C^R	5279	+0081	+1351	-0575	+0573	-0621	+0850	+0618	+0564	+0283
	5280	+0122	+1352	-0863	+0857	-1027	+1482	+1054	+1060	+0460
$\xi_{-z} = -20^\circ$	5281	+0163	+1352	-1150	+1142	-1491	+2233	+1645	+1771	+0635
	5282	+0204	+1352	-1436	+1423	-1988	+3093	+2123	+2510	+0800
	5283	+0246	+1353	-1718	+1702	-2532	+4043	+2560	+3389	+0937
	5284	+0287	+1353	-1997	+1975	-3134	+5088	+3027	+4175	+1160
	5285	+0000	-1561	-0001	-0000	+0145	-0014	+0666	-0321	-0385
	5285	+0016	-0644	+0070	-0146	+0000	+0000	+0000	+0000	+0000

Table 83

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5297	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5287	+0040	-0301	+0349	-0203	+0340	-0380	+0658	-0517	-0371
	5288	+0000	-1380	-0001	-0001	+0147	-0024	+0786	-0177	-0328
	5289	+0041	+1501	-0352	+0202	-0126	+0410	+0815	+0231	-0135
W_3 B C^R	5290	+0081	+1501	-0704	+0405	-0464	+0967	+0685	+0704	+0107
	5291	+0122	+1500	-1057	+0607	-0878	+1663	+0721	+1321	+0301
$\xi_{-z} = -20^\circ$	5292	+0163	+1500	-1409	+0808	-1331	+2450	+0896	+2079	+0486
	5293	+0204	+1500	-1761	+1006	-1834	+3334	+1105	+2784	+0723
	5294	+0246	+1500	-2111	+1201	-2400	+4311	+1294	+3584	+0897
	5295	+0287	+1500	-2459	+1392	-3022	+5388	+1545	+4399	+1085
	5296	+0000	-0600	+0001	-0002	+0142	-0021	+0755	-0206	-0330
	5296	+0016	-0635	+0070	-0141	+0000	+0000	+0000	+0000	+0000

Table 84

W_3 B C^R

$\xi_{-z} = -20°$

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0005
	5308	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5298	+0040	-0151	+0390	-0105	+0211	-0448	+6252	-0635	-3492
	5299	+0000	-0930	-0000	-0001	+0140	-0021	+7730	-0319	-3959
	5300	+0040	+1651	-0391	+0104	-0019	+0440	+8316	+0201	-2776
	5301	+0081	+1650	-0785	+0210	-0239	+1007	+7886	+0673	-2063
	5302	+0122	+1649	-1178	+0316	-0614	+1701	+3589	+1170	-0300
	5303	+0163	+1648	-1572	+0421	-1020	+2466	+0770	+1889	+1862
	5304	+0204	+1648	-1965	+0525	-1497	+3316	-0419	+2624	+3714
	5305	+0245	+1647	-2360	+0627	-2039	+4267	-0841	+3402	+5137
	5306	+0287	+1647	-2755	+0727	-2645	+5312	-0222	+4251	+8089
	5307	+0000	-1489	-0001	-0001	+0139	-0014	+7158	-0370	-3972
	5307	+0015	-0636	+0066	-0134	+0000	+0000	+0000	+0000	+0000

Table 85

W_3 B C^R

$\xi_{-z} = -20°$

0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
5319	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
5309	+0040	-0000	+0404	-0000	+0076	-0475	+0738	-0628	-3223
5310	+0000	-1328	-0001	-0001	+0143	-0024	+0835	-0214	-4190
5311	+0040	-1799	-0405	-0001	+0124	+0436	+0962	+0276	-4417
5312	+0081	+1800	-0812	+0000	+0040	+0982	+0948	+0775	-4868
5313	+0122	+1799	-1219	+0002	-0127	+1607	+0677	+1336	-4849
5314	+0163	+1798	-1627	+0005	-0401	+2333	-0094	+2073	-3178
5315	+0204	+1797	-2035	+0009	-0767	+3139	-0808	+2756	-0991
5316	+0245	+1796	-2446	+0015	-1223	+4033	-1234	+3502	+0245
5317	+0286	+1796	-2857	+0021	-1747	+5013	-1390	+4218	+1569
5318	+0000	-1300	-0001	-0001	+0143	-0023	+0843	-0138	-3967
5318	+0015	-0630	+0066	-0129	+0000	+0000	+0000	+0000	+0000

Table 86

W_3 B C^R

$\xi_{-z} = -20°$

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0005	-0004
	5330	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5320	+0040	+0149	+0390	+0104	-0286	-0485	+0684	-0679	-0267
	5321	+0000	-1250	-0001	-0001	+1464	-0027	+0713	-0180	-0430
	5322	+0041	-1649	-0392	-0106	+2707	+0407	+0882	+0138	-0631
	5323	+0081	-1650	-0783	-0210	+3699	+0874	+0933	+0550	-0789
	5324	+0122	-1650	-1174	-0312	+4373	+1438	+0813	+1110	-0962
	5325	+0162	-1651	-1568	-0413	+4677	+2069	+0344	+1792	-1169
	5326	+0203	-1651	-1959	-0511	+4155	+2768	-0490	+2414	-1270
	5327	+0244	-1652	-2353	-0606	+2957	+3565	-1471	+3220	-1250
	5328	+0285	-1653	-2746	-0697	+0629	+4472	-2131	+4059	-1226
	5329	+0000	-1190	-0001	-0001	+1559	-0028	+0682	-0115	-0423
	5329	+0013	-0603	+0062	-0109	+0000	+0000	+0000	+0000	+0000

Table 87

W_3 B C^R

$\xi_{-z} = -20°$

0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
5341	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
5331	+0041	+0299	+0351	+0202	-0134	-0444	+0718	-0421	-0057
5332	+0000	-1104	-0001	-0002	+0138	-0025	+0760	-0032	-0294
5333	+0041	-1498	-0351	-0204	+0400	+0346	+0877	+0395	-0520
5334	+0081	-1499	-0702	-0406	+0674	+0733	+1065	+0677	-0827
5335	+0122	-1499	-1051	-0607	+0991	+1177	+1284	+1203	-1125
5336	+0162	-1499	-1400	-0806	+1323	+1681	+1401	+1901	-1388
5337	+0203	-1499	-1747	-1002	+1671	+2230	+1429	+2781	-1564
5338	+0244	-1499	-2093	-1194	+2058	+2876	+1368	+3643	-1775
5339	+0285	-1499	-2437	-1384	+2481	+3561	+1351	+4770	-1985
5340	+0000	-1067	-0001	-0002	+0140	-0018	+0701	+0099	-0156
5340	+0012	-0595	+0061	-0103	+0000	+0000	+0000	+0000	+0000

Table 88

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	5352	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5342	+0040	-1501	-0351	-0202	+0115	+0498	-9071	+1238	+0331
	5343	+0000	+1602	-0001	+0000	-0078	+0100	-6961	+0651	+0408
	5344	+0040	+0301	+0350	+0203	-0322	-0342	-4548	+0124	+0520
W_3 B C^R	5345	+0081	+0300	+0702	+0405	-0630	-0913	-3489	-0476	+0638
	5346	+0122	+0300	+1055	+0607	-1049	-1612	-3653	-1121	+0901
$\xi_{-z} = +20^\circ$	5347	+0163	+0300	+1407	+0807	-1509	-2443	+0293	-2085	+1098
	5348	+0204	+0300	+1758	+1005	-2016	-3374	+3633	-3175	+1321
	5349	+0245	+0300	+2108	+1200	-2572	-4406	+7282	-4451	+1507
	5350	+0287	+0300	+2456	+1391	-3210	-5515	+9573	-5803	+1856
	5351	+0000	+1589	-0001	+0000	-0071	+0085	-7993	+0366	+0331
	5351	+0018	-0736	+0052	-0176	+0000	+0000	+0000	+0000	+0000

Table 89

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	5363	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5353	+0040	-1351	-0286	-0285	+0237	+0400	-8617	+0965	+0232
	5354	+0000	+0856	+0000	+0001	-0079	+0086	-6318	+0413	+0313
	5355	+0041	+0451	+0287	+0287	-0394	-0285	-3200	-0181	+0438
W_3 B C^R	5356	+0081	+0450	+0573	+0573	-0784	-0777	-3202	-0628	+0621
	5357	+0122	+0449	+0861	+0858	-1193	-1422	-5976	-1294	+0853
$\xi_{-z} = +20^\circ$	5358	+0163	+0449	+1148	+1142	-1671	-2195	-7589	-2226	+1012
	5359	+0204	+0448	+1434	+1424	-2168	-3091	-7889	-3279	+1232
	5360	+0246	+0448	+1716	+1701	-2723	-4092	-7614	-4314	+1553
	5361	+0287	+0447	+1995	+1976	-3347	-5166	-6715	-5744	+1797
	5362	+0000	+0989	-0000	+0001	-0080	+0081	-7107	+0029	+0189
	5362	+0018	-0729	+0053	-0172	+0000	+0000	+0000	+0000	+0000

Table 90

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5374	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5364	+0041	-1200	-0203	-0351	+0327	+0301	-0904	+0847	+0186
	5365	+0000	+0813	+0000	+0002	-0080	+0101	-0702	+0548	+0376
	5366	+0040	+0601	+0202	+0351	-0458	-0164	-0415	+0093	+0527
W_3 B C^R	5367	+0081	+0600	+0405	+0702	-0897	-0521	-0430	-0238	+0797
	5368	+0122	+0599	+0608	+1052	-1368	-1005	-0732	-0575	+1084
$\xi_{-z} = +20^\circ$	5369	+0163	+0598	+0810	+1400	-1874	-1616	-1294	-1221	+1331
	5370	+0204	+0597	+1010	+1748	-2375	-2365	-1799	-2123	+1529
	5371	+0245	+0596	+1209	+2094	-2946	-3237	-2214	-3097	+1825
	5372	+0286	+0596	+1404	+2438	-3543	-4205	-2343	-4239	+2132
	5373	+0000	+1516	-0001	+0000	-0085	+0098	-0737	+0379	+0324
	5373	+0018	-0736	+0050	-0169	+0000	+0000	+0000	+0000	+0000

Table 91

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5385	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5375	+0041	-1050	-0105	-0391	+0398	+0171	-0900	+0622	+0075
	5376	+0000	+1553	-0001	+0000	-0082	+0099	-0740	+0494	+0370
	5377	+0040	+0751	+0104	+0391	-0494	-0043	-0478	+0229	+0527
W_3 B C^R	5378	+0081	+0750	+0209	+0783	-0964	-0224	-0537	-0057	+0779
	5379	+0122	+0749	+0314	+1174	-1479	-0479	-0788	-0238	+1130
$\xi_{-z} = +20^\circ$	5380	+0162	+0749	+0418	+1565	-2040	-0830	-1273	-0481	+1469
	5381	+0203	+0748	+0522	+1956	-2641	-1261	-2240	-0805	+1850
	5382	+0244	+0747	+0624	+2348	-3304	-1787	-3310	-1267	+2253
	5383	+0285	+0747	+0725	+2739	-4002	-2457	-4071	-1982	+2731
	5384	+0000	+1484	-0001	+0000	-0085	+0092	-0826	+0308	+0296
	5384	+0017	-0731	+0050	-0163	+0000	+0000	+0000	+0000	+0000

Table 92

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0005	-0006	-0005	-0004
	5396	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5386	+0041	-0900	-0000	-0405	+0434	+0743	-7633	+0617	+0129
	5387	+0000	+1751	-0000	+0000	-0070	+0915	-7050	+0662	+0448
	5388	+0040	+0901	-0001	+0405	-0502	+1012	-5019	+0509	+0625
W_3 B C^R	5389	+0081	+0901	-0001	+0810	-0972	+1078	-4741	+0462	+0873
	5390	+0122	+0900	-0001	+1215	-1488	+1196	-3147	+0499	+1221
$\xi_{-z} = +20^\circ$	5391	+0162	+0900	-0001	+1621	-2105	+1333	-2138	+0481	+1642
	5392	+0203	+0900	-0001	+2028	-2795	+1632	-1554	+0473	+2183
	5393	+0244	+0900	-0002	+2436	-3550	+1992	-1410	+0584	+2723
	5394	+0285	+0900	-0002	+2847	-4432	+2387	-0973	+1076	+3559
	5395	+0000	-1635	-0000	-0000	-0058	+0885	-7541	+0680	+0464
	5395	+0017	-0720	+0052	-0159	+0000	+0000	+0000	+0000	+0000

Table 93

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5407	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5397	+0040	-0751	+0104	-0391	+0411	-0011	-0774	+0119	+0024
	5398	+0000	+1277	-0001	+0001	-0080	+0091	-0774	+0321	+0339
	5399	+0041	+1052	-0106	+0393	-0499	+0240	-0628	+0333	+0512
W_3 B C^R	5400	+0081	+1052	-0212	+0784	-0965	+0450	-0481	+0440	+0740
	5401	+0122	+1052	-0317	+1175	-1466	+0719	-0055	+0581	+0986
$\xi_{-z} = +20^\circ$	5402	+0162	+1052	-0421	+1567	-2048	+1090	+0549	+0950	+1416
	5403	+0203	+1053	-0525	+1958	-2647	+1574	+1505	+1465	+1845
	5404	+0244	+1053	-0628	+2349	-3296	+2157	+2535	+2124	+2254
	5405	+0285	+1054	-0729	+2739	-3964	+2862	+3418	+2921	+2710
	5406	+0000	+1532	-0001	+0001	-0077	+0090	-0846	+0008	+0215
	5406	+0017	-0648	+0073	-0155	+0000	+0000	+0000	+0000	+0000

Table 94

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5418	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5408	+0040	-0602	+0201	-0351	+0363	-0118	-0722	-0093	+0022
	5409	+0000	+1621	-0001	+0000	-0069	+0087	-0780	+0273	+0324
	5410	+0041	+1202	-0204	+0351	-0452	+0363	-0684	+0431	+0463
W_3 B C^R	5411	+0081	+1202	-0408	+0702	-0898	+0753	-0573	+0709	+0689
	5412	+0122	+1202	-0610	+1051	-1346	+1241	-0182	+1058	+0927
$\xi_{-z} = +20^\circ$	5413	+0163	+1203	-0813	+1401	-1872	+1880	+0382	+1818	+1299
	5414	+0204	+1204	-1015	+1750	-2425	+2637	+0905	+2708	+1606
	5415	+0245	+1204	-1213	+2096	-2991	+3518	+1471	+3623	+1929
	5416	+0286	+1205	-1408	+2439	-3605	+4498	+1840	+4656	+2265
	5417	+0000	+1570	-0001	+0000	-0070	+0091	-0916	-0074	+0194
	5417	+0017	-0642	+0073	-0151	+0000	+0000	+0000	+0000	+0000

Table 95

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	5430	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5420	+0040	-0451	+0285	-0286	+0284	-0205	-6940	-0166	+0152
	5421	+0000	+1516	-0002	+0001	-0071	+0102	-7993	+0343	+0398
	5422	+0041	+1351	-0288	+0286	-0390	+0477	-7229	+0621	+0515
W_3 B C^R	5423	+0081	+1351	-0574	+0572	-0784	+0981	-7366	+1101	+0716
	5424	+0122	+1352	-0862	+0857	-1198	+1624	-4510	+1630	+0878
$\xi_{-z} = +20^\circ$	5425	+0163	+1352	-1149	+1141	-1708	+2422	-2241	+2493	+1143
	5426	+0204	+1352	-1434	+1422	-2247	+3319	-0713	+3491	+1439
	5427	+0246	+1353	-1716	+1701	-2814	+4301	+0352	+4668	+1736
	5428	+0287	+1353	-1996	+1975	-3446	+5391	+2485	+5641	+2100
	5429	+0000	+1637	-0001	+0000	-0061	+0103	-8493	-0067	+0197
	5429	+0016	-0623	+0075	-0143	+0000	+0000	+0000	+0000	+0000

Table 96

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5441	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5431	+0040	-0301	+0350	-0202	+0180	-0297	-0608	-0338	+0128
	5432	+0000	+1541	-0003	+0001	-0063	+0085	-0738	+0204	+0287
W_3 B C^R	5433	+0041	+1500	-0351	+0202	-0305	+0517	-0651	+0576	+0350
	5434	+0081	+1500	-0704	+0406	-0646	+1090	-0882	+1196	+0539
	5435	+0122	+1500	-1057	+0608	-1056	+1803	-0881	+1914	+0707
$\xi_{-z} = +20^\circ$	5436	+0163	+1500	-1411	+0809	-1542	+2637	-1098	+2854	+0983
	5437	+0205	+1500	-1762	+1007	-2096	+3569	-1315	+3879	+1300
	5438	+0246	+1500	-2111	+1202	-2706	+4582	-1414	+4934	+1630
	5439	+0288	+1500	-2462	+1394	-3356	+5696	-1397	+6006	+1958
	5440	+0000	+1540	-0001	+0001	-0058	+0082	-0883	-0228	+0060
	5440	+0016	-0624	+0073	-0139	+0000	+0000	+0000	+0000	+0000

Table 97

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5452	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5442	+0040	-0150	+0390	-0104	+0055	-0361	-0639	-0293	+0176
	5443	+0000	+1645	-0001	+0000	-0061	+0090	-0715	+0266	+0281
	5444	+0041	+1650	-0392	+0105	-0204	+0564	-0669	+0702	+0312
W_3 B C^R	5445	+0081	+1649	-0783	+0211	-0462	+1156	-1034	+1442	+0421
	5446	+0122	+1649	-1178	+0317	-0821	+1872	-1461	+2229	+0583
	5447	+0163	+1648	-1573	+0422	-1237	+2674	-2039	+3003	+0799
$\xi_{-z} = +20^\circ$	5448	+0204	+1648	-1966	+0526	-1767	+3580	-2510	+4038	+1142
	5449	+0245	+1647	-2360	+0628	-2357	+4566	-2844	+5156	+1484
	5450	+0287	+1647	-2755	+0729	-2994	+5648	-3129	+6315	+1823
	5451	+0000	+1632	-0001	+0000	-0049	+0099	-0854	-0082	+0118
	5451	+0015	-0617	+0070	-0131	+0000	+0000	+0000	+0000	+0000

Table 98

W_3 B C^R

$\xi_{-z} = +20°$

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	5463	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5453	+0040	+0001	+0404	+0001	-0081	-0392	-0619	-0218	+0222
	5454	+0000	+1724	-0002	+0000	-0057	+0084	-0631	+0367	+0264
	5455	+0041	+1799	-0407	+0001	-0088	+0558	-0746	+0867	+0242
	5456	+0081	+1799	-0813	+0002	-0196	+1134	-1149	+1629	+0336
	5457	+0122	+1798	-1221	+0004	-0436	+1823	-1898	+2594	+0514
	5458	+0163	+1797	-1628	+0007	-0729	+2595	-2910	+3742	+0732
	5459	+0204	+1797	-2038	+0012	-1109	+3439	-3781	+4697	+0915
	5460	+0245	+1796	-2449	+0017	-1570	+4355	-4350	+5674	+1114
	5461	+0286	+1795	-2858	+0023	-2111	+5373	-4757	+6772	+1408
	5462	+0000	+1606	-0001	+0000	-0049	+0085	-0847	+0209	+0170
	5462	+0015	-0612	+0070	-0127	+0000	+0000	+0000	+0000	+0000

Table 99

W_3 B C^R

$\xi_{-z} = +20°$

	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0005	-0005
	5474	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5464	+0040	+0150	+0391	+0105	-1844	-0385	-0595	-0101	+3679
	5465	+0000	+1784	-0000	+0000	-0461	+0079	-0735	+0439	+3037
	5466	+0041	-1651	-0392	-0105	+0411	+0538	-0873	+1033	+2829
	5467	+0081	-1651	-0783	-0208	+0953	+1028	-1059	+1624	+2706
	5468	+0122	-1651	-1175	-0310	+1033	+1644	-1784	+2510	+3493
	5469	+0162	-1652	-1567	-0410	+0411	+2333	-2940	+3759	+5115
	5470	+0203	-1652	-1959	-0508	-0798	+3111	-4358	+4912	+6684
	5471	+0244	-1653	-2351	-0602	-2610	+3968	-5723	+6088	+8077
	5472	+0285	-1653	-2745	-0694	-5255	+4925	-6497	+7350	+9966
	5473	+0000	-1592	-0000	-0000	-0327	+0081	-0884	+0490	+3308
	5473	+0013	-0582	+0066	-0107	+0000	+0000	+0000	+0000	+0000

Table 100

Configuration / Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	5485	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	5475	+0041	+0300	+0351	+0202	-0283	-0360	-0302	+0298	+5311
	5476	+0000	-1632	-0000	-0000	-0052	+0085	-0517	+0745	+4068
	5477	+0041	-1500	-0352	-0203	+0173	+0477	-0746	+1345	+3285
W_3 B C^R	5478	+0081	-1500	-0701	-0404	+0382	+0901	-1016	+1857	+2766
	5479	+0122	-1500	-1053	-0606	+0618	+1381	-1344	+2678	+1862
$\xi_{-z} = +20°$	5480	+0162	-1500	-1401	-0803	+0910	+1924	-1572	+3561	+1229
	5481	+0203	-1500	-1750	-1000	+1266	+2470	-1488	+4261	-1591
	5482	+0244	-1500	-2096	-1193	+1650	+3105	-1573	+5096	-4453
	5483	+0285	-1500	-2439	-1382	+2072	+3800	-1632	+6197	-6387
	5484	+0000	+1691	-0001	+0000	-0055	+0092	-0797	+0467	+2985
	5484	+0012	-0569	+0065	-0100	+0000	+0000	+0000	+0000	+0000

Table 101

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
0000		-0001	-0001	-0002	-0002	-0006	-0004	-0006	-0006	-0005
3000		+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
✓	3001	+0051	-1800	-0506	-0000	-0208	+0627	-0287	+0622	+0350
✓	3002	+0040	-1800	-0405	-0000	+0136	+0482	-0287	+0822	+0385
✓	3003	+0030	-1800	-0299	-0000	-0007	+0344	-0143	+0630	+0296
✓	3004	+0020	-1800	-0202	-0000	+0101	+0221	+0000	+0711	+0369
✓	3005	+0010	-1800	-0097	-0000	+0087	+0106	+0000	+0317	+0126
	3007	+0010	-0001	+0101	-0000	+0338	-0108	+0000	-0199	+0269
	3008	+0021	-0000	+0208	-0000	+0521	-0238	+0143	+0030	+0178
	3009	+0031	-0000	+0305	-0000	+0525	-0352	+0000	-0105	+0060
	3010	+0041	-0000	+0407	-0000	+0309	-0482	+0000	-0217	+0087
	3011	+0051	-0000	+0507	-0000	+0683	-0619	+0299	-0185	+0188
	3012	+0061	-0000	+0609	-0000	+0340	-0764	+0311	-0329	-0040
	3013	+0082	-0000	+0820	-0000	+0503	-1080	+0455	-0162	+0116
	3014	+0102	-0000	+1017	-0000	+0578	-1387	+0599	+0116	+0097
	3015	+0122	-0000	+1224	-0000	+0310	-1725	+0897	+0452	-0091
	3016	+0143	-0000	+1426	-0000	+0202	-2087	+1042	+1060	+0078
	3017	+0163	-0000	+1634	-0000	+1608	-2481	+1472	+1888	+0407
	3018	+0184	-0000	+1836	-0000	+0820	-2895	+3773	+2503	-0185
	3019	+0204	+0000	+2043	+0000	-3519	-3336	+1760	+1996	+0107
	3020	+0183	+0000	+1835	+0000	+0613	-2892	+3773	+0202	-1067
	3021	+0204	+0000	+2040	+0001	-4177	-3324	+1760	+0052	-0692
	3022	+0225	+0000	+2250	+0001	-3254	-3785	+3198	+1381	-0756
	3023	+0245	+0000	+2451	+0001	-2586	-4269	+3342	+1308	-1500
	3024	+0266	+0000	+2658	+0000	-2233	-4790	+4205	+1366	-1063
	3025	+0287	+0000	+2866	+0000	-0953	-5334	+5067	+1239	-1869
	3026	+0295	+0000	+2953	+0001	-1251	-5571	+4779	+1102	-2137
	3027	+0000	+1779	-0001	+0000	+1405	+0001	-1524	-5068	-1262
	3027	+0018	-0928	-0009	-0178	+0000	+0000	+0000	+0000	+0000

✓ For these results $-\sigma$ and λ $-180°$ are tabulated instead of σ and λ.

Table 102

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0006	-0006
	3034	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	3029	+0051	-1750	-0505	-0044	+0424	+0619	+0001	+1590	+6345
†	3030	+0041	-1750	-0404	-0035	+0330	+0477	+0001	+1629	+4596
†	3032	+0020	-1750	-0198	-0017	+0137	+0220	+0000	+0964	+3280
†	3031	+0030	-1750	-0303	-0026	+0241	+0353	+0000	+0585	+3932
†	3033	+0010	-1750	-0100	-0009	+0039	+0119	+0000	+0086	+1054
	3035	+0010	+0050	+0100	+0009	-0127	-0109	+0000	-0071	+1046
	3036	+0020	+0050	+0201	+0017	-0161	-0229	+0015	+0253	+3752
	3037	+0030	+0050	+0302	+0026	-0340	-0354	+0031	+0202	+2937
	3038	+0041	+0050	+0404	+0035	-0411	-0479	+0046	+0115	+3981
	3039	+0051	+0050	+0504	+0044	-0542	-0615	+0060	-0197	+3453
	3040	+0061	+0050	+0606	+0053	-0639	-0758	+0060	-0228	+2931
W_4	3041	+0081	+0050	+0810	+0071	-0815	-1063	+0091	+0156	+0982
	3042	+0102	+0050	+1013	+0088	-1006	-1380	+0150	+0705	+2820
	3043	+0122	+0050	+1215	+0105	-1234	-1704	+0225	+0677	+2348
	3044	+0142	+0050	+1419	+0122	-1488	-2076	+0344	+1375	+3394
	3045	+0163	+0050	+1621	+0140	-1819	-2455	+0478	+1786	+1718
	3046	+0183	+0050	+1826	+0157	-2207	-2860	+0807	+2054	+3140
	3047	+0204	+0050	+2029	+0174	-2842	-3287	+1058	+1268	-2720
	3048	+0224	+0050	+2234	+0191	-3639	-3763	+1505	+1314	-8432
	3049	+0245	+0050	+2440	+0208	-4179	-4250	+1863	+1822	-8343
	3050	+0266	+0050	+2650	+0225	-4906	-4780	+2308	+2545	-6811
	3051	+0286	+0050	+2851	+0241	-5601	-5312	+2770	+2608	-6844
	3052	+0295	+0050	+2937	+0248	-5829	-5544	+2902	+3284	-3616
	3053	+0000	+0043	+0001	+0000	+0060	+0010	-0103	-3404	-6563
	3053	+0018	-0940	-0012	-0176	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 103

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0006
	3060	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	3055	+0051	-1700	-0499	-0088	+0098	+0595	-0014	+0957	+3087
†	3056	+0041	-1700	-0400	-0071	+0077	+0470	-0030	+0806	+3158
†	3057	+0031	-1700	-0301	-0053	+0059	+0336	-0015	+0929	+2307
†	3058	+0020	-1700	-0200	-0035	+0042	+0227	-0015	+0702	+2290
†	3059	+0010	-1700	-0101	-0018	+0022	+0101	+0000	+0635	+1327
	3061	+0010	+0100	+0100	+0018	-0016	-0118	+0030	+0408	+0857
	3062	+0020	+0099	+0200	+0035	-0032	-0237	+0030	+0275	+3878
	3063	+0030	+0100	+0299	+0052	-0052	-0354	+0045	+0256	+2307
	3064	+0040	+0100	+0398	+0070	-0075	-0478	+0045	+0340	+3414
	3065	+0051	+0100	+0501	+0088	-0094	-0612	+0060	+0123	+2450
	3066	+0061	+0100	+0599	+0105	-0112	-0753	+0060	-0315	+2688
W_4	3067	+0081	+0100	+0799	+0140	-0154	-1044	+0120	+0261	+2882
	3068	+0102	+0100	+1002	+0175	-0197	-1376	+0208	+0525	+1781
	3069	+0122	+0100	+1200	+0210	-0245	-1684	+0327	+0903	+2338
	3070	+0143	+0100	+1403	+0244	-0304	-2056	+0503	+1512	-0465
	3071	+0163	+0100	+1605	+0279	-0382	-2430	+0751	+1751	+1159
	3072	+0183	+0100	+1805	+0313	-0474	-2823	+1102	+2131	-0476
	3073	+0204	+0100	+2006	+0347	-0545	-3250	+1715	+2850	-2351
	3074	+0224	+0100	+2208	+0380	-0647	-3698	+2227	+3201	+5488
	3075	+0245	+0100	+2411	+0414	-0772	-4176	+2828	+3417	-6230
	3076	+0266	+0100	+2613	+0447	-0912	-4684	+3297	+3936	-5392
	3077	+0286	+0101	+2815	+0480	-1054	-5204	+3885	+4189	-5895
	3078	+0295	+0101	+2900	+0493	-1107	-5417	+4061	+4238	-0706
	3079	+0000	-1504	-0000	-0000	+0017	+0005	-0104	-2166	-2808
	3079	+0018	-0938	-0012	-0176	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 104

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0005
	3090	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
✓	3085	+0051	-1650	-0489	-0131	+0141	+0607	+0045	+0635	+0326
✓	3086	+0041	-1650	-0392	-0105	+0111	+0477	-0015	+0503	+0033
✓	3087	+0030	-1650	-0294	-0079	+0084	+0346	-0015	+0490	+0156
✓	3088	+0020	-1650	-0196	-0052	+0057	+0222	+0000	+0021	+0138
✓	3089	+0010	-1650	-0098	-0026	+0028	+0115	+0000	+0086	+0069
	3091	+0010	+0150	+0099	+0026	-0026	-0100	+0015	-0307	+0017
	3092	+0020	+0150	+0197	+0053	-0058	-0215	+0030	-0376	-0218
	3093	+0031	+0150	+0296	+0079	-0085	-0339	+0030	-0202	+0087
	3094	+0041	+0150	+0393	+0105	-0119	-0462	+0061	-0453	+0307
	3095	+0051	+0150	+0490	+0131	-0146	-0593	+0076	-0536	+0070
	3096	+0061	+0150	+0588	+0157	-0175	-0732	+0076	-0479	+0280
W_4	3097	+0081	+0150	+0785	+0210	-0243	-1016	+0152	-0537	-0308
	3098	+0102	+0150	+0981	+0261	-0317	-1333	+0287	-0089	-0356
	3099	+0122	+0150	+1178	+0313	-0392	-1650	+0436	+0614	-0283
	3100	+0142	+0150	+1375	+0365	-0480	-1998	+0689	+0991	-0129
	3101	+0163	+0150	+1572	+0416	-0590	-2358	+0971	+1741	-0395
	3102	+0183	+0150	+1769	+0467	-0718	-2749	+1402	+2047	-0496
	3103	+0204	+0150	+1967	+0518	-0860	-3153	+1908	+2151	-0943
	3104	+0224	+0150	+2164	+0568	-0988	-3575	+2576	+2481	-0550
	3105	+0245	+0150	+2362	+0618	-1149	-4026	+3152	+2515	-0931
	3106	+0266	+0151	+2558	+0667	-1334	-4475	+3630	+2185	-1222
	3107	+0286	+0151	+2756	+0716	-1522	-4937	+4221	+2367	-1595
	3108	+0295	+0151	+2837	+0736	-1602	-5127	+4420	+1424	-1825
	3109	+0000	+0259	+0001	+0000	+0007	+0001	+0259	-3098	-0869
	3109	+0017	-0942	-0013	-0172	+0000	+0000	+0000	+0000	+0000

✓ For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 105

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0005
	3116	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
✓	3111	+0051	-1600	-0476	-0173	+0189	+0580	-0059	+0761	-0039
✓	3112	+0040	-1600	-0380	-0138	+0151	+0451	-0044	+0633	+0127
✓	3113	+0030	-1600	-0286	-0104	+0112	+0331	-0015	+0584	-0063
✓	3114	+0020	-1600	-0189	-0069	+0073	+0211	-0015	+0235	-0089
✓	3115	+0010	-1600	-0095	-0035	+0036	+0106	-0015	-0368	-0212
	3117	+0010	+0200	+0096	+0035	-0034	-0097	+0015	-0507	-0134
	3118	+0020	+0200	+0190	+0069	-0077	-0210	+0029	-0655	-0145
	3119	+0030	+0200	+0287	+0104	-0117	-0323	+0044	-0451	+0201
	3120	+0041	+0200	+0382	+0139	-0162	-0459	+0044	-0460	-0014
	3121	+0051	+0200	+0476	+0173	-0201	-0579	+0059	-0542	+0093
	3122	+0061	+0200	+0572	+0208	-0243	-0707	+0074	-0721	-0265
W_4	3123	+0081	+0200	+0765	+0277	-0325	-0987	+0132	-0554	-0166
	3124	+0102	+0200	+0956	+0346	-0424	-1290	+0268	-0243	-0322
	3125	+0122	+0200	+1145	+0414	-0522	-1600	+0441	+0788	-0200
	3126	+0142	+0200	+1337	+0482	-0645	-1931	+0691	+1159	-0148
	3127	+0163	+0200	+1529	+0550	-0787	-2276	+1015	+1788	-0053
	3128	+0183	+0200	+1720	+0618	-0951	-2642	+1368	+2340	-0207
	3129	+0204	+0200	+1910	+0685	-1126	-3014	+1868	+2559	-0177
	3130	+0225	+0200	+2103	+0752	-1311	-3408	+2353	+2747	-0802
	3131	+0245	+0201	+2294	+0818	-1515	-3801	+2794	+3261	-0874
	3132	+0266	+0201	+2483	+0883	-1734	-4198	+3265	+3892	-0743
	3133	+0286	+0201	+2673	+0947	-1946	-4603	+3765	+3098	-1219
	3134	+0295	+0201	+2751	+0973	-2046	-4771	+3898	+2582	-1275
	3135	+0000	-1727	-0000	-0000	+0008	-0004	-0083	-2231	-0414
	3135	+0017	-0941	-0012	-0172	+0000	+0000	+0000	+0000	+0000

✓ For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 106

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0006
	3142	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	3137	+0051	-1550	-0460	-0214	+0241	+0563	-0057	+0160	-0734
†	3138	+0040	-1550	-0366	-0170	+0184	+0440	-0028	+0117	-1216
†	3139	+0030	-1550	-0275	-0128	+0137	+0323	-0029	+0092	-1817
†	3140	+0020	-1550	-0182	-0085	+0088	+0206	-0029	+0327	+0316
†	3141	+0010	-1551	-0091	-0042	+0040	+0104	-0014	-0051	-0346
	3143	+0010	+0250	+0093	+0043	-0048	-0095	+0014	+0132	+1210
	3144	+0020	+0250	+0184	+0086	-0097	-0198	+0028	+0103	+2284
	3145	+0030	+0250	+0276	+0128	-0148	-0309	+0042	+0223	+3158
	3146	+0041	+0250	+0369	+0172	-0201	-0435	+0057	+0661	+3801
	3147	+0051	+0250	+0461	+0214	-0256	-0553	+0086	+0220	+2367
	3148	+0061	+0250	+0552	+0257	-0309	-0678	+0101	+0490	+3612
W_4	3149	+0081	+0250	+0737	+0342	-0415	-0946	+0159	+0710	+3059
	3150	+0102	+0250	+0922	+0428	-0538	-1236	+0305	+0936	+2362
	3151	+0122	+0250	+1104	+0512	-0664	-1526	+0480	+1709	+2661
	3152	+0142	+0250	+1288	+0596	-0813	-1835	+0726	+2193	+2679
	3153	+0163	+0250	+1472	+0681	-0987	-2167	+1019	+2604	+1728
	3154	+0183	+0250	+1657	+0765	-1185	-2503	+1309	+3284	+1689
	3155	+0204	+0250	+1841	+0848	-1389	-2848	+1763	+3770	+2892
	3156	+0224	+0250	+2024	+0930	-1599	-3206	+2142	+4121	-0365
	3157	+0245	+0251	+2206	+1012	-1832	-3572	+2463	+4520	+0975
	3158	+0266	+0251	+2390	+1093	-2093	-3943	+2787	+5140	+2748
	3159	+0286	+0251	+2570	+1172	-2350	-4310	+3182	+4932	-1080
	3160	+0295	+0251	+2644	+1205	-2454	-4472	+3360	+4185	-8382
	3161	+0000	-1152	-0000	-0000	+0006	-0002	+0082	-0926	+3809
	3161	+0017	-0938	-0011	-0171	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 107

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0006
	3168	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
†	3163	+0051	-1500	-0438	-0253	+0288	+0525	-0059	+0856	+1171
†	3164	+0041	-1500	-0351	-0203	+0229	+0407	-0059	+0963	+0635
†	3165	+0030	-1500	-0261	-0151	+0169	+0296	-0030	+0880	+0027
†	3166	+0020	-1500	-0175	-0101	+0108	+0192	-0030	+0646	+1073
†	3167	+0010	-1500	-0087	-0050	+0051	+0089	-0015	+0391	-1016
	3169	+0010	+0300	+0089	+0051	-0053	-0096	+0015	+0657	+0402
	3170	+0020	+0300	+0175	+0101	-0115	-0193	+0015	+0676	+2048
	3171	+0030	+0300	+0263	+0152	-0172	-0297	+0030	+0933	+4291
	3172	+0041	+0300	+0352	+0203	-0236	-0408	+0045	+0462	+5087
	3173	+0051	+0300	+0439	+0253	-0300	-0527	+0074	+0517	+2131
	3174	+0061	+0300	+0527	+0304	-0359	-0654	+0089	+0812	+1725
W_4	3175	+0081	+0300	+0703	+0405	-0489	-0901	+0134	+1198	+1848
	3176	+0102	+0300	+0879	+0505	-0637	-1168	+0268	+1218	-0098
	3177	+0122	+0300	+1054	+0606	-0791	-1452	+0431	+1653	-0290
	3178	+0142	+0300	+1230	+0706	-0973	-1741	+0655	+2227	-0383
	3179	+0163	+0300	+1406	+0806	-1172	-2052	+0863	+2876	-1986
	3180	+0183	+0300	+1580	+0905	-1390	-2376	+1071	+3754	-0233
	3181	+0204	+0300	+1755	+1004	-1607	-2701	+1503	+4328	+3538
	3182	+0224	+0300	+1929	+1101	-1855	-3038	+1755	+5246	+5507
	3183	+0245	+0301	+2103	+1198	-2112	-3380	+1993	+5025	-4577
	3184	+0265	+0301	+2276	+1294	-2387	-3729	+2276	+5932	-2552
	3185	+0286	+0301	+2448	+1389	-2663	-4085	+2589	+5192	-8184
	3186	+0295	+0301	+2518	+1427	-2772	-4222	+2722	+4666	-7177
	3187	+0000	-0552	+0000	-0000	+0007	-0008	+0226	+0228	+4104
	3187	+0017	-0936	-0011	-0169	+0000	+0000	+0000	+0000	+0000

† For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 108

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0005
	3211	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
✓	3206	+0051	-1450	-0414	-0290	+0339	+0491	-0058	+1297	+0341
✓	3207	+0040	-1450	-0331	-0232	+0266	+0391	-0059	+0872	+0122
✓	3208	+0030	-1450	-0248	-0174	+0198	+0281	-0029	+0732	+0157
✓	3209	+0020	-1450	-0165	-0116	+0122	+0181	-0015	+0041	-0043
✓	3210	+0010	-1450	-0082	-0058	+0062	+0087	-0015	+0231	+0198
	3212	+0010	+0350	+0084	+0059	-0062	-0087	+0015	+0072	+0113
	3213	+0020	+0350	+0167	+0117	-0129	-0189	+0030	+0184	+0205
	3214	+0031	+0350	+0250	+0175	-0198	-0284	+0044	+0110	+0286
	3215	+0041	+0350	+0333	+0233	-0274	-0392	+0059	-0465	+0217
	3216	+0051	+0350	+0416	+0291	-0341	-0501	+0089	-0036	+0214
	3217	+0061	+0350	+0498	+0349	-0416	-0610	+0103	-0612	+0145
W_4	3218	+0081	+0350	+0664	+0465	-0573	-0843	+0118	-0378	+0029
	3219	+0102	+0350	+0832	+0581	-0737	-1106	+0252	+0467	-0149
	3220	+0122	+0350	+0997	+0696	-0922	-1359	+0400	+0864	-0097
	3221	+0142	+0350	+1163	+0811	-1123	-1643	+0578	+1910	+0029
	3222	+0163	+0350	+1328	+0925	-1344	-1933	+0740	+2716	+0331
	3223	+0183	+0350	+1493	+1039	-1580	-2228	+0873	+3103	+0088
	3224	+0204	+0350	+1658	+1153	-1807	-2540	+1242	+3661	+0160
	3225	+0224	+0350	+1822	+1266	-2080	-2862	+1330	+3695	-0163
	3226	+0245	+0350	+1985	+1377	-2355	-3192	+1641	+4182	-0163
	3227	+0204	+0350	+1658	+1153	-1815	-2552	+1304	+2242	-0307
	3228	+0266	+0351	+2147	+1488	-2631	-3523	+1819	+3131	-0605
	3229	+0286	+0351	+2308	+1597	-2922	-3872	+2058	+4038	-1084
	3230	+0295	+0351	+2374	+1641	-3037	-4007	+2177	+3109	-1063
	3231	+0000	+0241	+0001	+0000	+0024	-0015	+0017	-2456	-0352

✓ For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 109

	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
Configuration \ Exponent	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0006
	3238	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
✓	3233	+0051	-1400	-0388	-0326	+0383	+0460	-0089	+1019	+4374
✓	3234	+0041	-1400	-0311	-0261	+0300	+0363	-0089	+0832	+2889
✓	3235	+0031	-1400	-0234	-0196	+0233	+0263	-0060	+0511	+3182
✓	3236	+0020	-1399	-0155	-0130	+0155	+0173	-0016	+0796	+3569
✓	3237	+0010	-1399	-0077	-0065	+0076	+0074	+0000	+0306	+0804
	3239	+0010	+0399	+0078	+0065	-0059	-0084	+0000	+0395	+1177
	3240	+0020	+0400	+0155	+0130	-0143	-0171	+0030	+0610	+2446
	3241	+0030	+0400	+0233	+0195	-0212	-0261	+0059	+0761	+4196
	3242	+0040	+0400	+0310	+0260	-0299	-0363	+0059	+0694	+3697
	3243	+0051	+0400	+0388	+0326	-0389	-0465	+0103	+0273	+2854
	3244	+0061	+0400	+0466	+0391	-0469	-0559	+0117	+0058	+4299
W_4	3245	+0081	+0400	+0622	+0521	-0652	-0778	+0174	+0478	+2540
	3246	+0102	+0400	+0777	+0651	-0841	-1011	+0260	+0871	+1781
	3247	+0122	+0400	+0932	+0781	-1045	-1252	+0375	+1707	+1824
	3248	+0142	+0400	+1087	+0910	-1277	-1529	+0490	+2516	+3881
	3249	+0163	+0400	+1240	+1038	-1516	-1792	+0590	+3295	+4086
	3250	+0183	+0400	+1395	+1167	-1767	-2083	+0676	+3986	+4465
	3251	+0204	+0400	+1547	+1294	-2018	-2365	+0903	+4171	+4828
	3252	+0224	+0400	+1701	+1421	-2299	-2678	+0919	+5382	+3765
	3253	+0245	+0400	+1851	+1546	-2584	-2992	+1107	+5980	+5896
	3254	+0266	+0400	+2002	+1671	-2872	-3310	+1336	+5907	+0453
	3255	+0286	+0400	+2152	+1795	-3188	-3644	+1453	+6172	-0237
	3256	+0295	+0400	+2213	+1845	-3306	-3781	+1569	+5939	-4078
	3257	+0204	+0400	+1547	+1293	-2008	-2381	+0987	+3004	+2889
	3258	+0224	+0400	+1700	+1421	-2299	-2676	+0945	+3691	-2860
	3259	+0000	-0750	+0000	-0000	+0015	-0004	+0046	+0434	+9459
	3259	+0017	-0929	-0008	-0167	+0000	+0000	+0000	+0000	+0000

✓ For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 110

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0006	-0005
	3260	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
✓	3261	+0051	-1350	-0358	-0358	+0415	+0419	-0602	+1576	+0317
✓	3262	+0041	-1350	-0286	-0287	+0323	+0329	-0602	+1135	+0243
✓	3263	+0030	-1350	-0216	-0216	+0234	+0246	-0442	+0537	+0040
✓	3264	+0020	-1350	-0143	-0143	+0156	+0161	-0295	+0710	+0281
✓	3265	+0010	-1350	-0072	-0072	+0071	+0078	-0147	+0483	+0181
	3267	+0010	+0451	+0072	+0072	-0090	-0067	+0306	+0070	-0010
	3268	+0020	+0450	+0143	+0143	-0166	-0160	+0455	+0533	+0302
	3269	+0030	+0449	+0215	+0214	-0251	-0236	+0761	+5487	+2844
	3270	+0040	+0450	+0286	+0286	-0348	-0327	+1056	+0383	+0413
	3271	+0051	+0450	+0358	+0358	-0433	-0418	+1203	+0007	+0252
	3272	+0061	+0450	+0430	+0430	-0525	-0508	+1349	-0100	+0192
W_4	3273	+0081	+0450	+0573	+0573	-0728	-0703	+1952	+0464	+0206
	3274	+0102	+0450	+0716	+0716	-0942	-0906	+2396	+0586	+0176
	3275	+0122	+0450	+0859	+0859	-1171	-1138	+2997	+1590	+0170
	3276	+0142	+0450	+1001	+1001	-1412	-1385	+3587	+1934	+0242
	3277	+0163	+0450	+1143	+1143	-1675	-1645	+4324	+2387	+0245
	3278	+0183	+0450	+1284	+1284	-1947	-1915	+4770	+3636	+0367
	3279	+0194	+0450	+1355	+1355	-2082	-2049	+4475	+3924	+0409
	3280	+0204	+0450	+1425	+1425	-2216	-2191	+5065	+4399	+0475
	3281	+0214	+0450	+1495	+1495	-2359	-2331	+6246	+4437	+0447
	3282	+0224	+0450	+1565	+1565	-2516	-2478	+5361	+5136	+0241
	3283	+0234	+0450	+1634	+1634	-2649	-2636	+6835	+5312	+0320
	3284	+0245	+0450	+1704	+1704	-2799	-2776	+6835	+5958	+0386
	3285	+0255	+0450	+1773	+1772	-2955	-2931	+6983	+6206	+0364
	3286	+0265	+0450	+1842	+1841	-3103	-3094	+7721	+6333	+0082
	3287	+0276	+0450	+1911	+1911	-3271	-3247	+8028	+5774	-0083
	3288	+0286	+0450	+1979	+1979	-3427	-3411	+8176	+6615	+0276
	3289	+0295	+0450	+2035	+2034	-3555	-3537	+8470	+5738	+0014
	3290	+0000	-0613	+0000	-0000	+0006	-0002	+0674	+1369	+1222

✓ For these results $-\sigma$ and λ -180° are tabulated instead of σ and λ.

Table 111

W_4

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0006	-0006	-0006	-0005
	3315	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	3316	+0010	+0900	-0000	+0101	-0101	+0175	+0000	+0113	+0285
	3317	+0020	+0900	+0000	+0204	-0217	-0156	+0292	-0188	+0038
	3318	+0031	+0900	-0000	+0305	-0342	+0476	+0729	-0209	+0130
	3319	+0041	+0900	-0000	+0406	-0481	+0506	+1021	-0207	+0229
	3320	+0051	+0900	-0000	+0508	-0613	+0410	+1312	-0406	+0109
	3321	+0061	+0900	-0000	+0611	-0768	+0673	+1603	-0935	+0017
	3322	+0081	+0900	-0000	+0813	-1063	+0327	+2187	-1149	-0072
	3323	+0102	+0900	-0000	+1016	-1374	+0187	+2598	-1521	-0488
	3324	+0122	+0900	-0000	+1220	-1707	+0243	+3325	-1726	-0599
	3325	+0142	+0900	-0000	+1425	-2076	-0048	+4043	-1804	-0752
	3326	+0163	+0900	-0000	+1629	-2459	-0187	+4754	-2308	-1035
	3327	+0183	+0900	-0000	+1834	-2865	+0807	+5604	-2364	-1118
	3328	+0194	+0900	-0000	+1937	-3080	+1810	+5010	-2547	-1344
	3329	+0204	+0900	+0000	+2039	-3295	-2534	+6738	-2965	-1651
	3330	+0214	+0900	-0000	+2142	-3526	-2082	+8327	-4486	-2068
	3331	+0225	+0900	-0001	+2246	-3742	+2892	+7575	-4962	-2642
	3332	+0235	+0900	-0000	+2348	-3983	-1799	+7417	-5924	-3305
	3333	+0245	+0900	-0001	+2452	-4255	+1617	+7841	-6603	-3730
	3334	+0255	+0900	-0001	+2554	-4512	+2597	+7987	-7362	-3762
	3335	+0266	+0900	-0001	+2657	-4774	+1238	+8278	-7900	-4275
	3336	+0276	+0900	-0001	+2760	-5041	+0037	+8828	-7632	-4273
	3337	+0286	+0900	-0001	+2864	-5311	-1139	+9410	-8996	-4774
	3338	+0295	+0900	-0001	+2950	-5553	+1130	+9555	-8241	-4890
	3339	+0000	+1717	-0001	+0000	+0023	+0072	-1208	-7497	-2131
	3339	+0015	-0929	-0008	-0150	+0000	+0000	+0000	+0000	+0000

Table 112

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0006	-0004	-0006	-0005	-0005
	4901	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4892	-0040	+0000	-0406	+0000	-0841	+0600	+0404	+0404	-1145
	4892	+0000	+0000	+0001	+0000	-1847	+0027	+0404	-0347	-1565
	4893	+0040	+0000	+0406	+0001	-2672	-0554	+1012	-0983	-1314
$W_4\ B\ C^R$	4894	+0080	+0000	+0814	+0001	-3182	-1256	+1618	-1790	-1625
	4895	+0120	+0000	+1222	+0001	-4201	-2080	+2377	-2868	-1886
$\xi_{-z} = 0$	4896	+0160	+0000	+1632	+0001	-2427	-3012	+3438	-3868	-1492
	4897	+0200	+0000	+2042	+0001	-8404	-4067	+4352	-5038	-1455
	4898	+0240	+0000	+2455	+0001	-6712	-5258	+6931	-6527	-1800
	4900	+0280	+0000	+2868	+0002	-9501	-6586	+9361	-8368	-2848
	4900	-0000	+0000	-0002	+0001	-2299	+0020	-0304	-0652	-2381
	4900	-0000	+0000	-0062	+0047	+0000	+0000	+0000	+0000	+0000

Table 113

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	4919	+0000	+0150	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4909	-0040	+0150	-0391	-0105	+0131	+0583	-0083	+0785	-0225
	4910	+0000	+0150	+0001	+0000	-0004	+0025	-0054	+0076	+0128
	4911	+0040	+0150	+0393	+0105	-0142	-0535	+0033	-0560	+1171
$W_4\ B\ C^R$	4912	+0080	+0150	+0786	+0210	-0288	-1204	+0106	-1445	+1135
	4913	+0120	+0150	+1181	+0314	-0451	-1997	+0457	-2431	+1221
$\xi_{-z} = 0^\circ$	4914	+0160	+0150	+1575	+0417	-0682	-2858	+1090	-3428	+1802
	4916	+0200	+0150	+1971	+0519	-0978	-3823	+2262	-4351	+3021
	4916	+0240	+0150	+2366	+0619	-1325	-4865	+3668	-5434	+4740
	4918	+0280	+0150	+2761	+0717	-1749	-5965	+4901	-6543	+6897
	4918	+0000	+0150	-0000	+0000	-0008	+0022	-0184	-0211	-0824
	4918	+0000	+0150	-0054	+0038	+0000	+0000	+0000	+0000	+0000

Table 114

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4930	+0000	+0300	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4920	-0040	+0300	-0352	-0203	+0274	+0510	-0054	+0704	-0118
	4921	+0000	+0300	-0000	-0000	+0007	+0017	-0026	+0001	-0013
	4922	+0040	+0300	+0352	+0203	-0272	-0483	+0047	-0493	+0166
$W_4\ B\ C^R$	4924	+0080	+0300	+0704	+0406	-0580	-1065	+0151	-1244	+0281
	4924	+0120	+0300	+1056	+0607	-0926	-1735	+0493	-2012	+0376
$\xi_{-z} = 0^\circ$	4926	+0160	+0300	+1408	+0807	-1359	-2471	+0999	-2699	+0572
	4926	+0200	+0300	+1758	+1005	-1876	-3238	+1667	-3409	+0867
	4928	+0240	+0300	+2105	+1200	-2469	-4033	+2340	-4159	+1123
	4928	+0280	+0300	+2452	+1391	-3089	-4914	+3218	-5133	+1432
	4930	+0000	+0300	+0001	+0000	+0004	+0000	-0088	-0099	-0032
	4929	+0000	+0300	-0049	+0033	+0000	+0000	+0000	+0000	+0000

Table 115

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	4941	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4931	-0040	+0450	-0287	-0287	+0401	+0432	-1274	+0450	-0221
	4932	+0000	+0450	+0000	+0001	+0014	+0029	-0699	+0004	+0011
	4934	+0040	+0450	+0287	+0288	-0401	-0365	+0186	-0399	+0264
$W_4\ B\ C^R$	4934	+0080	+0450	+0574	+0575	-0852	-0826	+1369	-0973	+0479
	4936	+0120	+0450	+0860	+0861	-1369	-1329	+1963	-1339	+0762
$\xi_{-z} = 0^\circ$	4936	+0160	+0450	+1145	+1146	-1962	-1936	+3150	-1801	+1096
	4938	+0200	+0450	+1428	+1428	-2626	-2585	+3897	-2398	+1423
	4938	+0240	+0450	+1707	+1707	-3318	-3295	+5398	-3069	+1869
	4939	+0280	+0450	+1983	+1983	-4082	-4037	+7062	-3873	+2250
	4940	+0000	+0450	-0000	-0000	+0012	+0018	-0319	-0035	+0050
	4940	+0000	+0450	-0045	+0026	+0000	+0000	+0000	+0000	+0000

Table 116

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4952	+0000	+0600	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4942	-0040	+0600	-0203	-0352	+0505	+0318	-0084	+0271	-0300
	4943	+0000	+0600	-0000	+0001	+0015	+0037	-0009	-0155	-0041
W_4 B C^R	4944	+0040	+0600	+0203	+0352	-0492	-0226	+0066	-0488	+0274
	4946	+0080	+0600	+0405	+0705	-1092	-0524	+0186	-0871	+0546
$\xi_{-z} = 0^\circ$	4946	+0120	+0600	+0606	+1057	-1758	-0856	+0036	-1080	+0954
	4948	+0160	+0600	+0806	+1408	-2496	-1292	-0262	-1503	+1352
	4948	+0200	+0600	+1004	+1757	-3255	-1814	-0637	-1917	+1807
	4950	+0240	+0600	+1199	+2106	-4072	-2399	-1143	-2196	+2232
	4950	+0280	+0600	+1390	+2452	-4934	-3037	-1651	-2825	+2740
	0050	+0003	+0050	+0500	+0500	+ 250	+ 1	- 175	- 176	+ 250
	0050	+0003	+0050	+0500	+0500	+ 1	+ 1	- 175	- 176	+ 250

Table 117

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4963	+0000	+0750	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4954	-0040	+0750	-0105	-0392	+0589	+0168	-0128	+0012	-0424
	4954	+0000	+0750	-0000	+0001	+0025	+0031	-0055	-0233	-0104
	4956	+0040	+0750	+0104	+0393	-0524	-0084	-0015	-0411	+0235
W_4 B C^R	4956	+0080	+0750	+0209	+0785	-1208	-0239	+0075	-0642	+0597
	4957	+0120	+0750	+0313	+1180	-1986	-0399	-0015	-0819	+1083
$\xi_{-z} = 0^\circ$	4958	+0160	+0750	+0415	+1574	-2861	-0619	-0389	-1010	+1574
	4959	+0200	+0750	+0517	+1970	-3822	-0885	-1451	-1116	+2152
	4960	+0240	+0750	+0618	+2366	-4887	-1259	-2439	-1327	+2789
	4961	+0280	+0750	+0716	+2761	-5986	-1675	-3334	-1759	+3356
	4962	+0000	+0750	-0000	+0001	+0030	+0023	-0141	-0409	-0136
	4962	+0000	+0750	-0037	+0018	+0000	+0000	+0000	+0000	+0000

Table 118

W_4 B C^R

$\xi_{-z} = 0°$

Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
Exponent / Configuration									
0000	-0001	-0001	-0002	-0002	-0004	-0006	-0005	-0005	-0004
4974	+0000	+0900	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4964	-0040	+0900	-0001	-0405	+0621	+2633	-0142	-0559	-0639
4966	+0000	+0900	-0001	+0002	+0032	+2850	-0007	-0656	-0296
4966	+0040	+0900	-0001	+0408	-0558	+3112	+0157	-0727	+0013
4968	+0080	+0900	-0001	+0815	-1270	+2452	+0229	-0832	+0408
4968	+0120	+0900	-0001	+1224	-2087	+2121	+0390	-1010	+0898
4970	+0160	+0900	-0001	+1633	-3025	+1582	+0565	-1167	+1449
4970	+0200	+0900	-0001	+2044	-4076	-1666	+0740	-1112	+2152
4972	+0240	+0900	-0002	+2458	-5273	+5493	+0931	-1231	+2871
4972	+0280	+0900	-0001	+2872	-6613	+0502	+1121	-1351	+3740
4973	+0000	+0900	-0001	+0002	+0024	+2030	-0067	-1160	-0480
4974	+0000	+0900	-0022	+0013	+0000	+0000	+0000	+0000	+0000

Table 119

W_4 B C^R

$\xi_{-z} = 0°$

0000	-0001	-0001	-0002	-0002	-0006	-0004	-0006	-0005	-0005
4004	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000
3994	-0040	+0000	-0406	-0001	+2514	+0619	-0033	+1295	+3045
3995	+0000	+0000	-0000	-0001	+2533	+0039	-0034	+0487	+2350
3996	+0040	+0000	+0407	-0001	+1868	-0548	+0259	-0290	+2007
3998	+0080	+0000	+0815	-0000	+1431	-1245	+0700	-1239	+1482
3998	+0120	+0000	+1222	-0000	+0683	-2066	+1288	-2277	+1310
4000	+0160	+0000	+1633	-0001	+1644	-2998	+2034	-3290	+1876
4000	+0200	+0000	+2043	+0000	-4838	-4052	+2343	-4451	+2811
4002	+0240	+0000	+2456	+0000	-3053	-5234	+4437	-5968	+1404
4002	+0280	+0000	+2869	+0000	-4422	-6551	+6521	-7819	+0863
4003	+0000	+0000	+0000	-0001	+2824	+0023	-0454	+0479	+3122
4004	+0000	+0000	+0013	-0173	+0000	+0000	+0000	+0000	+0000

Table 120

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	4015	+0000	+0150	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4005	-0040	+0150	-0393	-0105	+0145	+0591	-0028	+0729	-0830
	4006	+0000	+0150	-0000	-0000	+0013	+0041	-0014	-0025	-0291
	4007	+0040	+0150	+0393	+0105	-0129	-0517	+0074	-0738	+0338
W_4 B C^R	4008	+0080	+0150	+0786	+0210	-0277	-1183	+0162	-1540	+0844
	4009	+0120	+0150	+1179	+0313	-0436	-1969	+0488	-2495	+1327
$\xi_{-z} = 0^\circ$	4010	+0160	+0150	+1575	+0417	-0672	-2834	+1125	-3492	+2239
	4012	+0200	+0150	+1970	+0519	-0983	-3786	+2280	-4392	+3729
	4012	+0240	+0150	+2365	+0619	-1331	-4821	+3694	-5379	+5891
	4014	+0280	+0150	+2760	+0718	-1780	-5904	+4946	-6604	+7533
	4014	+0000	+0150	-0001	+0000	+0008	+0026	-0029	-0272	-1073
	4014	+0000	+0150	+0010	-0169	+0000	+0000	+0000	+0000	+0000

Table 121

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4026	+0000	+0300	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4016	-0040	+0300	-0352	-0203	+0296	+0534	-0088	+0668	-0167
	4017	+0000	+0300	-0000	-0000	+0026	+0039	-0029	-0033	-0058
	4018	+0040	+0300	+0352	+0203	-0248	-0457	+0045	-0599	+0116
W_4 B C^R	4020	+0080	+0300	+0703	+0405	-0566	-1033	+0180	-1312	+0242
	4020	+0120	+0300	+1055	+0606	-0898	-1704	+0539	-2035	+0380
$\xi_{-z} = 0^\circ$	4022	+0160	+0300	+1407	+0807	-1343	-2434	+1032	-2793	+0596
	4022	+0200	+0300	+1757	+1005	-1863	-3198	+1690	-3481	+0899
	4024	+0240	+0300	+2105	+1200	-2457	-4000	+2350	-4183	+1184
	4024	+0280	+0300	+2451	+1391	-3094	-4865	+3251	-5218	+1478
	4025	+0000	+0300	-0000	-0000	+0023	+0026	-0095	-0164	-0081
	4025	+0000	+0300	+0011	-0167	+0000	+0000	+0000	+0000	+0000

Table 122

W_4 B C^R

$\xi_{-z} = 0°$

Configuration / Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	4037	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4027	-0040	+0450	-0287	-0287	+0415	+0423	-0515	+0731	-0202
	4028	+0000	+0450	+0000	+0000	+0024	+0040	+0065	+0060	+0003
	4030	+0040	+0450	+0287	+0287	-0384	-0351	+1110	-0399	+0249
	4030	+0080	+0450	+0574	+0574	-0851	-0806	+2307	-1009	+0423
	4032	+0120	+0450	+0859	+0860	-1363	-1312	+3565	-1473	+0684
	4032	+0160	+0450	+1145	+1145	-1961	-1915	+4422	-1902	+1033
	4034	+0200	+0450	+1427	+1428	-2620	-2552	+5177	-2499	+1386
	4034	+0240	+0450	+1707	+1707	-3310	-3282	+7295	-3181	+1803
	4035	+0280	+0450	+1982	+1982	-4067	-4020	+8818	-4031	+2232
	4036	+0000	+0450	-0000	-0000	+0025	+0021	-0388	-0029	-0009
	4036	+0000	+0450	+0011	-0163	+0000	+0000	+0000	+0000	+0000

Table 123

W_4 B C^R

$\xi_{-z} = 0°$

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4048	+0000	+0600	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4038	-0040	+0600	-0203	-0351	+0522	+0314	-0080	-0006	-0547
	4039	+0000	+0600	-0001	+0000	+0030	+0046	+0024	-0422	-0259
	4040	+0040	+0600	+0202	+0352	-0470	-0222	+0114	-0699	+0079
	4042	+0080	+0600	+0404	+0704	-1069	-0519	+0250	-1097	+0379
	4042	+0120	+0600	+0606	+1057	-1736	-0848	+0111	-1303	+0791
	4044	+0160	+0600	+0806	+1408	-2469	-1291	-0145	-1586	+1190
	4044	+0200	+0600	+1003	+1757	-3235	-1806	-0492	-2126	+1632
	4046	+0240	+0600	+1198	+2105	-4041	-2374	-0994	-2428	+2054
	4046	+0280	+0600	+1390	+2451	-4907	-3026	-1461	-3125	+2526
	4047	+0000	+0600	-0001	-0000	+0034	+0037	-0038	-0413	-0197
	4046	+0000	+0600	+0010	-0154	+0000	+0000	+0000	+0000	+0000

Table 124

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4059	+0000	+0750	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4050	-0040	+0750	-0105	-0393	+0608	+0187	-0102	+0231	-0378
	4050	+0000	+0750	-0001	-0000	+0043	+0049	+0004	-0119	-0088
	4052	+0040	+0750	+0104	+0392	-0518	-0083	+0109	-0234	+0267
$W_4\ B\ C^R$	4052	+0080	+0750	+0209	+0786	-1185	-0225	+0213	-0517	+0606
	4053	+0120	+0750	+0312	+1179	-1964	-0380	+0153	-0643	+1120
$\xi_{-z} = 0^\circ$	4054	+0160	+0750	+0415	+1575	-2835	-0597	-0196	-0836	+1636
	4055	+0200	+0750	+0517	+1969	-3788	-0852	-1226	-0934	+2207
	4056	+0240	+0750	+0617	+2365	-4851	-1224	-2165	-1158	+2815
	4057	+0280	+0750	+0716	+2759	-5938	-1653	-3076	-1227	+3562
	4058	+0000	+0750	-0001	-0000	+0045	+0045	-0035	-0214	-0097
	4058	+0000	+0750	+0012	-0158	+0000	+0000	+0000	+0000	+0000

Table 125

Configuration / Exponent										
	0000	-0001	-0001	-0002	-0002	-0004	-0005	-0005	-0006	-0004
	4070	+0000	+0900	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4060	-0040	+0900	+0003	-0408	+0665	-1862	-0088	+7588	-0280
	4061	+0000	+0900	-0000	+0000	+0050	+0533	-0014	+1676	+0084
	4062	+0040	+0900	-0000	+0406	-0538	+0550	+0106	+1667	+0412
$W_4\ B\ C^R$	4064	+0080	+0900	-0000	+0814	-1245	+0464	+0211	+0720	+0816
	4064	+0120	+0900	-0001	+1222	-2041	+0476	+0362	-0376	+1316
$\xi_{-z} = 0^\circ$	4066	+0160	+0900	-0001	+1632	-2973	+0381	+0572	-1312	+1849
	4066	+0200	+0900	-0000	+2043	-4025	+0091	+0860	-1218	+2503
	4068	+0240	+0900	-0001	+2456	-5227	+0781	+1072	-4673	+3144
	4068	+0280	+0900	-0000	+2869	-6557	+0486	+1342	+0738	+4333
	4069	+0000	+0900	-0001	-0001	+0054	+0427	-0020	-0610	-0064
	4070	+0000	+0900	+0013	-0153	+0000	+0000	+0000	+0000	+0000

Table 126

W_4 B C^R

$\xi_{-z} = 0°$

Configuration / Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4082	+0000	+1050	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4071	-0040	+1050	+0105	-0396	+0617	-0052	-0074	+0578	+0013
	4072	+0000	+1050	-0000	-0001	+0047	+0066	-0015	+0599	+0306
	4073	+0040	+1050	-0105	+0391	-0518	+0216	+0134	+0723	+0660
	4074	+0075	+1050	-0196	+0733	-1092	+0329	+0177	+0736	+0936
	4075	+0080	+1050	-0210	+0785	-1182	+0357	+0077	+0488	+0926
	4076	+0120	+1050	-0314	+1179	-1953	+0514	+0433	+0584	+1421
	4077	+0160	+1050	-0417	+1574	-2825	+0730	+1175	+0603	+1918
	4078	+0200	+1050	-0519	+1969	-3755	+1000	+2536	+0718	+2449
	4080	+0240	+1050	-0619	+2364	-4806	+1376	+3771	+1014	+3075
	4080	+0280	+1050	-0718	+2759	-5896	+1782	+5016	+1135	+3536
	4081	+0000	+1050	-0000	-0001	+0053	+0080	-0131	+0772	+0446

Table 127

W_4 B C^R

$\xi_{-z} = 0°$

0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
4093	+0000	+1200	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4083	-0040	+1200	+0202	-0351	+0543	-0207	-0041	-0127	-0257
4084	+0000	+1200	-0001	+0000	+0048	+0050	+0003	+0053	+0015
4085	+0040	+1200	-0204	+0352	-0443	+0339	+0077	+0305	+0298
4086	+0080	+1200	-0406	+0703	-1026	+0639	+0137	+0369	+0523
4088	+0120	+1200	-0608	+1055	-1662	+0996	+0454	+0903	+1089
4088	+0160	+1200	-0808	+1407	-2400	+1428	+0954	+1330	+1546
4090	+0200	+1200	-1006	+1757	-3162	+1953	+1471	+1788	+1937
4090	+0240	+1200	-1200	+2104	-3959	+2506	+2292	+2206	+2400
4092	+0280	+1200	-1392	+2451	-4830	+3141	+3067	+2555	+2858
4092	+0000	+1200	-0001	-0001	+0055	+0067	-0085	-0090	+0136
4092	+0000	+1200	+0013	-0141	+0000	+0000	+0000	+0000	+0000

Table 128

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	4104	+0000	+1350	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4094	-0040	+1350	+0286	-0287	+0455	-0371	-0519	-0325	-0218
	4095	+0000	+1350	-0003	+0002	+0057	+0030	-0095	+0011	-0016
W_4 B C^R	4096	+0040	+1350	-0289	+0288	-0335	+0430	+0485	+0453	+0195
	4097	+0080	+1350	-0577	+0576	-0787	+0887	+1054	+0677	+0333
$\xi_{-z} = 0^\circ$	4098	+0120	+1350	-0861	+0860	-1286	+1412	+0910	+1142	+0576
	4099	+0160	+1350	-1147	+1145	-1875	+2007	+1202	+1730	+0876
	4100	+0200	+1350	-1429	+1427	-2508	+2653	+0620	+2377	+1236
	4101	+0240	+1350	-1708	+1707	-3231	+3348	+2801	+3067	+1605
	4102	+0280	+1350	-1984	+1983	-3975	+4085	+3103	+3783	+2001
	4103	+0000	+1350	-0000	-0001	+0057	+0015	-0495	-0227	-0091
	4103	+0000	+1350	+0023	-0136	+0000	+0000	+0000	+0000	+0000

Table 129

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4115	+0000	+1500	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4106	-0040	+1500	+0351	-0203	+0328	-0463	+0022	-0519	-0196
	4106	+0000	+1500	-0001	-0000	+0056	+0027	+0036	+0012	-0029
	4108	+0040	+1500	-0352	+0202	-0193	+0521	+0050	+0577	+0111
W_4 B C^R	4108	+0080	+1500	-0705	+0405	-0504	+1119	+0094	+1024	+0156
	4110	+0120	+1500	-1056	+0605	-0826	+1792	-0159	+1750	+0232
$\xi_{-z} = 0^\circ$	4110	+0160	+1500	-1408	+0806	-1244	+2518	-0590	+2448	+0370
	4112	+0200	+1500	-1758	+1004	-1746	+3300	-1141	+3211	+0633
	4112	+0240	+1500	-2105	+1198	-2328	+4087	-1632	+4019	+0854
	4114	+0280	+1500	-2453	+1391	-2968	+4951	-2318	+4938	+1165
	4114	+0000	+1500	-0000	-0001	+0064	+0020	+0006	-0167	-0094
	4114	+0000	+1500	+0023	-0130	+0000	+0000	+0000	+0000	+0000

Table 130

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	4125	+0000	+1650	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4116	-0040	+1650	+0391	-0105	+0186	-0528	-0019	-0424	-0473
	4117	+0000	+1650	-0001	-0000	+0048	+0024	+0025	+0104	-0147
	4118	+0040	+1650	-0394	+0105	-0074	+0591	+0038	+0695	+0249
W_4 B C^R	4119	+0080	+1650	-0787	+0209	-0206	+1270	+0021	+1367	+0325
	4120	+0120	+1650	-1180	+0313	-0352	+2047	-0201	+2225	+0198
$\xi_{-z} = 0^\circ$	4121	+0160	+1650	-1576	+0416	-0567	+2920	-0810	+3121	+0198
	4122	+0200	+1650	-1970	+0517	-0833	+3686	-1936	+4197	+0620
	4123	+0240	+1650	-2360	+0618	-1177	+4941	-3151	+5424	+1976
	4124	+0280	+1650	-2761	+0716	-1588	+6033	-4217	+6450	+3986
	4125	+0000	+1650	-0000	-0000	+0057	+0022	10005	-0220	-1241
	4126	+0000	+1650	+0027	-0125	+0000	+0000	+0000	+0000	+0000

Table 131

	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0006	-0005	-0005
	4137	+0000	+1800	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4128	-0040	+1800	+0406	-0000	+0390	-0569	+0000	-0667	-0551
	4128	+0000	+1800	-0000	-0001	+0566	+0012	+0134	+0118	-0084
	4129	+0040	+1800	-0406	-0001	+0491	+0597	+0416	+0737	-0416
W_4 B C^R	4130	+0080	+1800	-0814	-0001	+0626	+1313	+0099	+1465	-0835
	4131	+0120	+1800	-1224	-0000	+0564	+2127	+0086	+2384	-1719
$\xi_{-z} = 0^\circ$	4132	+0160	+1800	-1634	-0001	+0846	+3055	-0096	+3485	-1650
	4133	+0200	+1800	-2047	-0000	+0563	+4109	+2091	+4779	-1934
	4134	+0240	+1800	-2455	-0001	+1444	+5294	+1064	+6095	-3205
	4135	+0280	+1800	-2873	-0001	+1104	+6636	+0465	+7545	-4260
	4136	+0000	+1800	-0001	-0000	+0593	+0009	-0584	-0471	-2218
	4136	+0000	+1800	+0027	-0119	+0000	+0000	+0000	+0000	+0000

Table 132

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0006	-0005	-0005
	4170	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4160	-0040	+0000	-0408	-0001	+1462	+0640	+6828	+0321	-6862
	4161	+0000	+0000	-0001	-0000	+1083	+0052	+5277	-0346	-5547
	4162	+0040	+0000	+0406	-0000	+0903	-0524	+4663	-1046	-4754
$W_4\ B\ C^R$	4164	+0080	+0000	+0813	-0000	+0844	-1233	+5441	-1886	-4897
$\xi_{-z} = -20^\circ$	4164	+0120	+0000	+1220	+0000	+0565	-2055	+4976	-2959	-4113
	4166	+0160	+0000	+1630	+0000	+0239	-2986	+4053	-3957	-2668
	4166	+0200	+0000	+2040	+0001	-0548	-4049	+3284	-5197	-1424
	4168	+0240	+0000	+2455	+0001	-0478	-5240	+5778	-7279	-4711
	4168	+0280	+0000	+2865	+0001	-0701	-6553	+8278	-8455	-2445
	4169	+0000	+0000	-0001	-0000	+1212	+0046	+3965	-0632	-6071
	4170	+0000	+0000	+0015	-0176	+0000	+0000	+0000	+0000	+0000

Table 133

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	4181	+0000	+0150	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4171	-0040	+0150	-0393	-0105	+0267	+0641	+0577	+0644	-6530
	4172	-0000	+0150	-0002	-0001	+0105	+0064	+0562	-0096	-5165
	4173	+0040	+0150	+0391	+0105	-0060	-0481	+0503	-0765	-3271
$W_4\ B\ C^R$	4174	+0080	+0150	+0785	+0209	-0206	-1153	+0635	-1557	-3120
$\xi_{-z} = -20^\circ$	4175	+0120	+0150	+1179	+0313	-0393	-1945	+0841	-2473	-1390
	4176	+0160	+0150	+1575	+0417	-0660	-2805	+1240	-3532	+0801
	4178	+0200	+0150	+1970	+0519	-0991	-3760	+2257	-4462	+3040
	4178	+0240	+0150	+2364	+0619	-1348	-4798	+3653	-5425	+5145
	4180	+0280	+0150	+2759	+0718	-1791	-5870	+4920	-6592	+7319
	4180	+0000	+0150	-0001	-0000	+0106	+0072	+0469	-0106	-4969
	4180	+0000	+0150	+0013	-0174	+0000	+0000	+0000	+0000	+0000

Table 134

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4192	+0000	+0300	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4182	-0040	+0300	-0353	-0204	+0413	+0556	+0544	+0435	-0712
	4183	+0000	+0300	-0001	-0001	+0126	+0053	+0573	-0137	-0513
	4184	+0040	+0300	+0353	+0204	-0189	-0436	+0545	-0696	-0282
$W_4\ B\ C^R$	4186	+0080	+0300	+0705	+0406	-0502	-1031	+0662	-1333	-0073
	4186	+0120	+0300	+1055	+0606	-0849	-1693	+0939	-2137	+0058
$\xi_{-z} = -20^\circ$	4188	+0160	+0300	+1407	+0807	-1310	-2429	+1331	-2871	+0341
	4188	+0200	+0300	+1758	+1005	-1847	-3187	+1941	-3523	+0754
	4190	+0240	+0300	+2107	+1201	-2470	-3992	+2526	-4244	+1064
	4190	+0280	+0300	+2455	+1392	-3114	-4859	+3297	-5227	+1450
	4191	+0000	+0300	-0001	-0001	+0121	+0045	+0509	+0029	-0441
	4191	+0000	+0300	+0016	-0171	+0000	+0000	+0000	+0000	+0000

Table 135

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4203	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4193	-0040	+0450	-0289	-0288	+0527	+0474	+0462	+0274	-0790
	4194	-0000	+0450	-0002	-0001	+0127	+0073	+0612	-0524	-0688
	4196	+0040	+0450	+0286	+0287	-0290	-0318	+0629	-0940	-0348
$W_4\ B\ C^R$	4196	+0080	+0450	+0574	+0575	-0776	-0788	+0660	-1412	-0072
	4198	+0120	+0450	+0858	+0859	-1294	-1284	+0752	-1828	+0213
$\xi_{-z} = -20^\circ$	4198	+0160	+0450	+1144	+1145	-1899	-1884	+0904	-2355	+0537
	4200	+0200	+0450	+1426	+1427	-2563	-2535	+0954	-2882	+0980
	4200	+0240	+0450	+1706	+1707	-3274	-3250	+1180	-3626	+1356
	4201	+0280	+0450	+1982	+1983	-4028	-3991	+1319	-4389	+1808
	4202	+0000	+0450	-0000	+0000	+0119	+0061	+0717	-0240	-0608
	4202	+0000	+0450	+0019	-0173	+0000	+0000	+0000	+0000	+0000

Table 136

W_4 B C^R

$\xi_{-z} = -20°$

Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
Exponent / Configuration									
0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
4214	+0000	+0600	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4204	-0040	+0600	-0205	-0351	+0611	+0349	+6008	+0081	-0864
4205	+0000	+0600	-0001	-0000	+0127	+0063	+7205	-0413	-0661
4206	+0040	+0600	+0202	+0352	-0400	-0202	+7357	-0779	-0284
4208	+0080	+0600	+0405	+0705	-1004	-0507	+7507	-1176	+0084
4208	+0120	+0600	+0605	+1057	-1685	-0846	+6152	-1515	+0432
4210	+0160	+0600	+0805	+1407	-2389	-1275	+4943	-1892	+0787
4210	+0200	+0600	+1004	+1759	-3157	-1795	+1765	-2384	+1170
4212	+0240	+0600	+1198	+2105	-3961	-2368	-3381	-2700	+1578
4212	+0280	+0600	+1389	+2450	-4807	-3017	-6699	-3368	+2088
4213	+0000	+0600	-0001	+0001	+0124	+0056	+6969	-0513	-0676
4214	+0000	+0600	+0011	-0165	+0000	+0000	+0000	+0000	+0000

Table 137

W_4 B C^R

$\xi_{-z} = -20°$

0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
4225	+0000	+0750	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4216	-0040	+0750	-0106	-0392	+0693	+0185	+0550	-0301	-1049
4216	+0000	+0750	-0001	-0000	+0147	+0055	+0698	-0587	-0764
4218	+0040	+0750	+0103	+0391	-0434	-0082	+0757	-0773	-0355
4218	+0080	+0750	+0208	+0784	-1133	-0228	+0741	-1053	+0098
4219	+0120	+0750	+0312	+1178	-1894	-0392	+0695	-1203	+0577
4220	+0160	+0750	+0415	+1573	-2747	-0615	+0484	-1345	+1027
4221	+0200	+0750	+0516	+1968	-3684	-0868	-0326	-1481	+1483
4222	+0240	+0750	+0617	+2366	-4722	-1246	-1077	-1777	+1951
4223	+0280	+0750	+0715	+2758	-5799	-1651	-1811	-2235	+2477
4224	+0000	+0750	-0001	-0000	+0155	+0038	+0623	-0830	-0868
4224	+0000	+0750	+0010	-0160	+0000	+0000	+0000	+0000	+0000

Table 138

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0006	-0005	-0005	-0004
	4236	+0000	+0900	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4226	-0040	+0900	-0002	-0406	+0727	+4884	+0475	-1156	-1329
	4227	+0000	+0900	-0002	-0080	+0152	+5048	+0643	-1135	-1010
	4228	+0040	+0900	-0002	+0407	-0447	+4294	+0720	-1274	-0608
W_4 B C^R	4230	+0080	+0900	-0002	+0812	-1161	+3396	+0690	-1406	-0096
	4230	+0120	+0900	-0002	+1220	-1965	+2744	+0905	-1511	+0363
$\xi_{-z} = -20^\circ$	4232	+0160	+0900	-0001	+1631	-2873	+1486	+1304	-1459	+0887
	4232	+0200	+0900	-0001	+2040	-3883	-1133	+1781	-1343	+1502
	4234	+0240	+0900	-0002	+2452	-5048	+6420	+2200	-1573	+2091
	4234	+0280	+0900	-0002	+2869	-6354	+11618	+2771	-1703	+2842
	4235	+0000	+0900	-0002	+0001	+0145	+4066	+0595	-1836	-1325
	4236	+0000	+0900	+0033	-0157	+0000	+0000	+0000	+0000	+0000

Table 139

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0004
	4247	+0000	+1050	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4237	-0040	+1050	+0104	-0392	+0707	-0067	+0461	+0885	-0867
	4238	+0000	+1050	-0001	+0000	+0164	+0058	+0590	+1762	-0573
	4239	+0040	+1050	-0106	+0392	-0409	+0193	+0693	+1731	-0203
W_4 B C^R	4240	+0080	+1050	-0210	+0785	-1097	+0325	+0692	+2068	+0238
	4241	+0120	+1050	-0314	+1179	-1850	+0481	+1117	+2508	+0723
$\xi_{-z} = -20^\circ$	4242	+0160	+1050	-0417	+1575	-2687	+0694	+1981	+2943	+1188
	4243	+0200	+1050	-0519	+1970	-3593	+0970	+3534	+3755	+1591
	4244	+0240	+1050	-0620	+2365	-4605	+1335	+4948	+7351	+2178
	4246	+0280	+1050	-0718	+2760	-5661	+1754	+6397	+6488	+2553
	4246	+0000	+1050	-0001	+0000	+0162	+0056	+0540	-3117	-0687
	4246	+0000	+1050	+0033	-0154	+0000	+0000	+0000	+0000	+0000

Table 140

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4258	+0000	+1200	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4248	-0040	+1200	+0201	-0352	+0636	-0207	+0521	-0349	-0768
	4249	+0000	+1200	-0001	-0001	+0148	+0061	+0648	-0150	-0505
	4250	+0040	+1200	-0204	+0352	-0348	+0336	+0749	+0075	-0199
$W_4\ B\ C^R$	4251	+0080	+1200	-0406	+0703	-0922	+0633	+0803	+0180	+0117
	4252	+0120	+1200	-0608	+1055	-1582	+0970	+1105	+0319	+0521
$\xi_{-z} = -20^\circ$	4253	+0160	+1200	-0809	+1408	-2290	+1298	+1725	+0615	+0844
	4254	+0200	+1200	-1007	+1758	-3009	+1919	+2419	+1071	+1129
	4255	+0240	+1200	-1202	+2105	-3781	+2471	+3446	+1235	+1397
	4256	+0280	+1200	-1393	+2452	-4618	+3098	+4419	+1688	+1752
	4257	+0000	+1200	-0001	-0001	+0142	+0061	+0625	-0015	-0420
	4257	+0000	+1200	+0033	-0149	+0000	+0000	+0000	+0000	+0000

Table 141

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4269	+0000	+1350	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4259	-0040	+1350	+0286	-0287	+0553	-0354	+0503	-0448	-0686
	4260	+0000	+1350	-0001	-0001	+0163	+0042	+0604	-0033	-0500
	4262	+0040	+1350	-0288	+0286	-0210	+0451	+0724	+0346	-0273
$W_4\ B\ C^R$	4262	+0080	+1350	-0575	+0573	-0649	+0910	+0887	+0614	-0155
	4264	+0120	+1350	-0861	+0858	-1134	+1414	+0887	+1081	+0051
$\xi_{-z} = -20^\circ$	4264	+0160	+1350	-1146	+1144	-1714	+2006	+1006	+1606	+0331
	4266	+0200	+1350	-1428	+1425	-2331	+2651	+1066	+2223	+0611
	4266	+0240	+1350	-1708	+1705	-3025	+3346	+1454	+2888	+0894
	4268	+0280	+1350	-1983	+1980	-3732	+4065	+1650	+3607	+1174
	4268	+0000	+1350	-0000	-0001	+0166	+0042	+0576	+0146	-0408
	4268	+0000	+1350	+0033	-0142	+0000	+0000	+0000	+0000	+0000

Table 142

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0005
	4281	+0000	+1500	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4270	-0040	+1500	+0350	-0203	+0409	-0444	+5032	-0718	-6583
	4271	+0000	+1500	-0001	-0000	+0148	+0038	+6392	-0211	-5734
	4272	+0040	+1500	-0352	+0202	-0086	+0534	+7918	+0248	-5134
$W_4\ B\ C^R$	4273	+0080	+1500	-0703	+0403	-0365	+1126	+9305	+0767	-4786
	4274	+0120	+1500	-1056	+0605	-0667	+1816	+8991	+1475	-5476
$\xi_{-z} = -20^\circ$	4275	+0160	+1500	-1408	+0805	-1047	+2528	+6372	+2171	-4767
	4276	+0200	+1500	-1758	+1003	-1530	+3294	+2520	+2947	-3554
	4277	+0240	+1500	-2110	+1200	-2093	+4075	-1217	+3496	-2565
	4278	+0280	+1500	-2452	+1389	-2694	+4945	-6741	+5103	+3307
	4279	+0240	+1500	-2106	+1197	-2072	+4073	-1511	+4147	+0564
	4280	+0000	+1500	-0001	-0000	+0147	+0045	+6186	+0029	-4453

Table 143

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4292	+0000	+1650	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4282	-0040	+1650	+0392	-0106	+0279	-0533	+0398	-0328	-0365
	4283	+0000	+1650	-0000	-0001	+0154	+0035	+0560	+0279	-0366
	4284	+0040	+1650	-0392	+0103	+0069	+0590	+0752	+0951	-0386
$W_4\ B\ C^R$	4285	+0080	+1650	-0787	+0208	-0054	+1278	+0900	+1571	-0520
	4286	+0120	+1650	-1180	+0311	-0161	+2059	+0826	+2525	-0631
$\xi_{-z} = -20^\circ$	4287	+0160	+1650	-1575	+0414	-0316	+2922	+0501	+3417	-0823
	4288	+0200	+1650	-1971	+0516	-0518	+3884	-0322	+4314	-1093
	4289	+0240	+1650	-2365	+0615	-0806	+4961	-1293	+6324	-0705
	4290	+0280	+1650	-2761	+0713	-1182	+6069	-2130	+7138	-0820
	4291	+0000	+1650	-0000	-0001	+0164	+0017	+0471	+0196	-0419
	4292	+0000	+1650	+0027	-0122	+0000	+0000	+0000	+0000	+0000

Table 144

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0005	-0004
	4303	+0000	+1800	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4294	-0040	+1800	+0405	-0001	+1430	-0554	+0556	-0561	-0331
	4294	+0000	+1800	-0001	-0001	+1582	+0021	+0631	+0041	-0429
	4295	+0040	+1800	-0407	-0001	+1950	+0617	+0810	+0674	-0554
$W_4\ B\ C^R$	4296	+0080	+1800	-0815	-0001	+2278	+1535	+1019	+1484	-0750
	4297	+0120	+1800	-1222	-0002	+2868	+2147	+1273	+2477	-0962
$\xi_{-z} = -20^\circ$	4298	+0160	+1800	-1633	-0002	+3472	+3091	+1545	+3635	-1145
	4299	+0200	+1800	-2043	-0002	+3749	+4138	+1998	+5009	-1290
	4300	+0240	+1800	-2456	-0003	+4604	+5527	+1987	+6308	-1423
	4301	+0280	+1800	-2870	-0003	+4485	+6658	+2077	+7889	-1549
	4302	+0000	+1800	-0001	-0001	+1731	+0024	+0567	-0299	-0554
	4302	+0000	+1800	+0032	-0117	+0000	+0000	+0000	+0000	+0000

Table 145

	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0006	-0005	-0005
	4314	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4304	-0040	+0000	-0405	+0001	-1410	+0639	-9690	+0543	+3850
	4306	+0000	+0000	+0000	+0001	-1151	+0054	-7605	-0215	+2405
	4306	+0040	+0000	+0406	+0001	-1083	-0521	-5807	-0937	+1786
$W_4\ B\ C^R$	4308	+0080	+0000	+0814	+0001	-1010	-1232	-5369	-1799	+1834
	4308	+0120	+0000	+1221	+0001	-0791	-2048	-3120	-2787	+0833
$\xi_{-z} = +20^\circ$	4310	+0160	+0000	+1631	+0000	-0380	-2979	-0274	-3881	+0090
	4310	+0200	+0000	+2042	+0001	-0793	-4044	+1676	-5106	-0415
	4312	+0240	+0000	+2454	+0001	-0441	-5216	+4358	-6548	-1375
	4312	+0280	+0000	+2869	+0001	-0489	-6538	+6617	-8335	-2228
	4313	+0000	+0000	-0000	+0001	-1169	+0051	-8639	-0552	+1535
	4314	+0000	+0000	+0023	-0179	+0000	+0000	+0000	+0000	+0000

Table 146

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4336	+0000	+0300	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4326	-0040	+0300	-0352	-0202	+0135	+0554	-0932	+0305	+0237
	4328	+0000	+0300	+0000	+0001	-0106	+0055	-0769	-0100	+0332
	4328	+0040	+0300	+0350	+0204	-0384	-0422	-0546	-0918	+0395
W_4 B C^R	4330	+0080	+0300	+0703	+0406	-0679	-1027	-0458	-1623	+0542
	4330	+0120	+0300	+1055	+0607	-1027	-1687	-0129	-2299	+0705
$\xi_{-z} = +20^\circ$	4332	+0160	+0300	+1408	+0808	-1441	-2418	+0677	-3078	+0766
	4332	+0200	+0300	+1757	+1006	-1930	-3175	+1528	-3907	+0957
	4334	+0240	+0300	+2106	+1201	-2493	-3993	+2349	-4702	+1113
	4334	+0280	+0300	+2451	+1392	-3115	-4661	+3274	-5749	+1375
	4335	+0000	+0300	-0001	+0001	-0104	+0053	-0829	-0437	+0301
	4335	+0000	+0300	+0020	-0171	+0000	+0000	+0000	+0000	+0000

Table 147

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	4325	+0000	+0150	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4315	-0040	+0150	-0392	-0104	-0006	+0631	-0944	+0655	+4027
	4316	+0000	+0150	-0001	+0001	-0112	+0064	-0715	-0072	+3326
	4317	+0040	+0150	+0392	+0106	-0238	-0477	-0502	-0867	+2960
W_4 B C^R	4318	+0080	+0150	+0785	+0210	-0384	-1164	-0379	-1724	+3187
	4319	+0120	+0150	+1178	+0314	-0520	-1949	+0065	-2648	+3382
$\xi_{-z} = +20^\circ$	4320	+0160	+0150	+1574	+0417	-0706	-2825	+1047	-3664	+2178
	4322	+0200	+0150	+1967	+0519	-0983	-3773	+2350	-4725	+2261
	4322	+0240	+0150	+2365	+0619	-1329	-4824	+3807	-5746	+4379
	4324	+0280	+0150	+2757	+0717	-1759	-5904	+5051	-6941	+6702
	4324	+0000	+0150	-0001	+0001	-0109	+0061	-0740	-0408	+2341
	4324	+0000	+0150	+0020	-0174	+0000	+0000	+0000	+0000	+0000

Table 148

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	4350	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4340	-0040	+0450	-0287	-0287	+0286	+0446	-9132	+0894	+0351
	4341	+0000	+0450	-0000	+0000	-0111	+0057	-8252	+0357	+0528
	4342	+0040	+0450	+0287	+0288	-0481	-0536	-5840	-0078	+0739
W_4 B C^R	4344	+0080	+0450	+0574	+0575	-0958	-0787	-4786	-0673	+0913
	4344	+0120	+0450	+0860	+0861	-1489	-1290	-4647	-0984	+1239
$\xi_{-z} = +20^\circ$	4346	+0160	+0450	+1145	+1146	-2071	-1689	-2354	-1462	+1531
	4346	+0200	+0450	+1427	+1428	-2705	-2542	-0717	-2104	+1803
	4348	+0240	+0450	+1707	+1708	-3397	-3251	+2247	-2963	+2097
	4348	+0280	+0450	+1983	+1983	-4131	-4018	+5198	-3697	+2474
	4349	+0000	+0450	-0000	+0000	-0100	+0042	-8616	+0274	+0557
	4349	+0000	+0450	+0019	-0168	+0000	+0000	+0000	+0000	+0000

Table 149

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4361	+0000	+0600	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4352	-0040	+0600	-0203	-0351	+0408	+0338	-0921	+0450	+0157
	4352	+0000	+0600	-0000	+0001	-0091	+0072	-0821	+0109	+0434
	4354	+0040	+0600	+0202	+0353	-0572	-0196	-0616	-0287	+0678
W_4 B C^R	4354	+0080	+0600	+0405	+0705	-1178	-0488	-0559	-0720	+0938
	4356	+0120	+0600	+0606	+1057	-1838	-0623	-0692	-0913	+1335
$\xi_{-z} + 20^\circ$	4356	+0160	+0600	+0805	+1408	-2578	-1262	-0986	-1597	+1612
	4357	+0200	+0600	+1004	+1759	-3374	-1779	-1369	-1688	+2250
	4358	+0240	+0600	+1199	+2108	-4182	-2352	-2016	-2093	+2661
	4359	+0280	+0600	+1390	+2453	-5024	-2989	-2395	-2867	+3059
	4360	+0000	+0600	-0001	+0000	-0084	+0069	-0873	-0320	+0304
	4360	+0000	+0600	+0019	-0164	+0000	+0000	+0000	+0000	+0000

Table 150

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4372	+0000	+0750	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4362	-0040	+0750	-0105	-0391	+0475	+0187	-0916	+0042	-0012
	4363	+0000	+0750	-0000	+0002	-0090	+0058	-0816	-0084	+0356
	4364	+0040	+0750	+0105	+0395	-0642	-0072	-0571	-0277	+0604
$W_4\ B\ C^R$	4366	+0080	+0750	+0209	+0788	-1329	-0210	-0616	-0467	+1024
$\xi_{-z} = +20^\circ$	4366	+0120	+0750	+0313	+1183	-2098	-0362	-0645	-0663	+1482
	4368	+0160	+0750	+0416	+1578	-2998	-0583	-1178	-0851	+2016
	4368	+0200	+0750	+0518	+1974	-3994	-0833	-2417	-0839	+2736
	4370	+0240	+0750	+0618	+2370	-5093	-1193	-3583	-0956	+3484
	4370	+0280	+0750	+0716	+2765	-6188	-1613	-4519	-1315	+4092
	4371	+0000	+0750	-0001	+0001	-0081	+0045	-0885	-0401	+0244
	4372	+0000	+0750	+0020	-0160	+0000	+0000	+0000	+0000	+0000

Table 151

	0000	-0001	-0001	-0002	-0002	-0004	-0005	-0006	-0006	-0004
	4383	+0000	+0900	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4374	-0040	+0900	-0001	-0407	+0506	+0377	-8776	-1408	-0038
	4374	+0000	+0900	-0001	+0001	-0088	+0551	-8171	-1040	+0358
	4375	+0040	+0900	-0001	+0407	-0649	+0540	-5748	-2196	+0611
$W_4\ B\ C^R$	4376	+0080	+0900	-0001	+0815	-1375	+0630	-6365	-2942	+1037
$\xi_{-z} = +20^\circ$	4377	+0120	+0900	-0001	+1223	-2166	+0569	-4398	-4341	+1469
	4378	+0160	+0900	-0001	+1633	-3122	+0527	-4259	-4831	+2109
	4379	+0200	+0900	-0001	+2043	-4174	+0594	-2901	-2434	+2900
	4380	+0240	+0900	-0002	+2455	-5407	+1061	-2285	-3607	+3727
	4382	+0280	+0900	-0001	+2869	-6752	+0668	-0753	-4505	+4623
	4382	-0000	+0900	-0001	-0000	-0084	+0459	-8992	-3384	+0268
	4382	-0000	+0900	+0034	-0156	10000	+0000	+0000	+0000	+0000

Table 152

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4394	+0000	+1050	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4384	-0040	+1050	+0104	-0393	+0497	-0074	-0787	-0202	+0035
	4385	+0000	+1050	-0001	+0000	-0084	+0059	-0803	+0001	+0449
W_4 B C^R	4386	+0040	+1050	-0106	+0394	-0631	+0205	-0553	+0003	+0681
	4388	+0080	+1050	-0211	+0788	-1328	+0358	-0651	+0047	+1090
ξ_{-z} +20°	4388	+0120	+1050	-0315	+1181	-2081	+0527	-0266	+0025	+1508
	4390	+0160	+1050	-0418	+1577	-2974	+0747	+0257	+0124	+2088
	4390	+0200	+1050	-0520	+1972	-3931	+1018	+1447	+0374	+2780
	4392	+0240	+1050	-0621	+2369	-5012	+1410	+2580	+0837	+3483
	4392	+0280	+1050	-0719	+2764	-6098	+1821	+3761	+1210	+4072
	4393	+0000	+1050	-0001	+0000	-0078	+0066	-0892	-0301	+0379
	4393	+0000	+1050	+0038	-0153	+0000	+0000	+0000	+0000	+0000

Table 153

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4405	+0000	+1200	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4395	-0040	+1200	+0201	-0350	+0433	-0186	-0850	-0390	+0060
	4396	+0000	+1200	-0001	+0001	-0081	+0074	-0895	-0022	+0434
	4397	+0040	+1200	-0204	+0352	-0557	+0347	-0744	+0264	+0674
W_4 B C^R	4398	+0080	+1200	-0406	+0704	-1170	+0661	-0910	+0388	+1001
	4400	+0120	+1200	-0608	+1057	-1851	+1021	-0711	+0681	+1399
ξ_{-z} +20°	4400	+0160	+1200	-0808	+1408	-2564	+1460	-0257	+0974	+1785
	4402	+0200	+1200	-1006	+1757	-3341	+1984	+0109	+1533	+2266
	4402	+0240	+1200	-1200	+2105	-4163	+2539	+0884	+2007	+2746
	4404	+0280	+1200	-1391	+2451	-5043	+3172	+1570	+2561	+3287
	4404	+0000	+1200	-0001	+0000	-0070	+0077	-0946	-0192	+0385
	4404	+0000	+1200	+0040	-0146	+0000	+0000	+0000	+0000	+0000

Table 154

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4416	+0000	+1350	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4406	-0040	+1350	+0286	-0287	+0340	-0325	-0792	-0568	+0047
	4407	+0000	+1350	-0001	+0001	-0085	+0058	-0851	-0097	+0354
	4408	+0040	+1350	-0289	+0288	-0475	+0471	-0762	+0221	+0526
W_4 B C^R	4409	+0080	+1350	-0576	+0576	-0957	+0936	-0927	+0584	+0795
	4410	+0120	+1350	-0862	+0861	-1482	+1467	-1256	+1260	+1224
$\xi_{-z} = +20^\circ$	4411	+0160	+1350	-1146	+1145	-2114	+2083	-1392	+1957	+1599
	4412	+0200	+1350	-1429	+1428	-2742	+2739	-1482	+2615	+1919
	4413	+0240	+1350	-1709	+1708	-3453	+3429	-1273	+3303	+2244
	4414	+0280	+1350	-1983	+1983	-4209	+4175	-1256	+4090	+2666
	4415	+0000	+1350	-0001	+0000	-0082	+0062	-0939	-0305	+0265
	4415	+0000	+1350	+0041	-0141	+0000	+0000	+0000	+0000	+0000

Table 155

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4427	+0000	+1500	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4418	-0040	+1500	+0352	-0203	+0221	-0433	-0768	-0640	+0144
	4418	+0000	+1500	-0002	+0001	-0080	+0054	-0845	-0087	+0355
	4420	+0040	+1500	-0353	+0203	-0346	+0562	-0891	+0417	+0502
W_4 B C^R	4420	+0080	+1500	-0705	+0406	-0660	+1158	-1042	+0937	+0690
	4422	+0120	+1500	-1058	+0608	-1046	+1841	-1693	+1760	+0932
$\xi_{-z} = +20^\circ$	4422	+0160	+1500	-1409	+0808	-1516	+2580	-2495	+2765	+1360
	4424	+0200	+1500	-1760	+1006	-2081	+3370	-3354	+3741	+1802
	4424	+0240	+1500	-2107	+1201	-2686	+4184	-3957	+4646	+2078
	4426	+0280	+1500	-2451	+1391	-3313	+5066	-4635	+5722	+2386
	4426	+0000	+1500	-0001	+0000	-0077	+0062	-0938	-0161	+0344
	4426	+0000	+1500	+0039	-0135	+0000	+0000	+0000	+0000	+0000

Table 156

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4438	+0000	+1650	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4428	-0040	+1650	+0392	-0105	+0090	-0500	-0700	-0795	+0145
	4429	+0000	+1650	-0001	+0000	-0063	+0051	-0765	-0184	+0292
	4430	+0040	+1650	-0394	+0105	-0213	+0628	-0844	+0474	+0458
W_4 B C^R	4431	+0080	+1650	-0787	+0210	-0386	+1308	-1137	+1081	+0525
	4432	+0120	+1650	-1181	+0314	-0572	+2091	-1696	+1975	+0687
$\xi_{-z} = +20^\circ$	4433	+0160	+1650	-1575	+0417	-0818	+2960	-2622	+3058	+0935
	4434	+0200	+1650	-1970	+0519	-1153	+3926	-4138	+4437	+1289
	4435	+0240	+1650	-2365	+0619	-1567	+4995	-5760	+5819	+1700
	4436	+0280	+1650	-2759	+0717	-2052	+6121	-6983	+7096	+2073
	4437	-0000	+1650	-0000	+0000	-0067	+0067	-0900	-0366	+0252
	4438	-0000	+1650	+0037	-0118	+0000	+0000	+0000	+0000	+0000

Table 157

	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0005	-0004
	4449	+0000	+1800	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4440	-0040	+1800	+0406	-0000	-0297	-0534	-0697	-0816	+0249
	4440	+0000	+1800	-0002	+0000	-0519	+0036	-0788	-0154	+0301
	4441	+0040	+1800	-0408	+0000	-0769	+0631	-1001	+0454	+0366
W_4 B C^R	4442	+0080	+1800	-0817	+0001	-1287	+1351	-1351	+1310	+0529
	4443	+0120	+1800	-1224	+0001	-1821	+2168	-1700	+2261	+0666
$\xi_{-z} = +20^\circ$	4444	+0160	+1800	-1633	+0001	-2296	+3105	-2064	+3500	+0891
	4445	+0200	+1800	-2043	+0002	-3043	+4158	-2247	+4914	+1124
	4446	+0240	+1800	-2456	+0001	-2310	+5328	-2475	+6297	+1110
	4447	+0280	+1800	-2869	+0001	-2839	+6662	-2670	+7841	+1162
	4448	-0000	+1800	+0000	+0000	-0390	+0046	-0918	-0373	+0237
	4448	-0000	+1800	+0036	-0111	+0000	+0000	+0000	+0000	+0000

Table 158

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
$W_4\ B\ C^F$ $\xi_{-z} = 0^\circ$	0000	-0001	-0001	-0002	-0002	-0006	-0004	-0006	-0005	-0005
	4460	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4450	-0040	+0000	-0406	+0000	-0708	+0579	-1338	+0535	+0280
	4451	+0000	+0000	-0000	+0000	-0669	+0031	-1203	-0031	+0160
	4452	+0040	+0000	+0408	+0000	-1129	-0542	-0916	-0514	+0176
	4454	+0080	+0000	+0814	+0000	-0643	-1243	-0470	-1151	+0137
	4454	+0120	+0000	+1222	+0000	-1963	-2037	+0438	-1957	-0131
	4456	+0160	+0000	+1633	+0000	-0862	-2956	+1036	-2724	+0528
	4456	+0200	+0000	+2043	+0001	-6512	-4005	+1334	-3664	+0745
	4458	+0240	+0000	+2455	+0001	-6150	-5143	+3438	-4832	-0242
	4458	+0280	+0000	+2869	+0001	-5341	-6431	+6600	-6109	-0539
	4460	+0000	+0000	-0001	+0000	+0210	+0010	-2190	-0484	-1412
	4460	+0000	+0000	-0071	+0047	+0000	+0000	+0000	+0000	+0000

Table 159

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
$W_4\ B\ C^F$ $\xi_{-z} = 0^\circ$	0000	-0001	-0001	-0002	-0002	-0006	-0004	-0006	-0005	-0005
	4460	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4450	-0040	+0000	-0406	+0000	-0708	+0579	-1338	+0535	+0280
	4451	+0000	+0000	-0000	+0000	-0669	+0031	-1203	-0031	+0160
	4452	+0040	+0000	+0408	+0000	-1129	-0542	-0916	-0514	+0176
	4454	+0080	+0000	+0814	+0000	-0643	-1243	-0470	-1151	+0137
	4454	+0120	+0000	+1222	+0000	-1963	-2037	+0438	-1957	-0131
	4456	+0160	+0000	+1633	+0000	-0862	-2956	+1036	-2724	+0528
	4456	+0200	+0000	+2043	+0001	-6512	-4005	+1334	-3664	+0745
	4458	+0240	+0000	+2455	+0001	-6150	-5143	+3438	-4832	-0242
	4458	+0280	+0000	+2869	+0001	-5341	-6431	+6600	-6109	-0539
	4460	+0000	+0000	-0001	+0000	+0210	+0010	-2190	-0484	-1412
	4460	+0000	+0000	-0071	+0047	+0000	+0000	+0000	+0000	+0000

Table 160

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	4471	+0000	+0150	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4461	-0040	+0150	-0392	-0105	+0124	+0580	-0065	+0768	+0682
	4462	+0000	+0150	+0001	+0000	-0012	+0034	-0006	+0165	+0794
	4463	+0040	+0150	+0393	+0105	-0150	-0512	+0069	-0305	+1410
$W_4\ B\ C^F$	4464	+0080	+0150	+0787	+0210	-0284	-1184	+0189	-0979	+1353
	4465	+0120	+0150	+1180	+0314	-0459	-1931	+0489	-1692	+1496
$\xi_{-z} = 0^\circ$	4466	+0160	+0150	+1575	+0417	-0685	-2794	+1119	-2370	+2389
	4468	+0200	+0150	+1969	+0519	-0998	-3730	+2139	-2972	+4524
	4468	+0240	+0150	+2366	+0619	-1330	-4767	+3625	-3738	+5950
	4470	+0280	+0150	+2760	+0717	-1761	-5840	+4827	-4605	+8058
	4470	+0000	+0150	-0000	+0000	-0011	+0016	-0062	+0042	+0663
	4470	+0000	+0150	-0070	+0041	+0000	+0000	+0000	+0000	+0000

Table 161

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4482	+0000	+0300	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4472	-0040	+0300	-0351	-0203	+0255	+0512	-0079	+0922	+0047
	4473	+0000	+0300	+0000	-0000	-0004	+0028	+0010	+0420	+0151
	4474	+0040	+0300	+0352	+0203	-0286	-0446	+0098	-0092	+0249
$W_4\ B\ C^F$	4470	+0080	+0300	+0704	+0405	-0586	-1027	+0169	-0570	+0343
	4470	+0120	+0300	+1056	+0607	-0915	-1676	+0525	-1015	+0428
$\xi_{-z} = 0^\circ$	4478	+0160	+0300	+1408	+0807	-1362	-2402	+1029	-1417	+0655
	4478	+0200	+0300	+1758	+1005	-1884	-3159	+1740	-1927	+0928
	4480	+0240	+0300	+2107	+1200	-2476	-3957	+2319	-2325	+1249
	4480	+0280	+0300	+2453	+1392	-3119	-4795	+2957	-2940	+1559
	4482	+0000	+0300	+0000	-0000	-0019	+0016	-0020	+0471	+0197
	4481	+0000	+0300	-0065	+0031	+0000	+0000	+0000	+0000	+0000

Table 162

W_4 B C^F

$\xi_{-z} = 0°$

Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
4495	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4483	-0040	+0450	-0287	-0287	+0381	+0435	-1043	+0922	+0083
4484	+0000	+0450	-0000	-0000	-0005	+0041	+0136	+0517	+0219
4486	+0040	+0450	+0287	+0287	-0396	-0336	+1477	+0147	+0389
4486	+0080	+0450	+0574	+0574	-0845	-0776	+2497	-0189	+0546
4488	+0120	+0450	+0861	+0860	-1355	-1284	+3391	-0359	+0791
4488	+0160	+0450	+1146	+1145	-1951	-1879	+5029	-0545	+1141
4490	+0200	+0450	+1428	+1428	-2610	-2515	+5936	-0948	+1441
4490	+0240	+0450	+1708	+1707	-3297	-3215	+7568	-1431	+1750
4491	+0280	+0450	+1983	+1983	-4043	-3952	+9827	-1907	+2121
4492	-0000	+0450	-0001	-0001	-0009	+0036	+0607	+0678	+0319
4492	-0000	+0450	-0062	+0025	+0000	+0000	+0000	+0000	+0000

Table 163

W_4 B C^F

$\xi_{-z} = 0°$

0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
4504	+0000	+0600	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4494	-0040	+0600	-0203	-0353	+0520	+0308	-0264	+0652	-0089
4495	+0000	+0600	+0000	+0000	+0014	+0043	-0033	+0278	+0120
4496	+0040	+0600	+0203	+0352	-0481	-0215	+0069	+0048	+0353
4498	+0080	+0600	+0405	+0704	-1061	-0511	+0216	-0173	+0592
4498	+0120	+0600	+0607	+1057	-1717	-0838	+0095	-0219	+0917
4500	+0160	+0600	+0807	+1407	-2439	-1276	-0156	-0401	+1278
4500	+0200	+0600	+1005	+1758	-3210	-1791	-0510	-0607	+1725
4502	+0240	+0600	+1201	+2106	-4025	-2367	-0922	-0781	+2164
4502	+0280	+0600	+1392	+2452	-4871	-3020	-1101	-1307	+2521
4504	+0000	+0600	-0000	-0001	+0019	+0032	-0020	+0405	+0212
4504	+0000	+0600	-0058	+0023	+0000	+0000	+0000	+0000	+0000

Table 164

W_4 B C^F

$\xi_{-z} = 0°$

Exponent / Configuration	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0004
	4517	+0000	+0750	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4506	-0040	+0750	-0105	-0394	+0561	+0165	-0119	+4556	-0114
	4506	+0000	+0750	-0000	+0001	+0016	+0041	-0034	+2207	+0125
	4508	+0040	+0750	+0105	+0393	-0538	-0088	+0067	+0828	+0368
	4508	+0080	+0750	+0209	+0786	-1208	-0226	+0166	-0302	+0680
	4509	+0120	+0750	+0313	+1181	-1972	-0393	+0137	-0759	+1062
	4510	+0160	+0750	+0417	+1577	-2634	-0012	-0225	-0835	+1530
	4511	+0200	+0750	+0519	+1972	-3788	-0091	-1106	-1215	+2012
	4512	+0240	+0750	+0620	+2370	-4850	-1248	-2029	-2491	+2536
	4513	+0280	+0750	+0717	+2762	-5954	-1662	-2922	-4867	+3043
	4514	+0000	+0750	-0000	-0001	+0017	+0033	-0062	+2651	+0171
	4514	+0000	+0750	-0003	+0017	+0000	+0000	+0000	+0000	+0000

Table 165

W_4 B C^F

$\xi_{-z} = 0°$

0000	-0001	-0001	-0002	-0002	-0004	-0006	-0005	-0006	-0004
4530	+0000	+0900	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4520	-0040	+0900	-0000	-0408	+0593	+4392	-0135	+4683	-0081
4521	+0000	+0900	-0000	+0000	+0019	+4713	-0049	+3881	+0173
4522	+0040	+0900	-0000	+0407	-0553	+4160	+0065	+3362	+0435
4524	+0080	+0900	-0000	+0814	-1251	+2740	+0210	+3094	+0764
4524	+0120	+0900	-0000	+1222	-2047	+2413	+0354	+2255	+1157
4526	+0160	+0900	+0000	+1632	-2968	+1964	+0505	+2541	+1715
4526	+0200	+0900	+0000	+2044	-4014	-0782	+0716	+3362	+2292
4528	+0240	+0900	-0000	+2461	-5187	+5739	+0969	+2401	+2859
4528	+0280	+0900	+0000	+2872	-6495	+0864	+1222	+1406	+3495
0050	+0003	+0050	+0500	+0500	+ 250	- 4	- 175	- 4	+ 1
0050	+0003	+0050	+0500	+0500	+ 1	- 4	- 175	- 4	+ 1

Table 166

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4541	+0000	+1050	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4531	-0040	+1050	+0105	-0393	+0582	-0067	-0072	+0418	-0009
	4532	+0000	+1050	-0001	+0001	+0032	+0053	+0004	+0463	+0229
	4533	+0040	+1050	-0105	+0391	-0511	+0196	+0111	+0466	+0461
$W_4\ B\ C^F$	4534	+0080	+1050	-0210	+0784	-1175	+0313	+0217	+0398	+0717
	4535	+0120	+1050	-0314	+1180	-1937	+0474	+0557	+0369	+1053
$\xi_{-z} = 0^\circ$	4536	+0160	+1050	-0417	+1575	-2793	+0687	+1205	+0403	+1491
	4538	+0200	+1050	-0519	+1969	-3729	+0974	+2423	+0636	+1957
	4538	+0240	+1050	-0618	+2363	-4772	+1327	+3612	+1014	+2559
	4540	+0280	+1050	-0716	+2757	-5865	+1731	+4850	+1270	+3059
	4540	+0000	+1050	-0000	-0001	+0041	+0051	-0009	+0195	+0117
	4540	+0000	+1050	-0025	+0011	+0000	+0000	+0000	+0000	+0000

Table 167

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4552	+0000	+1200	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4542	-0040	+1200	+0203	-0354	+0521	-0220	-0016	+0490	+0096
	4543	+0000	+1200	-0000	+0000	+0029	+0036	+0070	+0562	+0260
	4544	+0040	+1200	-0203	+0352	-0440	+0306	+0170	+0711	+0475
$W_4\ B\ C^F$	4545	+0080	+1200	-0406	+0704	-1028	+0606	+0212	+0767	+0679
	4546	+0120	+1200	-0607	+1056	-1677	+0943	+0560	+0823	+0939
$\xi_{-z} = 0^\circ$	4547	+0160	+1200	-0808	+1409	-2401	+1373	+1023	+1184	+1304
	4548	+0200	+1200	-1006	+1757	-3158	+1897	+1529	+1715	+1719
	4549	+0240	+1200	-1200	+2106	-3964	+2451	+2209	+2237	+2117
	4550	+0280	+1200	-1392	+2452	-4804	+3092	+2702	+2856	+2564
	4551	-0000	+1200	+0001	-0002	+0033	+0035	+0083	+0614	+0305
	4551	-0000	+1200	-0019	+0002	+0000	+0000	+0000	+0000	+0000

Table 168

W_4 B C^F

$\xi_{-z} = 0°$

Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
4563	+0000	+1350	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4553	-0040	+1350	+0288	-0289	+0433	-0529	-0826	+0392	+0116
4554	+0000	+1350	-0001	+0001	+0036	+0042	-0168	+0506	+0228
4556	+0040	+1350	-0288	+0287	-0353	+0440	+1156	+0783	+0389
4556	+0080	+1350	-0575	+0574	-0798	+0894	+1879	+1009	+0516
4558	+0120	+1350	-0862	+0861	-1312	+1410	+2037	+1429	+0736
4558	+0160	+1350	-1146	+1145	-1880	+1984	+1521	+2021	+1062
4560	+0200	+1350	-1429	+1428	-2513	+2636	+0798	+2630	+1396
4560	+0240	+1350	-1708	+1707	-3226	+3305	+3119	+3260	+1748
4562	+0280	+1350	-1984	+1983	-3958	+4038	+3119	+3932	+2064
4562	+0000	+1350	-0001	-0000	+0039	+0048	+0037	+0561	+0283
4562	+0000	+1350	-0017	-0000	+0000	+0000	+0000	+0000	+0000

Table 169

W_4 B C^F

$\xi_{-z} = 0°$

0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
4574	+0000	+1500	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4564	-0040	+1500	+0351	-0203	+0318	-0429	-0063	+0037	+0073
4565	+0000	+1500	-0002	+0000	+0040	+0046	-0048	+0368	+0173
4566	+0040	+1500	-0354	+0203	-0223	+0533	-0019	+0829	+0317
4567	+0080	+1500	-0705	+0405	-0504	+1124	-0005	+1324	+0423
4568	+0120	+1500	-1058	+0607	-0846	+1785	-0237	+1845	+0468
4569	+0160	+1500	-1409	+0806	-1268	+2499	-0701	+2572	+0691
4570	+0200	+1500	-1759	+1004	-1774	+3261	-1294	+3375	+0969
4571	+0240	+1500	-2107	+1200	-2360	+4047	-1670	+4170	+1303
4572	+0280	+1500	-2454	+1391	-3006	+4687	-2133	+4865	+1593
4573	+0000	+1500	-0001	-0000	+0032	+0061	-0041	+0691	+0303
4574	+0000	+1500	-0013	-0002	+0000	+0000	+0000	+0000	+0000

Table 170

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	4585	+0000	+1650	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4576	-0040	+1650	+0391	-0105	+0167	-0501	-0030	-0192	+0350
	4576	+0000	+1650	-0000	-0000	+0036	+0032	-0018	+0118	+0277
$W_4\ B\ C^F$	4578	+0040	+1650	-0394	+0105	-0094	+0587	+0025	+0605	+1208
	4578	+0080	+1650	-0789	+0209	-0227	+1274	-0005	+1160	+1264
	4580	+0120	+1650	-1183	+0313	-0384	+2034	-0189	+1789	+1292
$\xi_{-z} = 0^\circ$	4580	+0160	+1650	-1577	+0416	-0583	+2877	-0815	+2654	+2056
	4582	+0200	+1650	-1973	+0518	-0866	+3819	-1854	+3606	+3204
	4582	+0240	+1650	-2364	+0617	-1213	+4859	-3162	+4727	+5138
	4583	+0280	+1650	-2757	+0715	-1632	+5952	-4186	+5541	+7082
	4584	+0000	+1650	-0000	-0000	+0047	+0040	+0010	-0011	-0248
	4584	+0000	+1650	-0012	-0001	+0000	+0000	+0000	+0000	+0000

Table 171

	0000	-0001	-0001	-0002	-0002	-0006	-0004	-0006	-0005	-0005
	4596	+0000	+1800	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4586	-0040	+1800	+0406	-0001	+5363	-0538	-0322	-0367	+0139
	4587	+0000	+1800	-0000	-0001	+5149	+0021	-0321	+0003	-0137
$W_4\ B\ C^F$	4588	+0040	+1800	-0408	-0001	+4757	+0601	-0321	+0452	-0287
	4589	+0080	+1800	-0815	-0001	+4808	+1297	-0464	+1092	-0388
	4590	+0120	+1800	-1224	-0001	+5194	+2092	-1204	+1834	-0615
$\xi_{-z} = 0^\circ$	4591	+0160	+1800	-1636	-0001	+5751	+3007	-1501	+2802	-0178
	4592	+0200	+1800	-2046	-0000	+2693	+4036	-0501	+3894	+0365
	4593	+0240	+1800	-2459	-0001	+9635	+5197	-1359	+4975	+0156
	4594	+0280	+1800	-2873	-0001	+5261	+6496	-2075	+6100	-0582
	4595	+0000	+1800	-0000	-0000	+5538	+0024	-0810	-0196	-1003
	4596	+0000	+1800	-0009	-0002	+0000	+0000	+0000	+0000	+0000

Table 172

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0006	-0004	-0006	-0005	-0005
	4607	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4598	-0040	+0000	-0408	-0001	+7916	+0612	+3125	+0507	-2177
	4598	+0000	+0000	+0000	-0000	+5605	+0044	+2532	-0009	-1798
	4599	+0040	+0000	+0407	-0000	+4808	-0517	+2239	-0504	-1473
W_4 B C^F	4600	+0080	+0000	+0813	-0000	+4043	-1220	+2375	-1187	-1438
	4601	+0120	+0000	+1224	-0000	+2319	-2018	+2524	-1981	-1463
$\xi_{-z} = -20^\circ$	4602	+0160	+0000	+1632	-0000	+1868	-2938	+1932	-2795	-0766
	4603	+0200	+0000	+2043	+0001	-4680	-3977	+1079	-3850	-0442
	4604	+0240	+0000	+2456	+0001	-4636	-5119	+2566	-4930	-0625
	4606	+0280	+0000	+2870	+0001	-4961	-6417	+4956	-6170	-1000
	4606	+0000	+0000	-0001	-0000	+6390	+0035	+1302	-0412	-3234
	4606	+0000	+0000	-0068	+0049	+0000	+0000	+0000	+0000	+0000

Table 173

Configuration / Exponent										
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	4618	+0000	+0150	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4608	-0040	+0150	-0393	-0105	+0143	+0590	+0382	+0795	-1410
	4609	+0000	+0150	-0000	-0000	+0025	+0046	+0534	+0296	-1046
	4610	+0040	+0150	+0393	+0105	-0139	-0502	+0579	-0228	-0476
W_4 B C^F	4612	+0080	+0150	+0786	+0210	-0289	-1162	+0703	-0842	-0249
	4612	+0120	+0150	+1180	+0314	-0457	-1917	+0975	-1608	+0022
$\xi_{-z} = -20^\circ$	4614	+0160	+0150	+1575	+0417	-0693	-2786	+1519	-2360	+0854
	4614	+0200	+0150	+1970	+0519	-1027	-3717	+2456	-3082	+2894
	4616	+0240	+0150	+2364	+0619	-1391	-4752	+3771	-3858	+4886
	4616	+0280	+0150	+2759	+0717	-1815	-5826	+4920	-4703	+6635
	4618	+0000	+0150	-0000	+0000	+0017	+0034	+0515	+0136	-1762
	4617	+0000	+0150	-0064	+0043	+0000	+0000	+0000	+0000	+0000

Table 174

Configuration \ Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4636	+0000	+0300	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4626	-0040	+0300	-0352	-0203	+0318	+0522	+0237	+0888	-0082
	4627	+0000	+0300	+0001	-0000	+0056	+0048	+0386	+0396	-0045
	4628	+0040	+0300	+0352	+0203	-0218	-0435	+0398	-0064	+0122
W_4 B C^F	4630	+0080	+0300	+0703	+0405	-0521	-1009	+0519	-0605	+0192
	4630	+0120	+0300	+1055	+0606	-0856	-1668	+0909	-1120	+0246
$\xi_{-z} = -20^\circ$	4632	+0160	+0300	+1407	+0806	-1304	-2379	+1390	-1624	+0457
	4632	+0200	+0300	+1757	+1004	-1834	-3147	+2051	-2072	+0784
	4634	+0240	+0300	+2106	+1200	-2440	-3947	+2547	-2604	+1097
	4634	+0280	+0300	+2452	+1391	-3082	-4790	+3103	-3199	+1423
	4636	+0000	+0300	+0001	-0000	+0057	+0035	+0341	+0396	-0001
	4635	+0000	+0300	-0058	+0035	+0000	+0000	+0000	+0000	+0000

Table 175

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4647	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4637	-0040	+0450	-0287	-0288	+0432	+0442	+0194	+0880	-0079
	4638	-0000	+0450	-0001	-0001	+0045	+0054	+0508	+0387	-0054
	4640	+0040	+0450	+0286	+0287	-0360	-0319	+0584	+0013	+0182
W_4 B C^F	4640	+0080	+0450	+0574	+0574	-0826	-0769	+0731	-0366	+0367
	4642	+0120	+0450	+0860	+0860	-1316	-1273	+0909	-0539	+0552
$\xi_{-z} = -20^\circ$	4642	+0160	+0450	+1144	+1144	-1902	-1864	+1176	-0799	+0818
	4644	+0200	+0450	+1427	+1427	-2545	-2503	+1279	-1218	+1086
	4644	+0240	+0450	+1708	+1707	-3245	-3219	+1488	-1611	+1448
	4645	+0280	+0450	+1982	+1981	-3991	-3942	+1576	-2177	+1792
	4646	+0000	+0450	-0000	-0001	+0044	+0045	+0526	+0458	+0053
	4646	+0000	+0450	-0058	+0025	+0000	+0000	+0000	+0000	+0000

Table 176

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	4658	+0000	+0600	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4648	-0040	+0600	-0203	-0351	+0534	+0321	+2170	+0605	-0228
	4649	+0000	+0600	+0000	+0000	+0070	+0054	+5186	+0278	-0138
$W_4\ B\ C^F$	4650	+0040	+0600	+0202	+0351	-0433	-0210	+6068	+0003	+0143
	4652	+0080	+0600	+0405	+0704	-1022	-0501	+7940	-0256	+0364
$\xi_{-z} = -20^\circ$	4652	+0120	+0600	+0607	+1057	-1673	-0832	+8089	-0443	+0630
	4654	+0160	+0600	+0807	+1408	-2367	-1274	+6949	-0543	+0915
	4654	+0200	+0600	+1005	+1758	-3113	-1794	+5516	-0774	+1247
	4656	+0240	+0600	+1201	+2106	-3897	-2364	+1922	-1017	+1600
	4656	+0280	+0600	+1393	+2453	-4726	-3028	-0096	-1561	+1950
	4658	+0000	+0600	+0000	+0000	+0073	+0040	+5198	+0325	-0071
	4658	+0000	+0600	-0053	+0019	+0000	+0000	+0000	+0000	+0000

Table 177

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0004
	4669	+0000	+0750	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4660	-0040	+0750	-0105	-0392	+0590	+0183	+0134	+4090	-0294
	4660	+0000	+0750	-0001	-0001	+0086	+0058	+0411	+1860	-0160
	4662	+0040	+0750	+0104	+0392	-0479	-0075	+0498	+0285	+0128
$W_4\ B\ C^F$	4662	+0080	+0750	+0209	+0786	-1150	-0211	+0643	-1390	+0405
	4663	+0120	+0750	+0313	+1179	-1880	-0371	+0745	-3009	+0715
$\xi_{-z} = -20^\circ$	4664	+0160	+0750	+0416	+1575	-2725	-0596	+0643	-3045	+1071
	4665	+0200	+0750	+0518	+1969	-3617	-0874	+0054	-4144	+1399
	4666	+0240	+0750	+0619	+2365	-4592	-1246	-0566	-5458	+1757
	4667	+0280	+0750	+0717	+2760	-5661	-1649	-1173	-8454	+2138
	4668	+0000	+0750	-0001	-0001	+0076	+0050	+0372	+0747	-0199
	4668	+0000	+0750	-0048	+0016	+0000	+0000	+0000	+0000	+0000

Table 178

W_4 B C^F

$\xi_{-z} = -20°$

Exponent / Configuration	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0006	-0005	-0006	-0004
	4680	+0000	+0900	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4670	-0040	+0900	-0001	-0405	+0626	+5436	+0164	-0127	-0448
	4671	+0000	+0900	-0001	+0001	+0094	+5138	+0469	-0753	-0279
	4672	+0040	+0900	-0001	+0407	-0475	+4317	+0584	-1340	+0021
	4674	+0080	+0900	-0001	+0815	-1160	+3398	+0757	-2200	+0327
	4674	+0120	+0900	-0001	+1223	-1927	+2750	+1078	-3499	+0627
	4676	+0160	+0900	-0001	+1633	-2824	+1140	+1487	-4107	+1033
	4676	+0200	+0900	-0000	+2043	-3817	-0332	+1999	-3637	+1520
	4678	+0240	+0900	-0001	+2457	-4954	+3920	+2350	-5532	+2000
	4678	+0280	+0900	-0001	+2870	-6233	+1282	+2862	-6392	+2542
	4679	+0000	+0900	-0001	-0000	+0096	+3769	+0457	-4842	-0424
	4680	+0000	+0900	-0032	+0010	+0000	+0000	+0000	+0000	+0000

Table 179

W_4 B C^F

$\xi_{-z} = -20°$

0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0004
4691	+0000	+1050	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4681	-0040	+1050	+0104	-0392	+0612	-0066	+0119	+1657	-0248
4682	+0000	+1050	-0001	-0001	+0088	+0068	+0408	+1151	-0163
4683	+0040	+1050	-0106	+0392	-0459	+0195	+0545	+1825	+0111
4684	+0080	+1050	-0210	+0785	-1107	+0319	+0745	+1122	+0368
4685	+0120	+1050	-0314	+1178	-1826	+0476	+1268	-0617	+0584
4686	+0160	+1050	-0417	+1572	-2649	+0702	+2100	-0090	+0903
4688	+0200	+1050	-0518	+1967	-3553	+0953	+3638	+1363	+1372
4688	+0240	+1050	-0619	+2361	-4573	+1315	+4902	+3796	+1841
4690	+0280	+1050	-0717	+2756	-5637	+1716	+6212	+6328	+2264
0050	+0003	+0050	+0500	+0500	+ 250	+ 1	- 175	- 4	+ 1
0050	+0003	+0050	+0500	+0500	+ 1	+ 1	- 175	- 4	+ 1

Table 180

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4702	+0000	+1200	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4692	-0040	+1200	+0203	-0353	+0574	-0201	+0076	+0371	-0070
	4693	+0000	+1200	-0000	-0001	+0098	+0055	+0329	+0441	+0020
W_4 B C^F	4694	+0040	+1200	-0204	+0351	-0370	+0323	+0477	+0612	+0216
	4695	+0080	+1200	-0406	+0702	-0931	+0622	+0627	+0714	+0442
$\xi_{-z} = -20^\circ$	4696	+0120	+1200	-0608	+1055	-1557	+0950	+1117	+0685	+0604
	4697	+0160	+1200	-0808	+1406	-2235	+1378	+1848	+1072	+0883
	4698	+0200	+1200	-1006	+1757	-2944	+1903	+2593	+1572	+1184
	4699	+0240	+1200	-1200	+2103	-3720	+2461	+3456	+1945	+1464
	4700	+0280	+1200	-1391	+2449	-4551	+3072	+4202	+2434	+1795
	4701	+0000	+1200	-0000	-0001	+0101	+0060	+0344	+0490	+0027
	4701	+0000	+1200	-0014	+0005	+0000	+0000	+0000	+0000	+0000

Table 181

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4713	+0000	+1350	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4703	-0040	+1350	+0287	-0288	+0480	-0314	+0157	+0522	+0055
	4704	+0000	+1350	-0001	+0000	+0098	+0050	+0335	+0705	+0108
	4706	+0040	+1350	-0287	+0285	-0266	+0436	+0529	+0923	+0215
W_4 B C^F	4705	+0080	+1350	-0574	+0572	-0700	+0887	+0679	+1173	+0333
	4708	+0120	+1350	-0861	+0859	-1171	+1399	+0829	+1529	+0451
$\xi_{-z} = -20^\circ$	4708	+0160	+1350	-1146	+1143	-1728	+1983	+1083	+2007	+0663
	4710	+0200	+1350	-1428	+1425	-2320	+2609	+1247	+2617	+0887
	4710	+0240	+1350	-1706	+1704	-2997	+3277	+1636	+3139	+1130
	4712	+0280	+1350	-1982	+1979	-3693	+4013	+1788	+3728	+1334
	4712	+0000	+1350	+0000	-0002	+0104	+0053	+0325	+0899	+0189
	4712	+0000	+1350	-0011	+0000	+0000	+0000	+0000	+0000	+0000

Table 182

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0005
	4724	+0000	+1500	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4714	-0040	+1500	+0350	-0203	+0354	-0414	+2507	+0216	-0412
	4715	+0000	+1500	-0001	-0001	+0101	+0049	+3554	+0474	-0056
	4716	+0040	+1500	-0352	+0201	-0134	+0533	+5486	+0863	+0674
W_4 B C^F	4717	+0080	+1500	-0704	+0404	-0414	+1118	+6530	+1353	+0976
	4718	+0120	+1500	-1056	+0605	-0709	+1777	+5931	+1872	+1312
$\xi_{-z} = -20^\circ$	4719	+0160	+1500	-1407	+0805	-1111	+2481	+3389	+2488	+2106
	4720	+0200	+1500	-1757	+1002	-1573	+3243	-0497	+3175	+3749
	4721	+0240	+1500	-2105	+1197	-2137	+4010	-1966	+3827	+5799
	4722	+0280	+1500	-2451	+1388	-2776	+4843	-3163	+4393	+7339
	4723	+0000	+1500	-0001	-0001	+0100	+0063	+3961	+0734	+0965
	4724	+0000	+1500	-0009	-0004	+0000	+0000	+0000	+0000	+0000

Table 183

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	4735	+0000	+1650	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4726	-0040	+1650	+0393	-0106	+0210	-0505	+0181	+0077	-0330
	4726	+0000	+1650	-0001	-0001	+0092	+0031	+0293	+0418	-0405
	4728	+0040	+1650	-0393	+0104	-0014	+0583	+0475	+0898	-0462
W_4 B C^F	4728	+0080	+1650	-0786	+0208	-0126	+1259	+0589	+1548	-0816
	4730	+0120	+1650	-1182	+0312	-0250	+2015	+0546	+2208	-1294
$\xi_{-z} = -20^\circ$	4730	+0160	+1650	-1576	+0414	-0427	+2865	+0174	+3116	-0918
	4731	+0200	+1650	-1970	+0516	-0671	+3793	-0674	+4071	-0535
	4732	+0240	+1650	-2365	+0616	-0985	+4844	-1795	+4974	-0147
	4733	+0280	+1650	-2759	+0714	-1374	+5928	-2692	+5849	+0242
	4734	+0000	+1650	-0001	-0001	+0081	+0033	+0262	+0460	-0283
	4734	+0000	+1650	-0007	-0006	+0000	+0000	+0000	+0000	+0000

Table 184

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0006	-0005	-0005
	4742	+0000	+1800	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4736	-0040	+1800	+0406	-0001	+0933	-0505	+1895	-0042	+0742
	4737	+0000	+1800	-0000	-0001	+0968	+0042	+2031	+0336	+0091
	4738	+0040	+1800	-0405	-0001	+1114	+0612	+2922	+0774	-0399
W_4 B C^F	4739	+0080	+1800	-0813	-0001	+1305	+1324	+3947	+1361	-1260
	4740	+0120	+1800	-1222	-0001	+1558	+2115	+5283	+2148	-1956
$\xi_{-z} = -20^\circ$	4741	+0160	+1800	-1631	-0002	+2077	+3023	+6748	+3138	-2427
	0742	+0200	+1800	-2042	-0002	+2091	+4021	+9093	+3974	-3076
	1742	+0240	+1800	-2455	-0003	+2971	+5172	+9105	+4812	-4800
	2742	+0280	+1800	-2868	-0002	+2839	+6449	+9086	+5869	-5530
	3742	-0000	+1800	+0000	-0001	+1042	+0051	+0386	+0012	-0796
	3742	-0000	+1800	-0036	+0005	+0000	+0000	+0000	+0000	+0000

Table 185

	0000	-0001	-0001	-0002	-0002	-0006	-0004	-0006	-0005	-0008
	4753	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4744	-0040	+0000	-0406	+0001	-7764	+0598	-5514	+0507	+1742
	4744	+0000	+0000	+0002	+0001	-6635	+0032	-4230	-0016	+1342
	4745	+0040	+0000	+0406	+0000	-5773	-0527	-3253	-0492	+1097
W_4 B C^F	4746	+0080	+0000	+0814	+0001	-6031	-1219	-2532	-1154	+0904
	4747	+0120	+0000	+1223	+0001	-5659	-2028	-1381	-1943	+0692
$\xi_{-z} = +20^\circ$	4748	+0160	+0000	+1633	+0000	-3248	-2946	+0351	-2812	+0443
	4749	+0200	+0000	+2044	+0001	-6595	-3997	+1784	-3817	-0014
	4750	+0240	+0000	+2458	+0001	-4868	-5149	+3983	-4774	-0296
	4752	+0280	+0000	+2870	+0001	-4276	-6424	+6764	-6116	-0950
	0050	+0003	+0050	+0500	+0500	-4680	+ 1	- 4	- 175	- 175
	0050	+0003	+0050	+0500	+0500	- 4	+ 1	- 4	- 175	- 175

Table 186

Configuration / Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4775	+0000	+0300	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4765	-0040	+0300	-0351	-0202	+0178	+0520	-0537	+0528	+0155
	4766	+0000	+0300	+0001	+0001	-0062	+0030	-0387	+0111	+0220
	4767	+0040	+0300	+0352	+0204	-0318	-0446	-0138	-0312	+0281
W_4 B C^F	4768	+0080	+0300	+0704	+0406	-0597	-1033	-0007	-0836	+0335
	4770	+0120	+0300	+1057	+0608	-0941	-1682	+0370	-1420	+0380
$\xi_{-z} = +20°$	4770	+0160	+0300	+1408	+0808	-1387	-2401	+0905	-1915	+0542
	4772	+0200	+0300	+1759	+1006	-1902	-3172	+1676	-2328	+0848
	4772	+0240	+0300	+2108	+1202	-2500	-3957	+2287	-2836	+1116
	4774	+0280	+0300	+2454	+1393	-3140	-4794	+3001	-3423	+1376
	4774	+0000	+0300	-0000	+0000	-0060	+0013	-0398	+0003	+0166
	4774	+0000	+0300	-0052	+0030	+0000	+0000	+0000	+0000	+0000

Table 187

	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0005
	4764	+0000	+0150	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4754	-0040	+0150	-0394	-0104	+0014	+0578	-0644	+0501	+1953
	4755	+0000	+0150	-0000	+0001	-0086	+0033	-0467	+0016	+1900
	4756	+0040	+0150	+0393	+0106	-0206	-0513	-0247	-0474	+2076
W_4 B C^F	4758	+0080	+0150	+0787	+0211	-0340	-1181	-0084	-1113	+1751
	4758	+0120	+0150	+1181	+0314	-0493	-1955	+0297	-1832	+1481
$\xi_{-z} = +20°$	4760	+0160	+0150	+1577	+0418	-0713	-2812	+1015	-2642	+1462
	4760	+0200	+0150	+1971	+0520	-1028	-3741	+2110	-3416	+2273
	4762	+0240	+0150	+2367	+0620	-1354	-4794	+3570	-4219	+3595
	4762	+0280	+0150	+2762	+0718	-1788	-5872	+4831	-5048	+5369
	4764	+0000	+0150	-0000	+0001	-0083	+0007	-0493	-0439	-0588
	4763	+0000	+0150	-0057	+0037	+0000	+0000	+0000	+0000	+0000

Table 188

W_4 B C^F

$\xi_{-z} = +20°$

Configuration \ Exponent	Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
	4786	+0000	+0450	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4776	-0040	+0450	-0288	-0286	+0288	+0458	-5663	+0382	+0080
	4777	+0000	+0450	+0001	+0002	-0086	+0064	-4072	+0069	+0202
	4778	+0040	+0450	+0288	+0289	-0454	-0308	-1485	-0274	+0354
	4780	+0080	+0450	+0574	+0575	-0898	-0769	+0528	-0690	+0427
	4780	+0120	+0450	+0860	+0862	-1413	-1261	+1246	-0955	+0654
	4782	+0160	+0450	+1145	+1146	-2025	-1853	+1678	-1232	+1004
	4782	+0200	+0450	+1429	+1430	-2678	-2494	+2110	-1584	+1314
	4784	+0240	+0450	+1708	+1710	-3369	-3185	+4433	-1981	+1650
	4784	+0280	+0450	+1984	+1985	-4115	-3922	+6458	-2450	+1957
	4786	+0000	+0450	-0000	+0001	-0092	+0064	-3840	-0007	+0208
	4785	+0000	+0450	-0048	+0026	+0000	+0000	+0000	+0000	+0000

Table 189

W_4 B C^F

$\xi_{-z} = +20°$

0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
4797	+0000	+0600	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4788	-0040	+0600	-0203	-0351	+0433	+0305	-0652	+0413	+0071
4788	+0000	+0600	+0000	+0001	-0053	+0048	-0517	+0124	+0234
4790	+0040	+0600	+0203	+0352	-0514	-0211	-0202	-0143	+0390
4790	+0080	+0600	+0404	+0704	-1075	-0506	-0006	-0390	+0598
4792	+0120	+0600	+0606	+1056	-1750	-0844	-0156	-0506	+0910
4792	+0160	+0600	+0807	+1408	-2488	-1265	-0472	-0671	+1296
4793	+0200	+0600	+1004	+1757	-3271	-1789	-1013	-0839	+1785
4794	+0240	+0600	+1200	+2107	-4093	-2353	-1509	-1177	+2144
4795	+0280	+0600	+1391	+2452	-4937	-2992	-1731	-1587	+2509
4796	+0000	+0600	-0000	+0000	-0053	+0027	-0492	+0113	+0243
4796	+0000	+0600	-0044	+0022	+0000	+0000	+0000	+0000	+0000

Table 190

Exponent / Configuration	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4808	+0000	+0750	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4798	-0040	+0750	-0106	-0392	+0489	+0182	-0545	-0069	-0104
	4799	+0000	+0750	-0001	+0000	-0061	+0066	-0483	-0282	+0115
	4800	+0040	+0750	+0104	+0393	-0578	-0069	-0130	-0402	+0282
W_4 B C^F	4802	+0080	+0750	+0208	+0787	-1240	-0196	+0008	-0575	+0539
	4802	+0120	+0750	+0312	+1181	-2004	-0351	-0084	-0725	+0906
$\xi_{-z} = +20^\circ$	4804	+0160	+0750	+0415	+1574	-2879	-0578	-0529	-0736	+1360
	4804	+0200	+0750	+0517	+1969	-3847	-0836	-1648	-0738	+1934
	4806	+0240	+0750	+0617	+2364	-4925	-1206	-2950	-0780	+2578
	4806	+0280	+0750	+0715	+2759	-6032	-1611	-3870	-1149	+3072
	4807	+0000	+0750	-0001	+0000	-0043	+0054	-0615	-0540	+0020
	4808	+0000	+0750	-0041	+0020	+0000	+0000	+0000	+0000	+0000

Table 191

	0000	-0001	-0001	-0002	-0002	-0004	-0005	-0006	-0006	-0004
	4819	+0000	+0900	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4810	-0040	+0900	-0001	-0405	+0496	+0368	-4498	-4620	-0276
	4810	+0000	+0900	-0001	+0002	-0076	+0470	-3750	-4594	-0017
	4811	+0040	+0900	-0001	+0409	-0616	+0452	-0162	-5071	+0147
W_4 B C^F	4812	+0080	+0900	-0001	+0814	-1307	+0540	+1184	-6274	+0445
	4813	+0120	+0900	-0001	+1224	-2093	+0554	+1932	-7410	+0830
$\xi_{-z} = +20^\circ$	4814	+0160	+0900	-0001	+1634	-3034	+0425	+3278	-7000	+1360
	4815	+0200	+0900	-0001	+2044	-4064	+0458	+5220	-6072	+1981
	4816	+0240	+0900	-0002	+2457	-5259	+1017	+5519	-6245	+2579
	4818	+0280	+0900	-0002	+2871	-6574	+0684	+6429	-8046	+3276
	4818	+0000	+0900	-0001	+0001	-0061	+0259	-4647	-8747	-0184
	4818	+0000	+0900	-0023	+0014	+0000	+0000	+0000	+0000	+0000

Table 192

W_4 B C^F

$\xi_{-z} = +20°$

Serial No.	$\sigma°$	$\lambda°$	$\alpha°$	$\beta°$	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
Exponent / Configuration									
0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0006	-0004
4830	+0000	+1050	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4820	-0040	+1050	+0104	-0392	+0513	-0091	-0489	-2164	-0138
4821	+0000	+1050	-0001	+0002	-0051	+0048	-0490	-1972	+0098
4822	+0040	+1050	-0106	+0393	-0559	+0191	-0164	-0936	+0300
4824	+0080	+1050	-0210	+0786	-1199	+0317	+0007	-1485	+0538
4824	+0120	+1050	-0314	+1179	-1967	+0481	+0255	-1955	+0882
4826	+0160	+1050	-0417	+1574	-2815	+0711	+0846	-0565	+1301
4826	+0200	+1050	-0518	+1968	-3773	+0951	+2138	-0237	+1946
4828	+0240	+1050	-0619	+2362	-4809	+1332	+2994	+3436	+2543
4828	+0280	+1050	-0717	+2757	-5892	+1746	+4074	+6627	+3094
4829	+0000	+1050	-0001	+0000	-0041	+0042	-0564	-3762	+0019
4829	+0000	+1050	-0014	+0009	+0000	+0000	+0000	+0000	+0000

Table 193

W_4 B C^F

$\xi_{-z} = +20°$

0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
4841	+0000	+1200	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4831	-0040	+1200	+0202	-0352	+0438	-0206	-0424	-0146	+0029
4832	+0000	+1200	-0001	+0001	-0060	+0055	-0439	-0041	+0207
4833	+0040	+1200	-0204	+0353	-0515	+0335	-0128	+0066	+0358
4834	+0080	+1200	-0407	+0705	-1077	+0629	-0030	+0110	+0513
4836	+0120	+1200	-0608	+1057	-1735	+0962	+0197	+0147	+0792
4836	+0160	+1200	-0809	+1410	-2457	+1423	+0651	+0523	+1105
4838	+0200	+1200	-1008	+1760	-3200	+1953	+1105	+1156	+1537
4838	+0240	+1200	-1203	+2109	-4014	+2506	+1814	+1595	+1935
4840	+0280	+1200	-1394	+2454	-4864	+3123	+2396	+2006	+2459
4840	+0000	+1200	-0001	+0000	-0057	+0060	-0466	-0205	+0151
4840	+0000	+1200	-0010	+0001	+0000	+0000	+0000	+0000	+0000

Table 194

W_4 B C^F

ξ_{-z} = +20°

Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
0000	-0001	-0001	-0002	-0002	-0004	-0004	-0006	-0005	-0004
4857	+0000	+1350	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4847	-0040	+1350	+0287	-0288	+0388	-0324	-6322	+0035	+0194
4848	+0000	+1350	-0002	+0001	-0053	+0053	-4695	+0279	+0335
4850	+0040	+1350	-0288	+0287	-0405	+0448	-2776	+0571	+0469
4850	+0080	+1350	-0575	+0575	-0859	+0899	-0455	+0754	+0540
4852	+0120	+1350	-0861	+0860	-1341	+1406	-1512	+1160	+0736
4852	+0160	+1350	-1146	+1145	-1945	+2010	-2262	+1690	+1067
4854	+0200	+1350	-1429	+1428	-2566	+2654	-4671	+2464	+1443
4854	+0240	+1350	-1708	+1706	-3255	+3338	-3502	+3120	+1766
4850	+0280	+1350	-1983	+1982	-3968	+4105	-4695	+3898	+2079
4856	+0000	+1350	-0000	-0000	-0016	+0049	-5495	+0384	+0341
4856	+0000	+1350	-0005	-0002	+0000	+0000	+0000	+0000	+0000

Table 195

W_4 B C^F

ξ_{-z} = +20°

0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
4868	+0000	+1500	+0000	+0000	+0000	+0000	+0000	+0000	+0000
4858	-0040	+1500	+0351	-0203	+0258	-0429	-0449	+0013	+0216
4859	+0000	+1500	-0000	-0000	-0031	+0045	-0519	+0303	+0327
4860	+0040	+1500	-0353	+0203	-0272	+0533	-0371	+0736	+0421
4861	+0080	+1500	-0705	+0405	-0561	+1126	-0385	+1148	+0480
4862	+0120	+1500	-1058	+0607	-0896	+1788	-0632	+1669	+0575
4863	+0160	+1500	-1408	+0807	-1326	+2497	-1111	+2337	+0771
4864	+0200	+1500	-1759	+1004	-1842	+3273	-1826	+3169	+1114
4865	+0240	+1500	-2107	+1200	-2436	+4055	-2298	+4009	+1451
4860	+0280	+1500	-2452	+1391	-3083	+4899	-2873	+4808	+1801
4867	+0000	+1500	-0000	-0001	-0012	+0054	-0653	+0496	+0406
4868	+0000	+1500	-0002	-0006	+0000	+0000	+0000	+0000	+0000

Table 196

Configuration / Exponent	Serial No.	σ°	λ°	α°	β°	C_y	C_z	$2\,C_\ell$	C_m	$5{\cdot}33\,C_n$
	0000	-0001	-0001	-0002	-0002	-0004	-0004	-0005	-0005	-0004
	4879	+0000	+1650	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4870	-0040	+1650	+0392	-0105	+0114	-0493	-0443	-0125	+0232
	4870	+0000	+1650	-0001	+0000	-0031	+0045	-0517	+0509	+0314
W_4 B C^F	4872	+0040	+1650	-0394	+0105	-0161	+0604	-0470	+0766	+0364
	4872	+0080	+1650	-0787	+0209	-0304	+1283	-0514	+1304	+0389
$\xi_{-z} = +20^\circ$	4874	+0120	+1650	-1182	+0313	-0471	+2044	-0820	+2002	+0469
	4874	+0160	+1650	-1576	+0416	-0691	+2886	-1490	+2858	+0592
	4875	+0200	+1650	-1971	+0518	-0974	+3821	-2612	+3791	+0734
	4876	+0240	+1650	-2367	+0619	-1345	+4874	-4024	+4810	+0962
	4877	+0280	+1650	-2762	+0717	-1772	+5961	-5180	+5800	+1241
	4878	+0000	+1650	-0000	-0000	-0031	+0057	-0576	+0436	+0367
	4878	+0000	+1650	+0001	-0010	+0000	+0000	+0000	+0000	+0000

Table 197

	0000	-0001	-0001	-0002	-0002	-0005	-0004	-0005	-0005	-0005
	4890	+0000	+1800	+0000	+0000	+0000	+0000	+0000	+0000	+0000
	4880	-0040	+1800	+0406	-0000	-0103	-0510	-0459	-0436	+1522
	4881	+0000	+1800	-0001	-0000	-0169	+0038	-0553	-0005	+1758
	4882	+0040	+1800	-0406	-0000	-0243	+0607	-0688	+0502	+2306
W_4 B C^F	4883	+0080	+1800	-0814	+0000	-0527	+1313	-0897	+1194	+3113
	4884	+0120	+1800	-1223	+0000	-0902	+2110	-1197	+1898	+3610
$\xi_{-z} = +20^\circ$	4885	+0160	+1800	-1632	+0000	-1122	+3014	-1408	+2968	+5585
	4886	+0200	+1800	-2044	+0001	-1742	+4040	-1407	+3965	+6353
	4887	+0240	+1800	-2456	+0000	-1118	+5193	-1572	+4952	+6244
	4888	+0280	+1800	-2870	+0001	-1427	+6480	-1692	+5990	+5804
	4889	+0000	+1800	-0001	-0000	-0047	+0040	-0659	-0105	+1105
	4890	+0000	+1800	+0002	-0002	+0000	+0000	+0000	+0000	+0000

SYMBOLS

A		gross aspect ratio of the wing
A_N		net aspect ratio of the control
a		body radius
a_1, a_2, a_3, a_4		coefficients in equation (9)
$\bar{\bar{c}}$		aerodynamic mean chord of the wing (4 inch)
C_R		root chord of wing (6 inch)
$C_{y,y',z,z'}$	$\equiv$	$\frac{Y,\ Y',\ Z,\ Z'}{q\ S_W}$
C_{ℓ}	$\equiv$	$\frac{L}{q\ S_W\ 2s}$
$C_{m,m',n,n'}$	$\equiv$	$\frac{M,\ M',\ N,\ N'}{q\ S_W\ \bar{\bar{c}}}$
d	=	body diameter
F	=	non linearity factor (see Fig. 18(a))
H	=	total head pressure
k	=	pitching moment stabiliser effectiveness (see equation (2))
k_η	=	pitching moment control effectiveness (see equation (3))
$k_{B(W)}, k_{W(B)}, K_{B(W)}, K_{W(B)}$		interference factors see Appendix
ℓ_c		control arm i.e. distance of control hinge line from the reference point O
N	=	number of wing panels
q	=	kinetic pressure
S_W	=	wing gross area
S_C	=	control net area
s	=	semi span of wing
t_1	=	$\beta \tan \gamma$
t_o	=	$\beta \tan \theta_o$
$Oxyz$ $Oxy'z'$	}	right handed axes fixed in the body see Fig. 2
α		angle of incidence $\alpha \equiv \sin^{-1}(\sin\sigma \cos\lambda)$
β		angle of sideslip $\beta \equiv \cos^{-1}(\sin\sigma \sin\lambda)$
$\bar{\beta}$		$\sqrt{M^2 - 1}$
γ		semi apex angle of the wing

SYMBOLS (Contd)

Γ	circulation
ΔC_{m_c}	increment in pitching moment due to addition of the control
ΔC_{m_η}	increment in pitching moment due to control deflection η
ΔC_ℓ	increment in rolling moment due to control deflection
ΔC_{N_p}	derived panel normal force see equation (9)
ΔC_{ℓ_p}	derived panel rolling moment see equation (12)
ε	downwash angle
$\bar{\varepsilon}$	mean downwash angle over the control equation (12)
η	elevator angle
θ_o	semi angle of cone
σ	body incidence
λ	roll angle
ξ	aileron angle
$\xi_{-y,y,-z,z}$	control deflections

Subscripts

ℓ	local condition at the control
∞	free stream conditions

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8	H. Lomax L. Sluder	Downwash in the vertical and horizontal planes of symmetry behind a triangular wing in supersonic flow. N.A.C.A. T.N. 1803, 1949
9	J. R. Spahr	Contribution of the wing panels to the forces and moments of supersonic wing-body combinations at combined angles. N.A.C.A. T.N. 4146, 1958

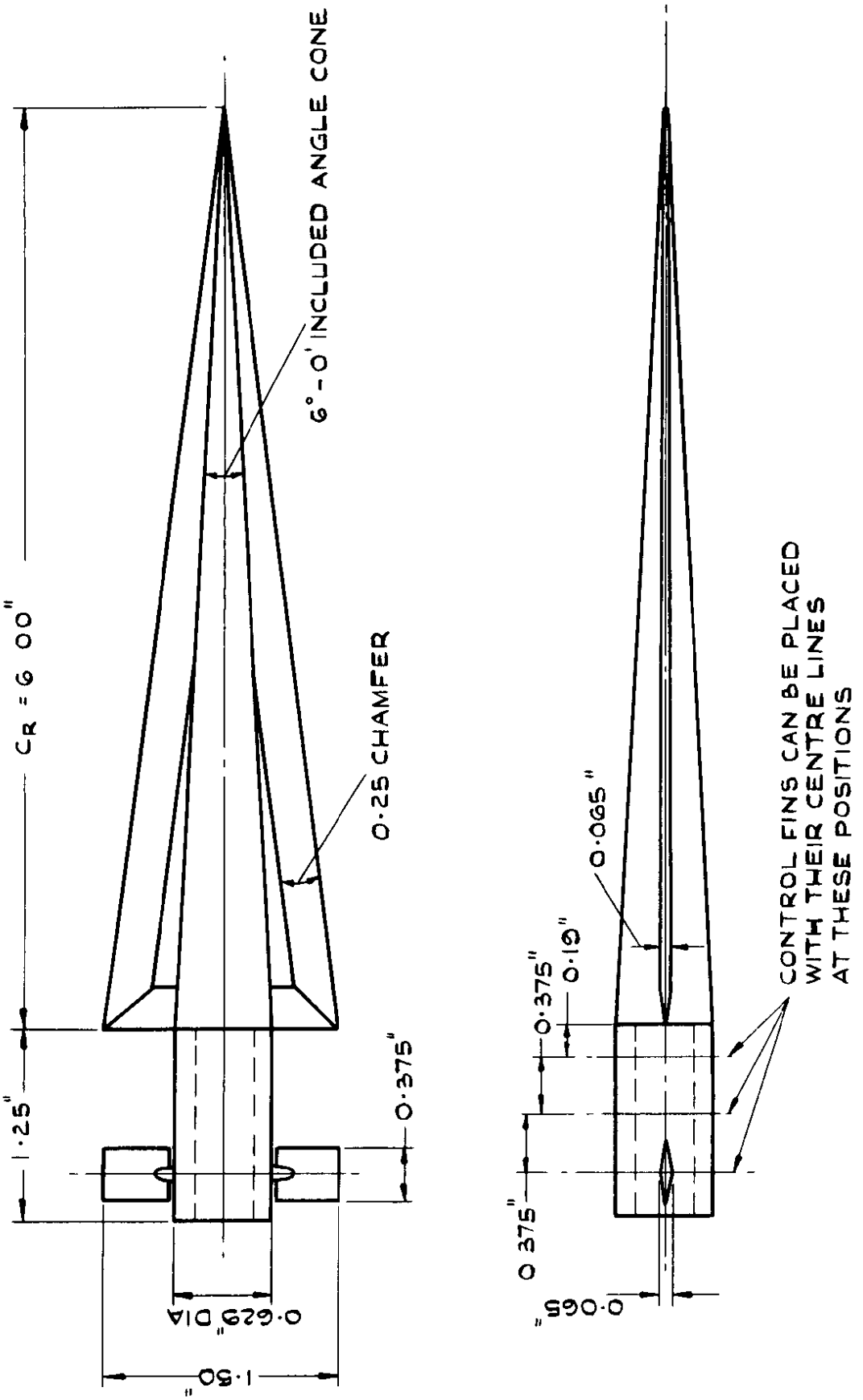


FIG 1 DRAWING OF MODEL W_2

MODELS W_3 & W_4 HAVE WINGS & CONTROL PANELS OF THE SAME DIMENSIONS AS W_2 MOUNTED IN IDENTICAL CONE CYLINDER BODIES

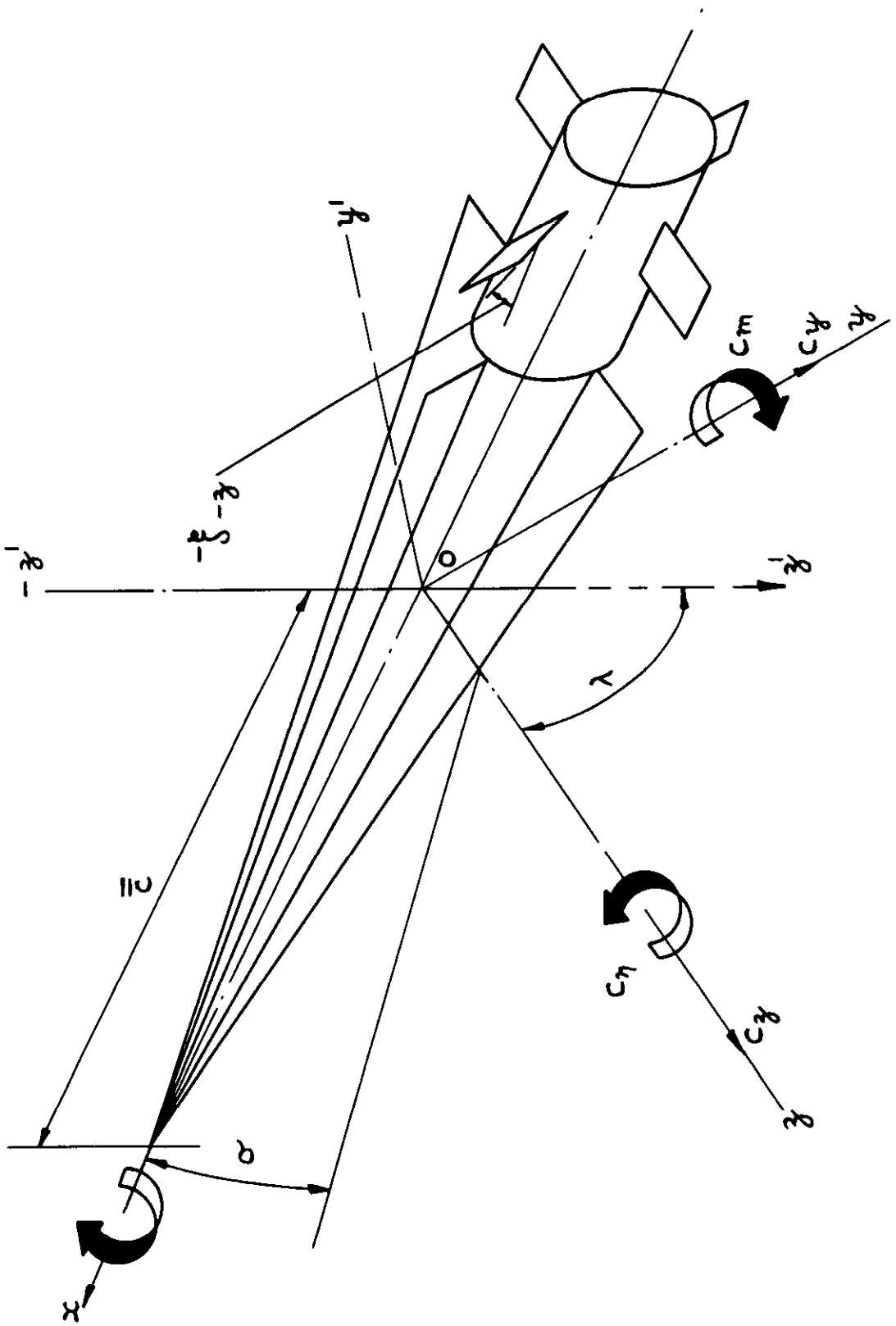


FIG 2 NOTATION USED IN DEFINING THE AXES USED

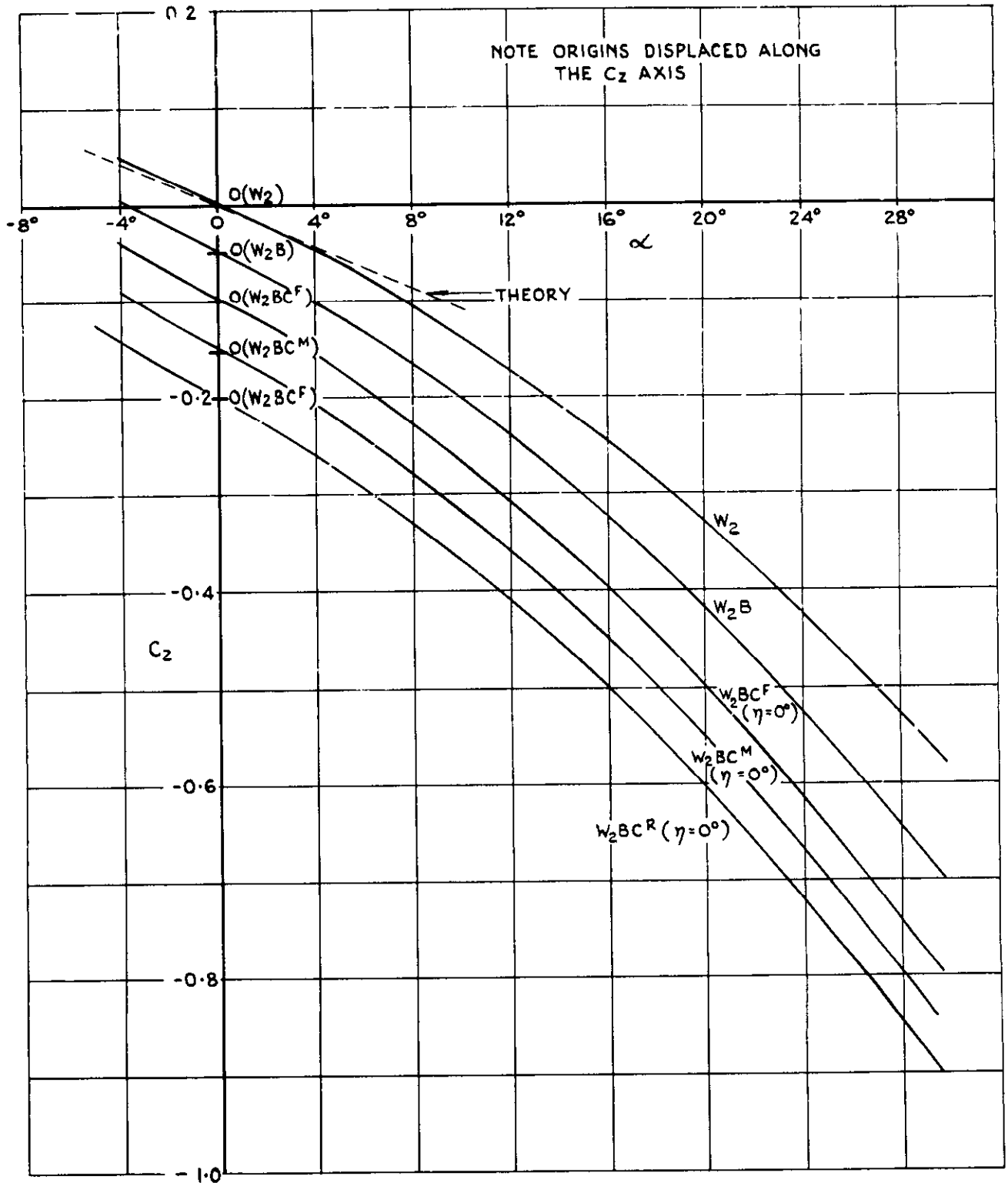


FIG. 3 C_Z v α FOR W_2 W_2B W_2BC^F W_2BC^M AND W_2BC^R (CONTROLS AT η = 0°) AT λ = 0

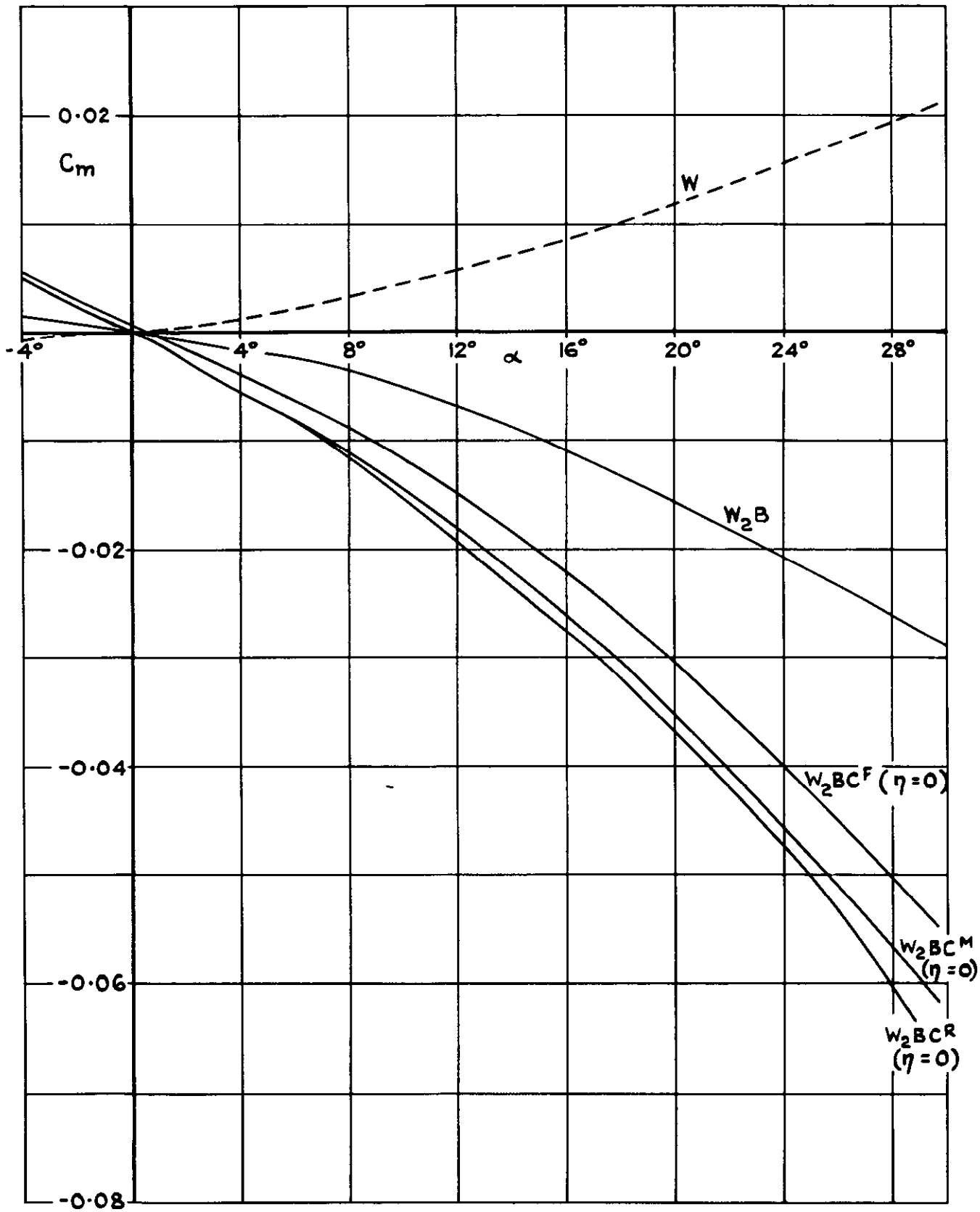


FIG. 4 C_m v α FOR W_2 W_2B, W_2BC^F, W_2BC^M AND W_2BC^R (CONTROLS AT $\eta = 0°$) AT $\lambda = 0$

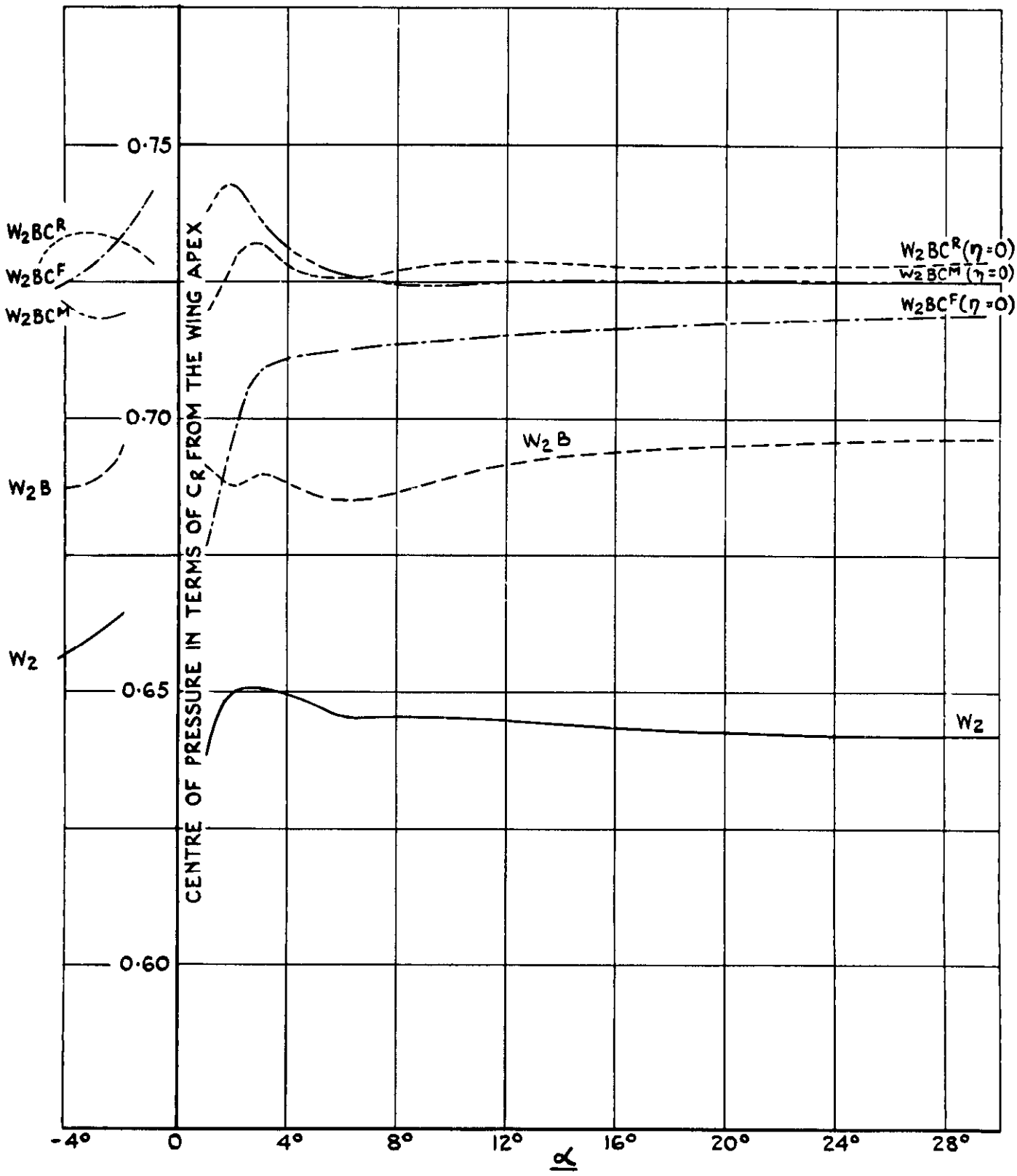


FIG. 5 CENTRE OF PRESSURE FOR W_2, W_2B, W_2BC^F, W_2BC^M AND W_2BC^R (CONTROLS AT $\eta = 0°$)

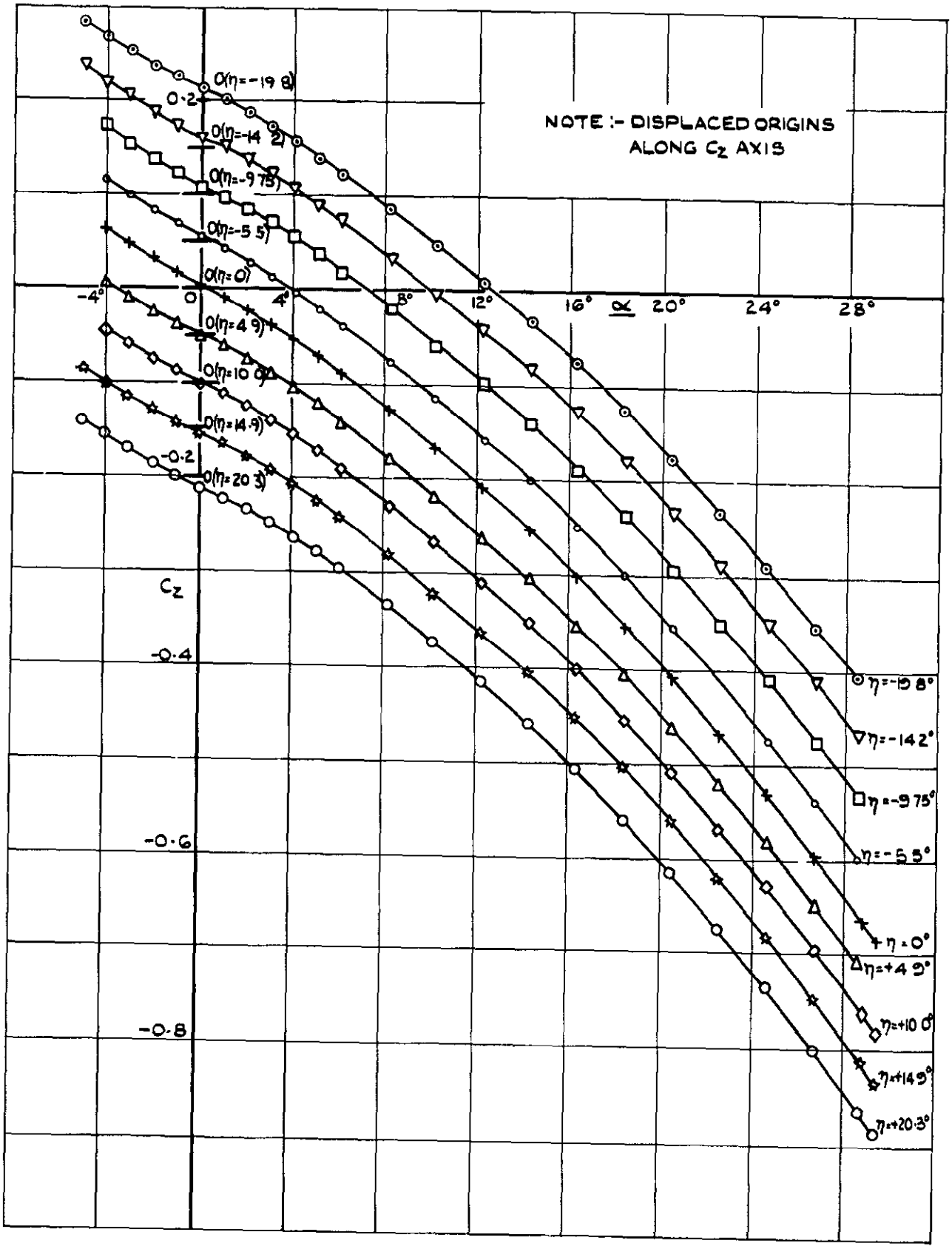


FIG 6 C_z v α FOR W_2BC^F
(CONTROLS IN FRONT POSITION) AT $\lambda = 0$

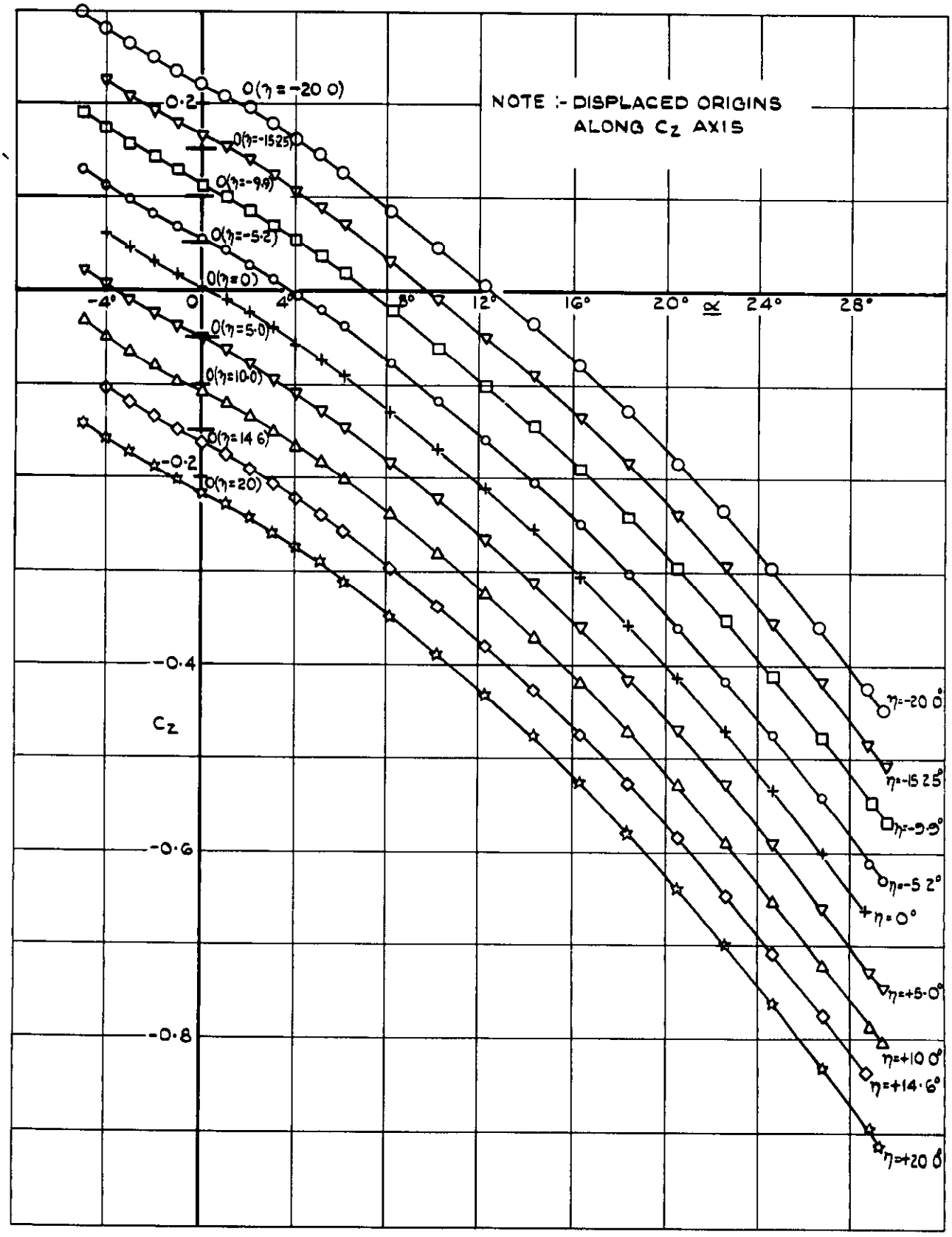


FIG 7 C_z v α FOR W_2BC^M
(CONTROLS IN MIDDLE POSITION) AT $\lambda = 0$

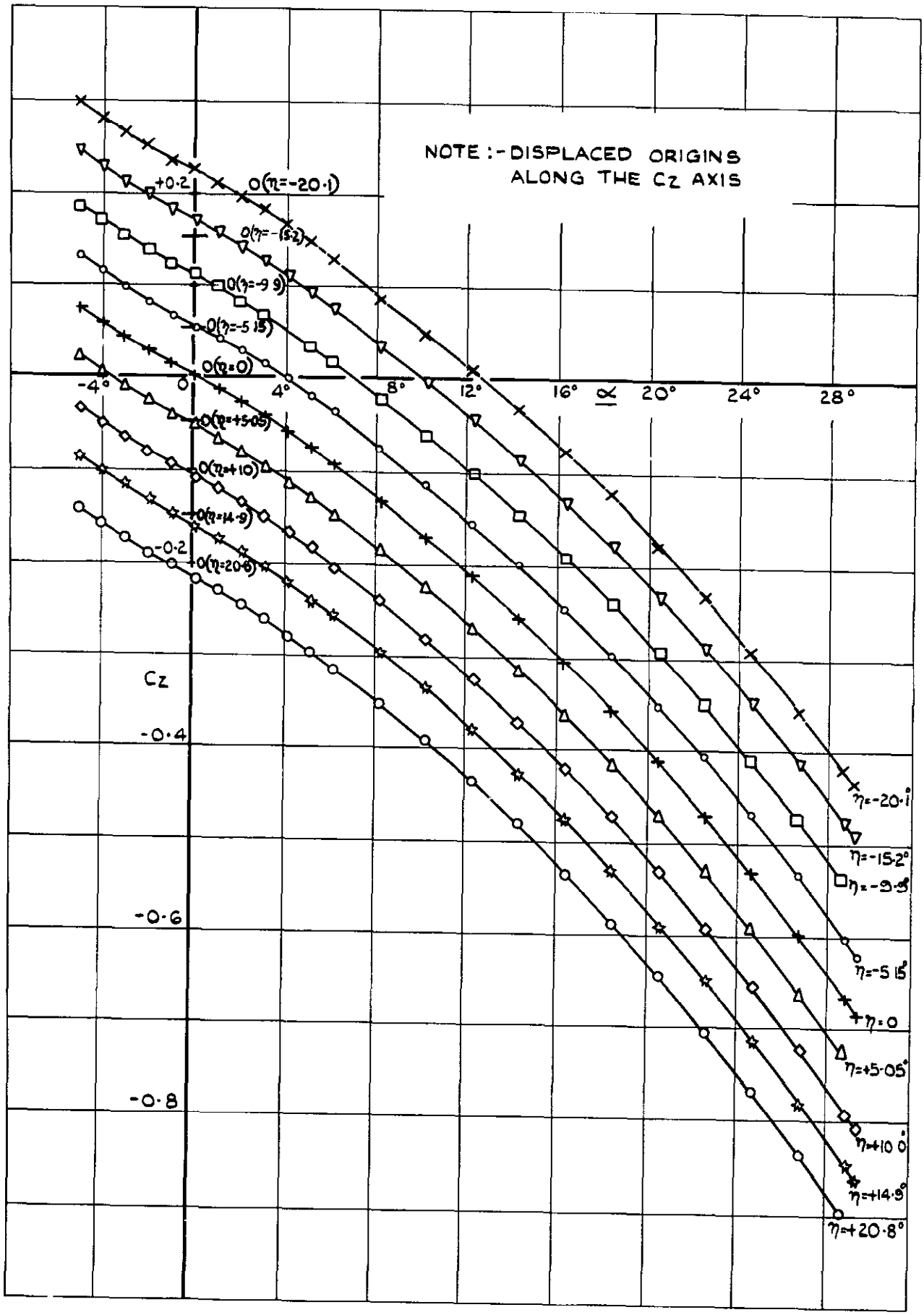


FIG 8 C_z v α FOR W_2BC^R
(CONTROLS IN REAR POSITION) AT $\lambda = 0$

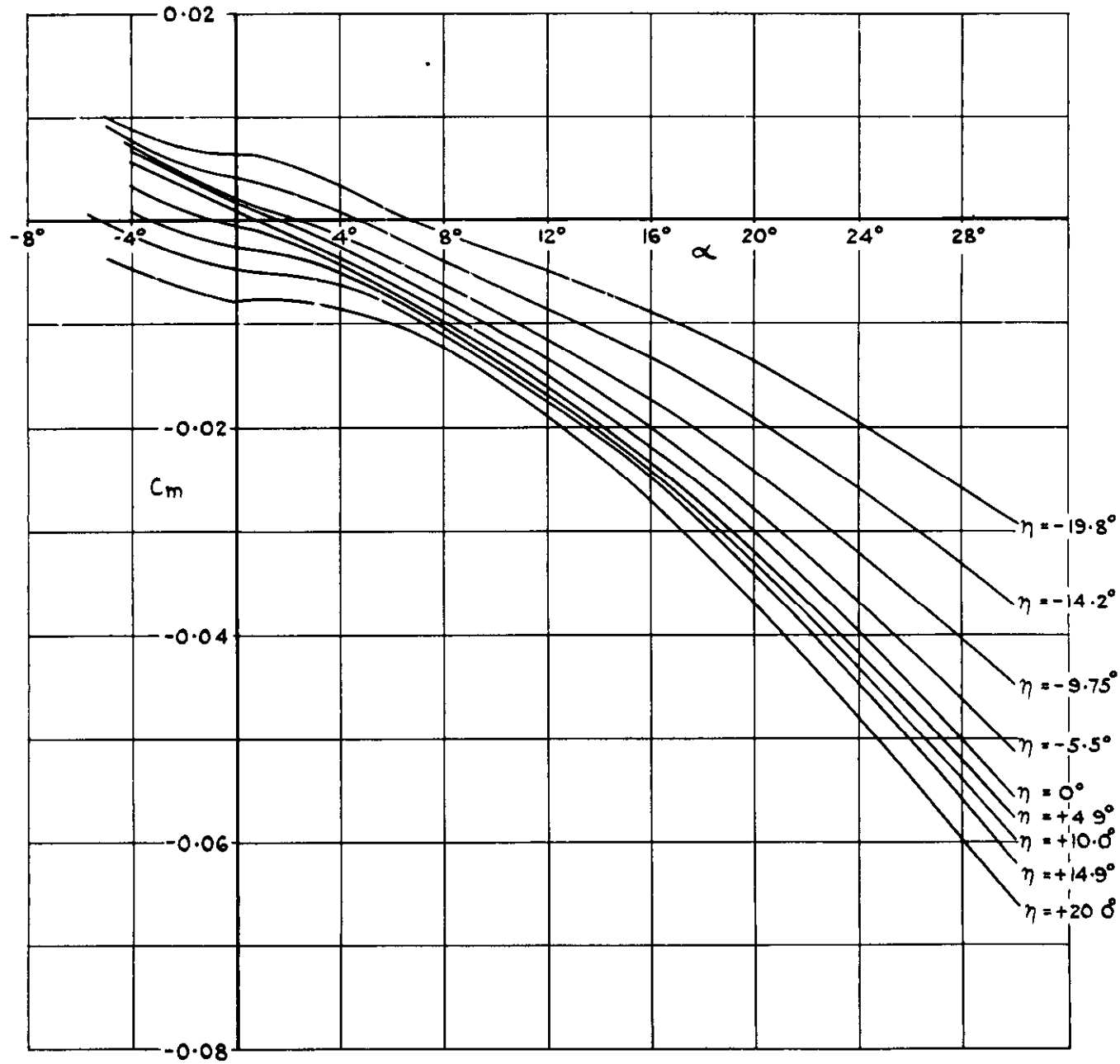


FIG. 9 C_m v α FOR W_2BC^F
(CONTROLS IN FORWARD POSITION) AT $\lambda=0$

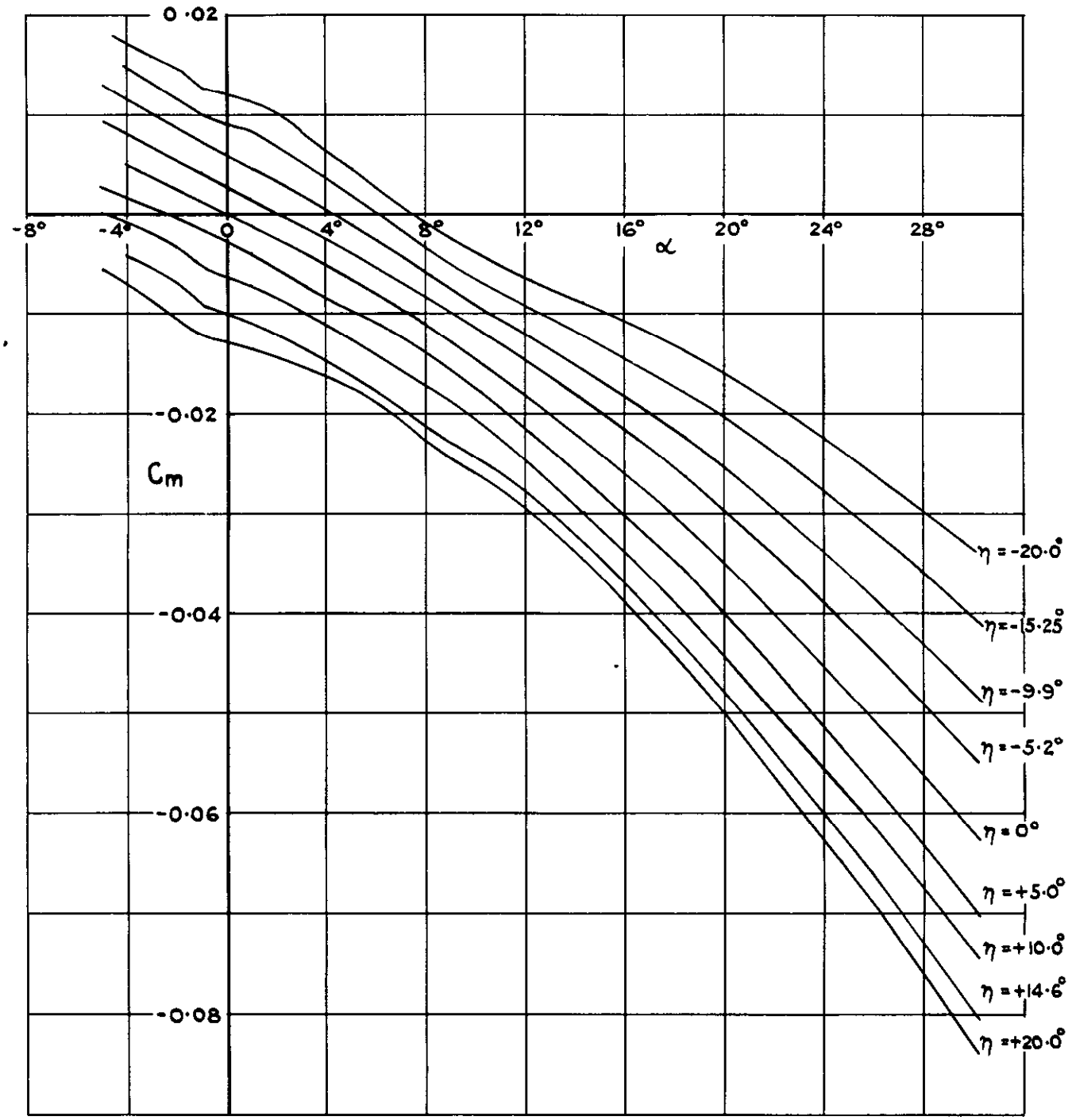


FIG.10 C_m v α FOR W_2BC^M (CONTROLS IN MIDDLE POSITION) AT $\lambda = 0$

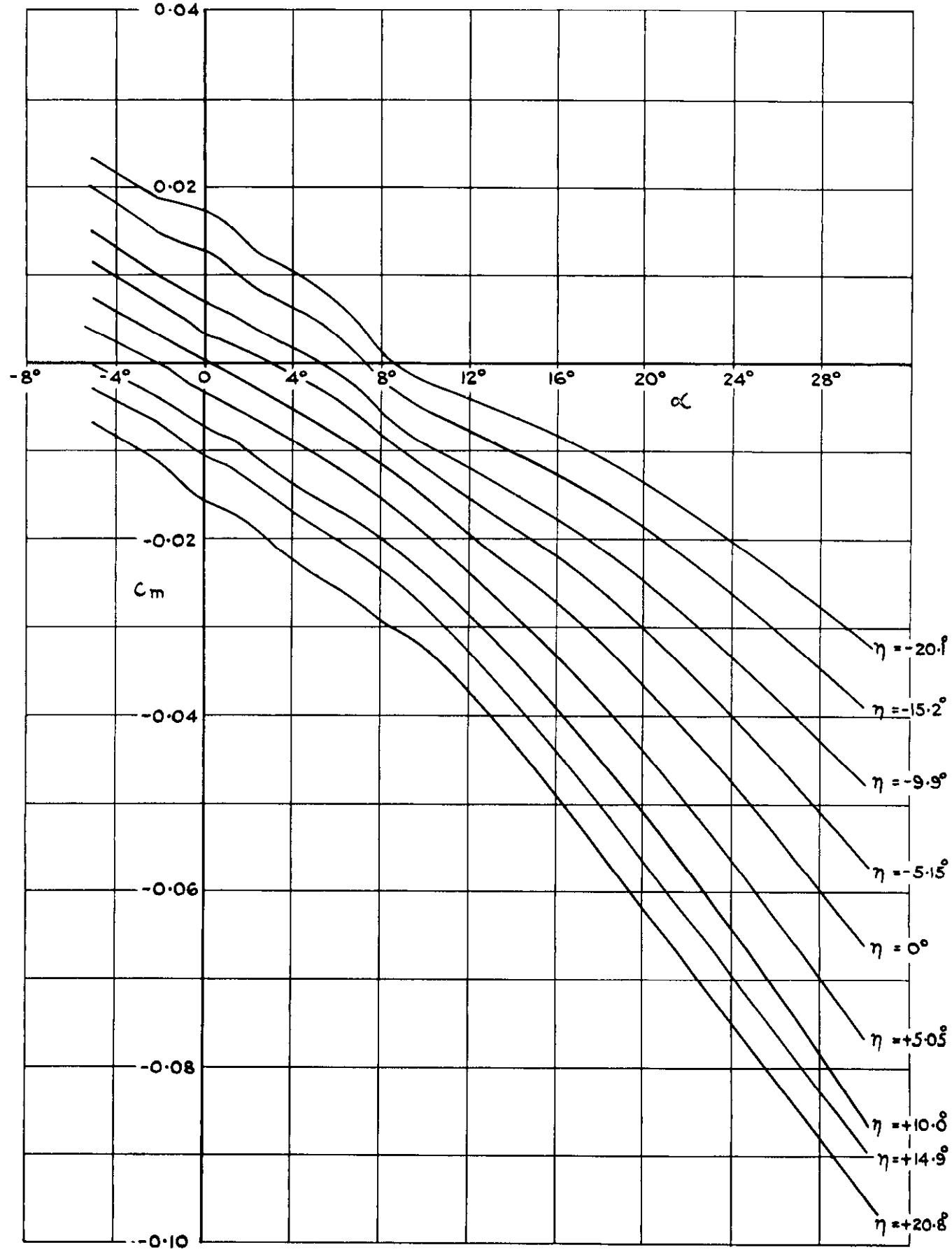


FIG. 11 C_m v α FOR W_2BC^R
(CONTROLS IN REAR POSITION) AT $\lambda = 0$

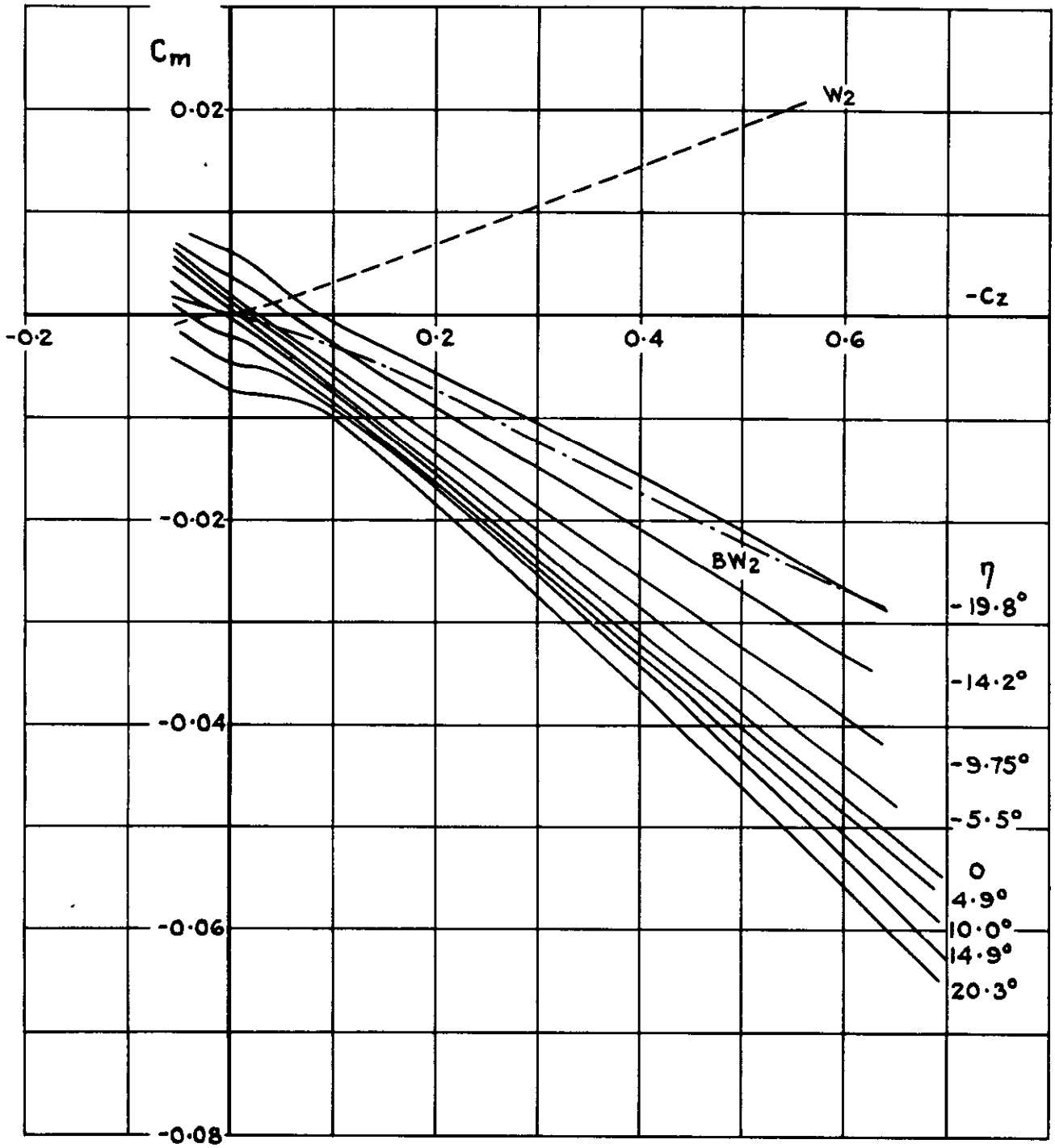


FIG. 12 C_m v C_z FOR W_2BC^F AT $\lambda = 0$

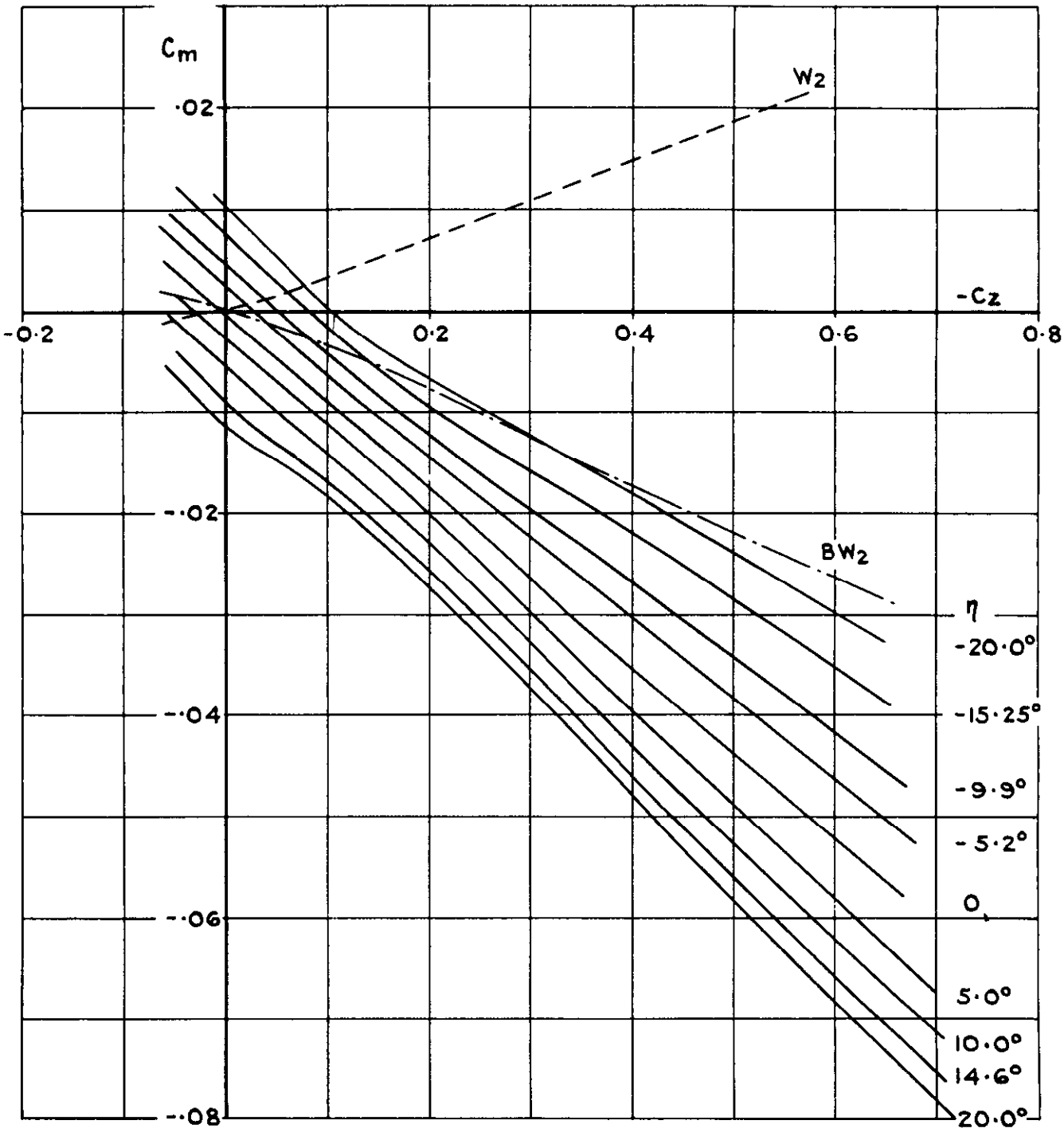


FIG. 13 C_m v C_z FOR W_2BC^M AT $\lambda = 0$

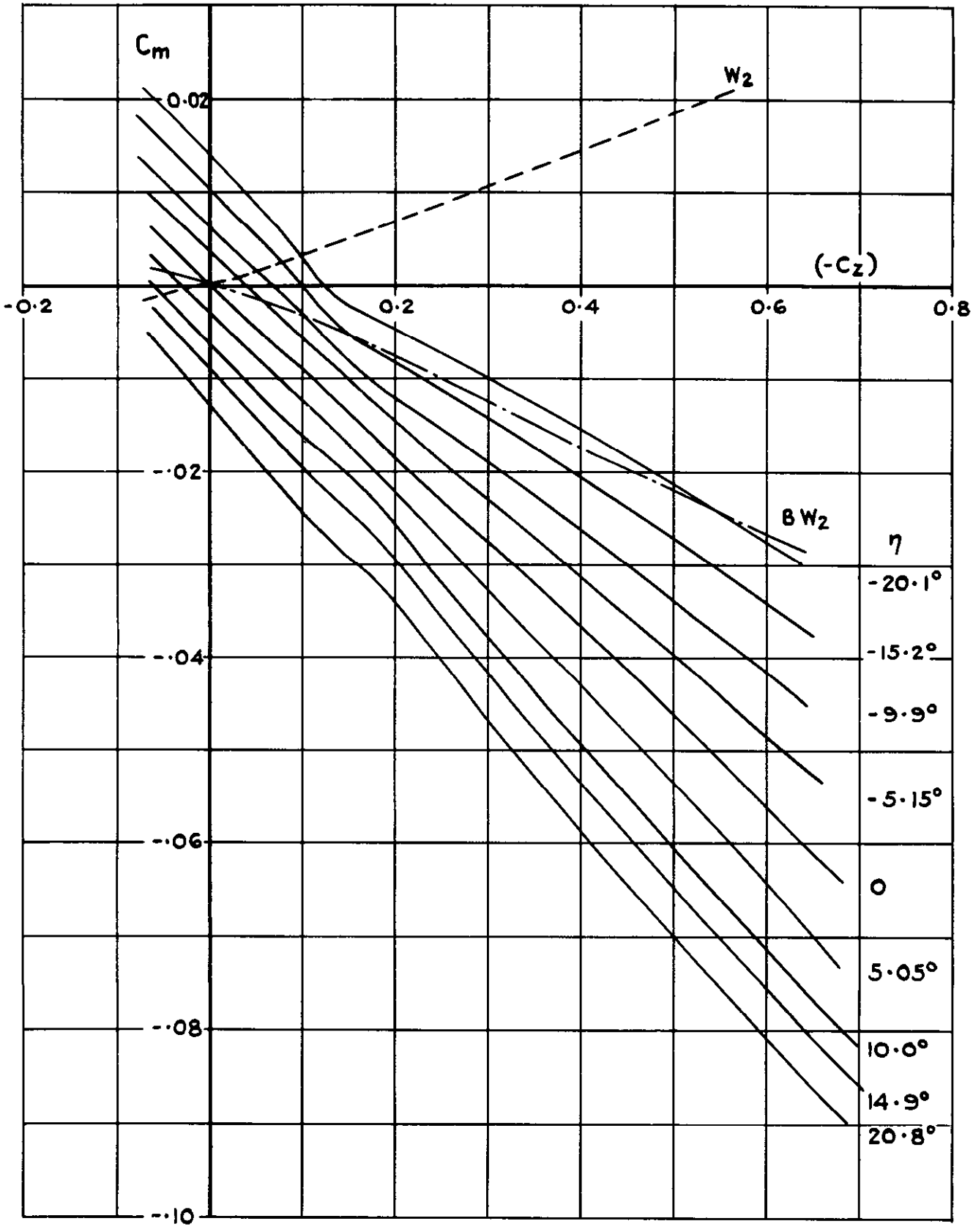


FIG. 14 C_m v C_z FOR W_2BC^R AT $\lambda = 0$

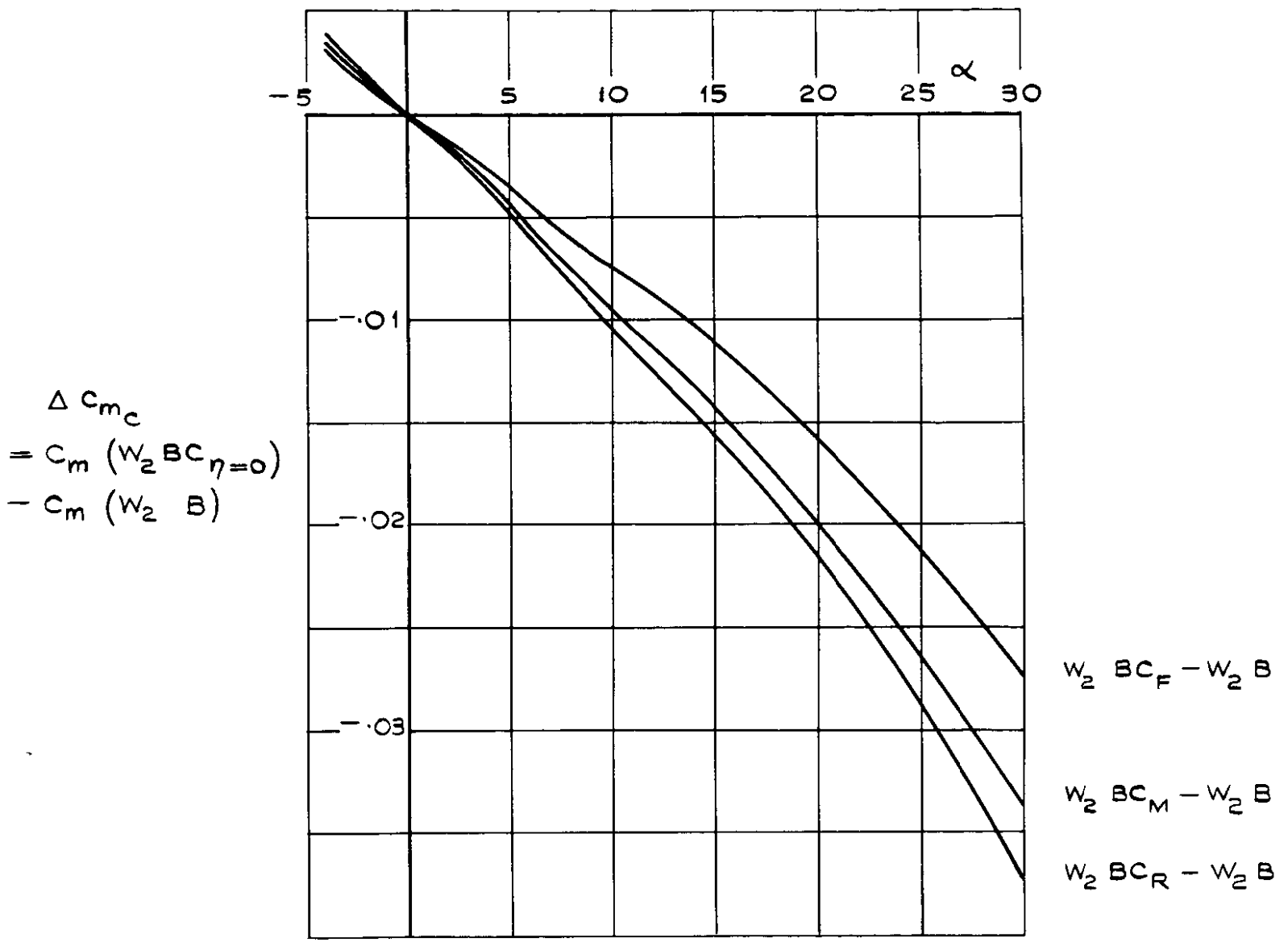


FIG. 15 STABILISING MOMENT DUE TO THE CONTROLS AT $\eta = 0$

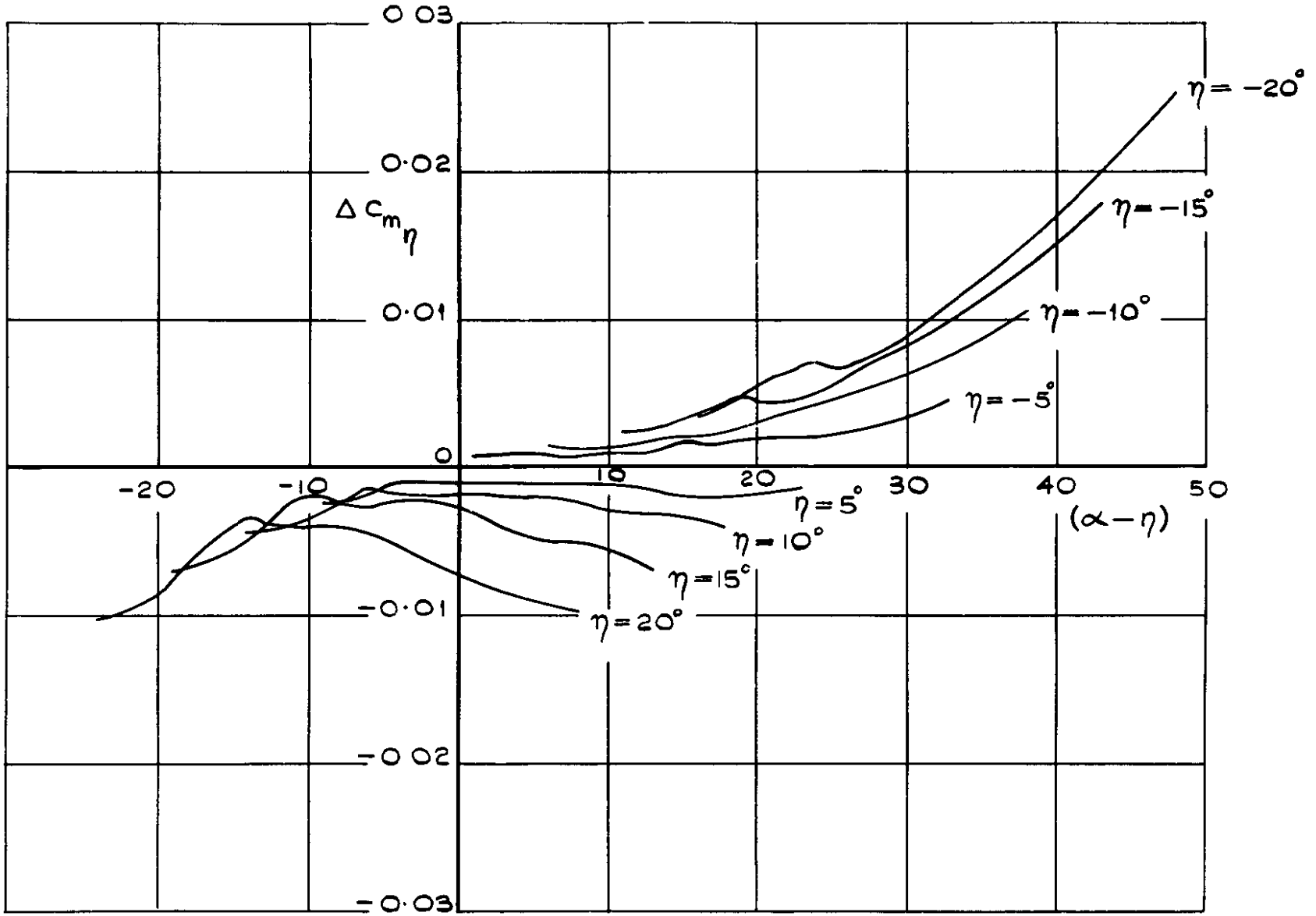


FIG.16 (a) INCREMENT IN PITCHING MOMENT DUE TO CONTROL DEFLECTION W_2BC^F

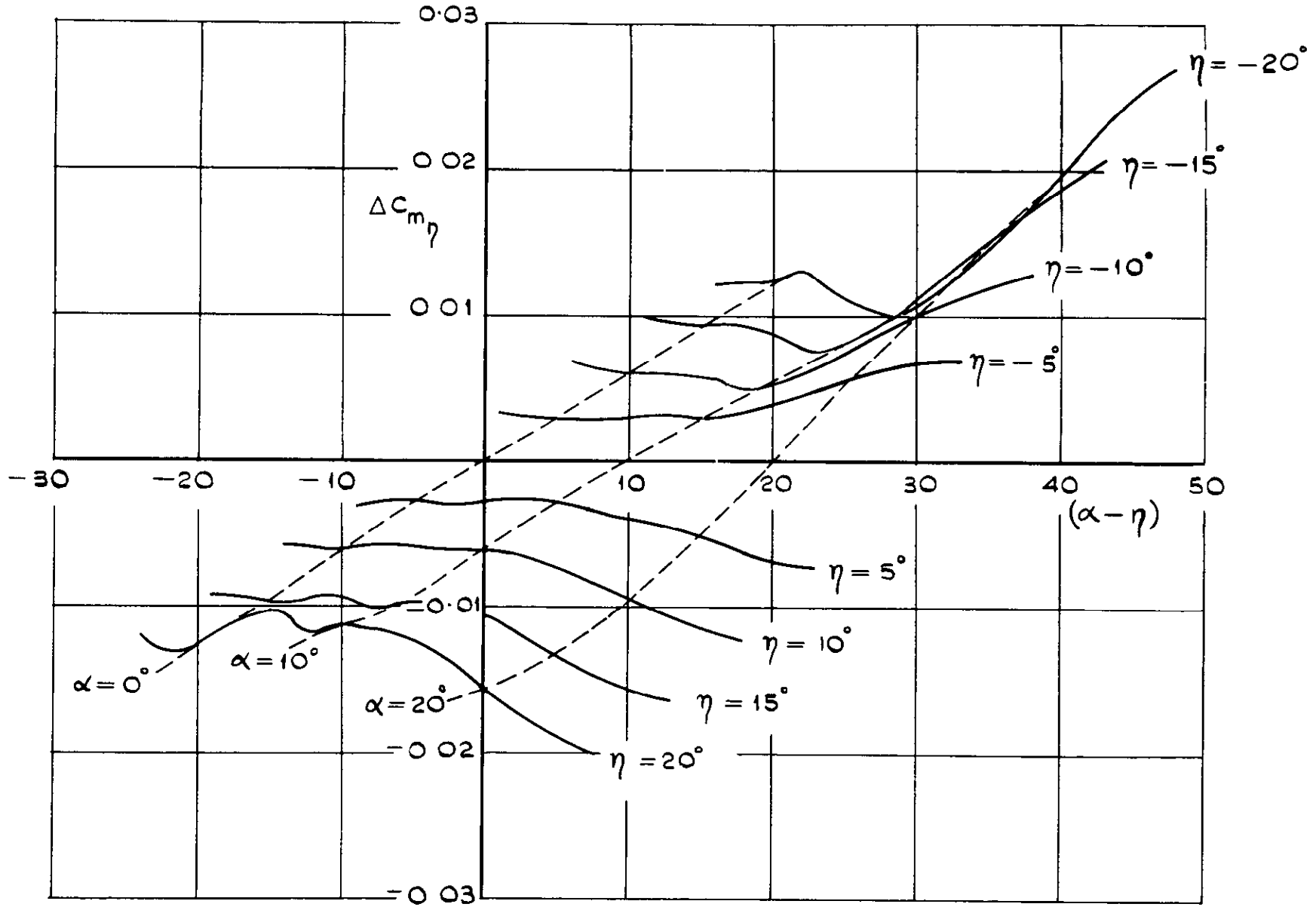


FIG.16 (b) INCREMENT IN PITCHING MOMENT DUE TO CONTROL DEFLECTION $W_2 BC^M$

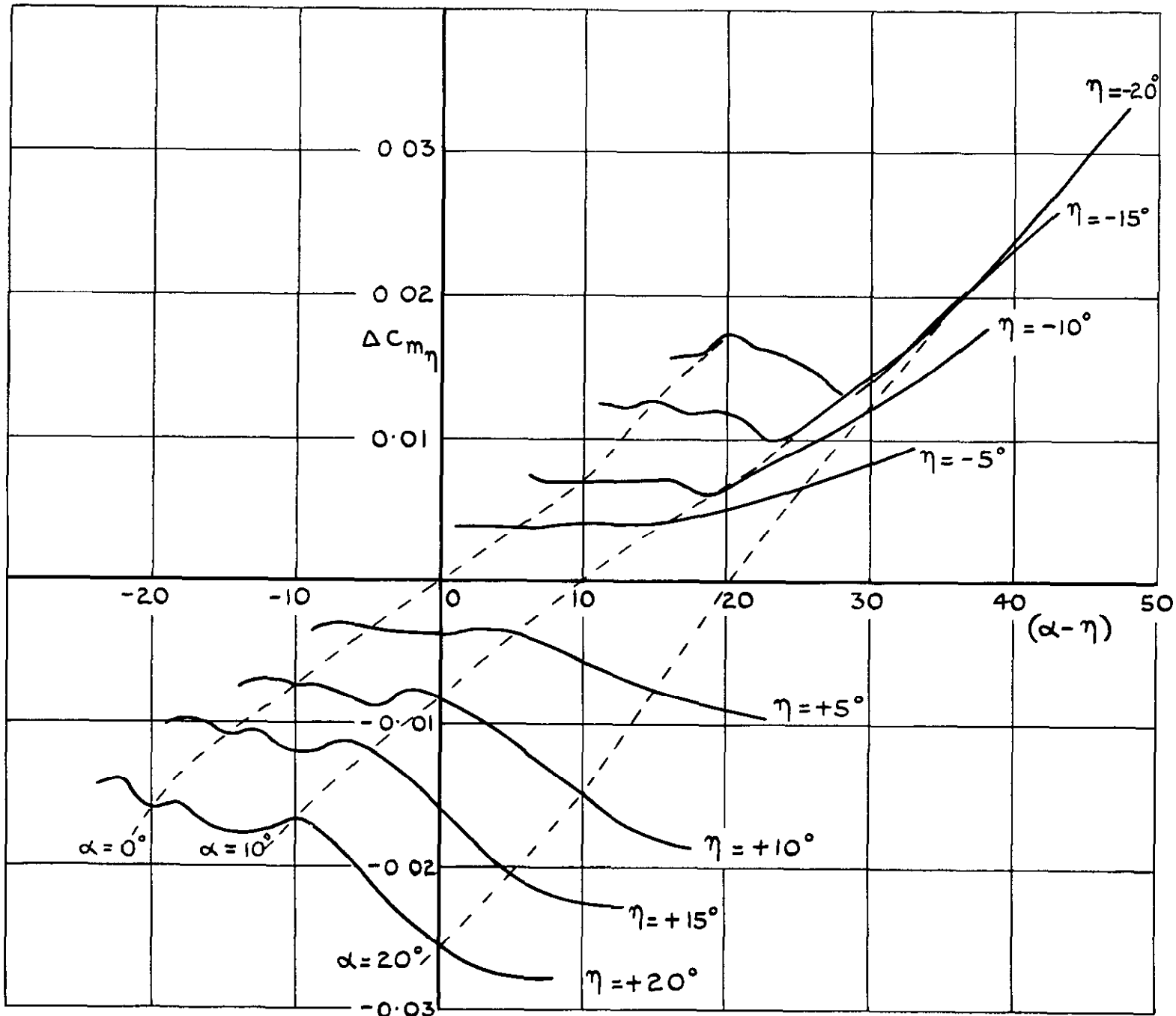
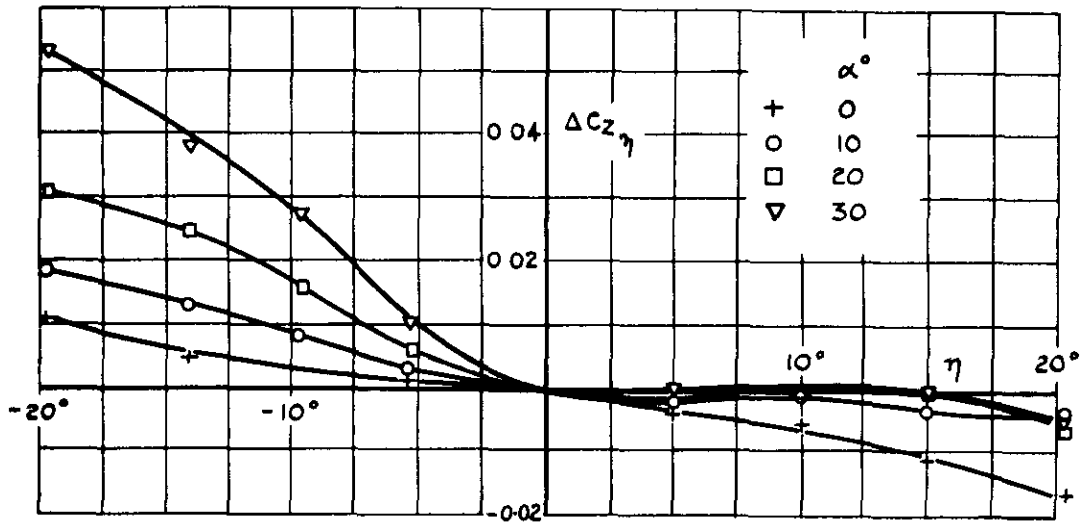
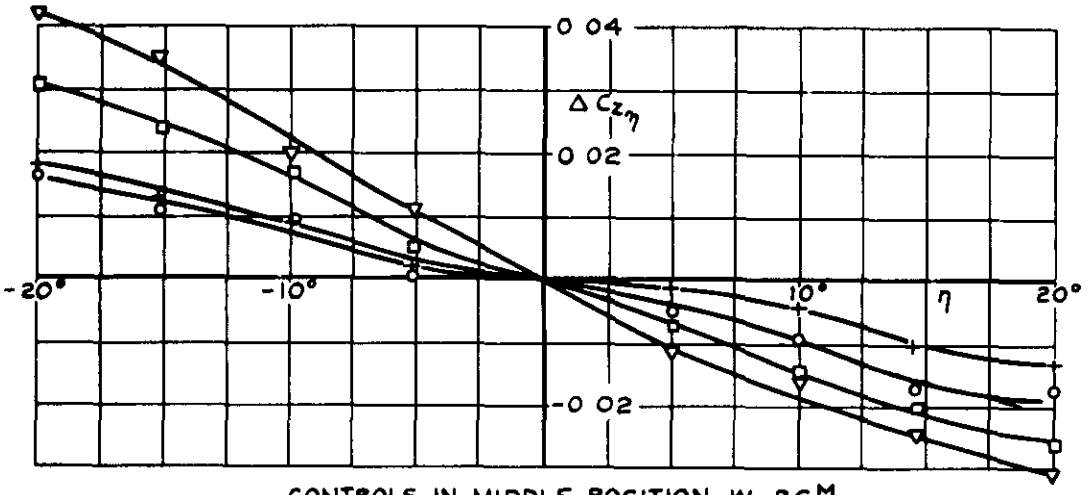


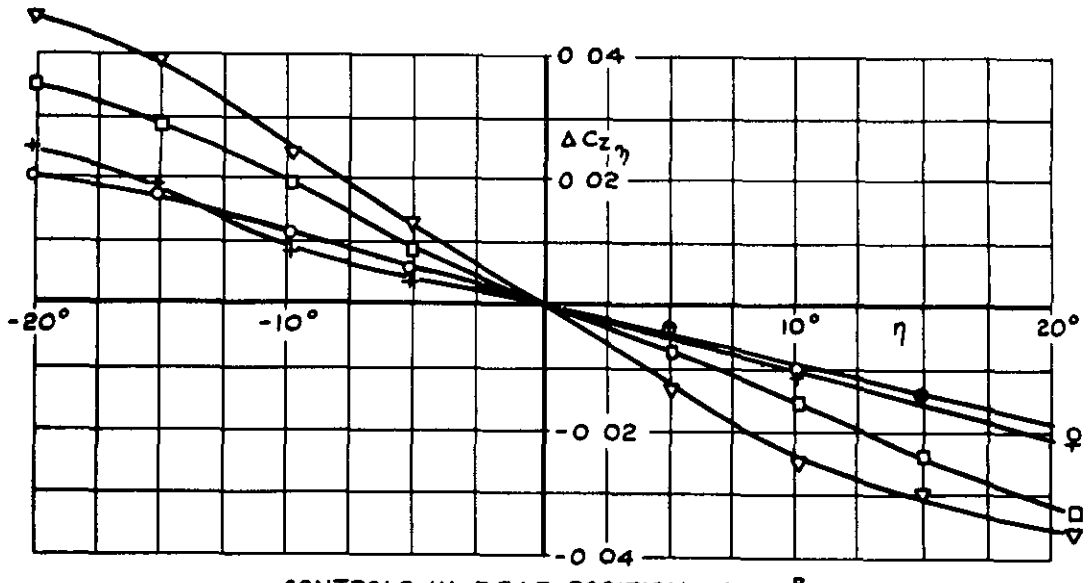
FIG. 16(c) INCREMENT IN PITCHING MOMENT DUE TO CONTROL DEFLECTION W_2 B C^R



CONTROLS IN FRONT POSITION $W_2 BC^F$



CONTROLS IN MIDDLE POSITION $W_2 BC^M$



CONTROLS IN REAR POSITION $W_2 BC^R$

FIG. 17 INCREMENT IN C_z DUE TO DEFLECTING CONTROLS FOR $W_2 BC^F$, $W_2 BC^M$ AND $W_2 BC^R$

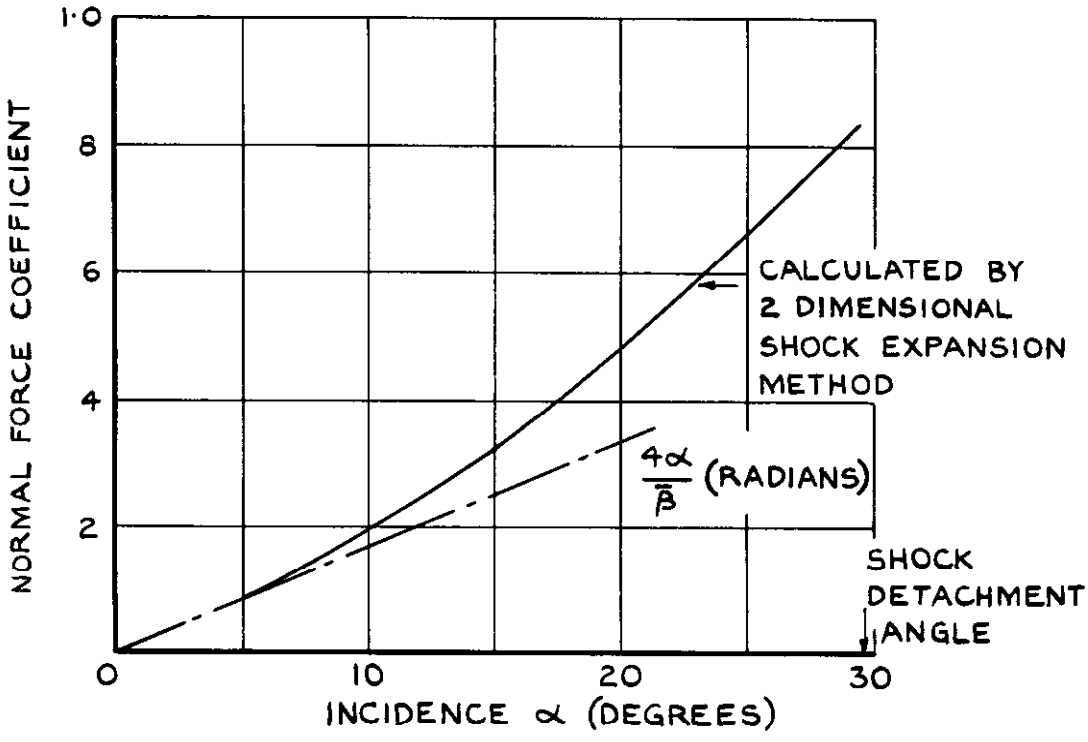


FIG.18 (a) TWO DIMENSIONAL CALCULATION OF NORMAL FORCE FOR THE CONTROL SECTION

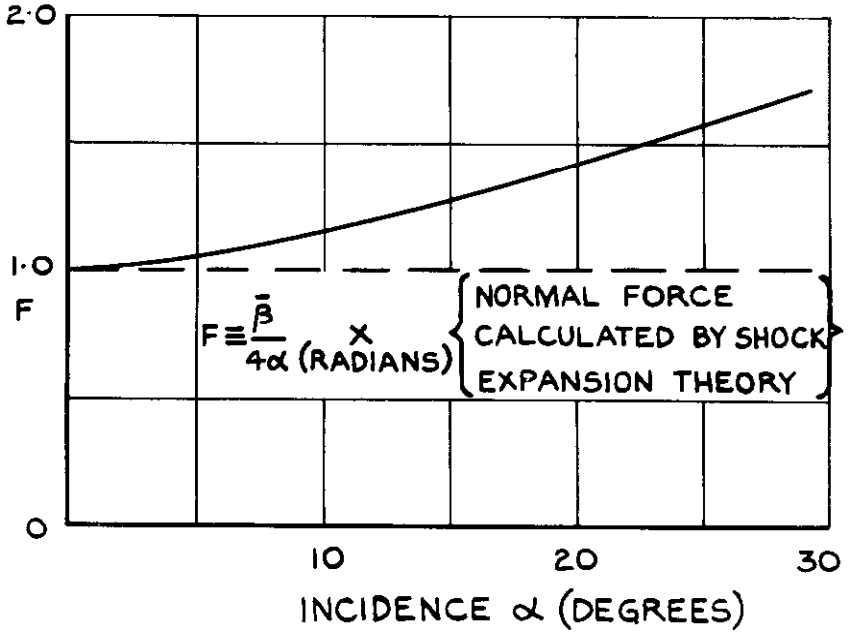


FIG 18 (b) NON LINEAR NORMAL FORCE FACTOR F

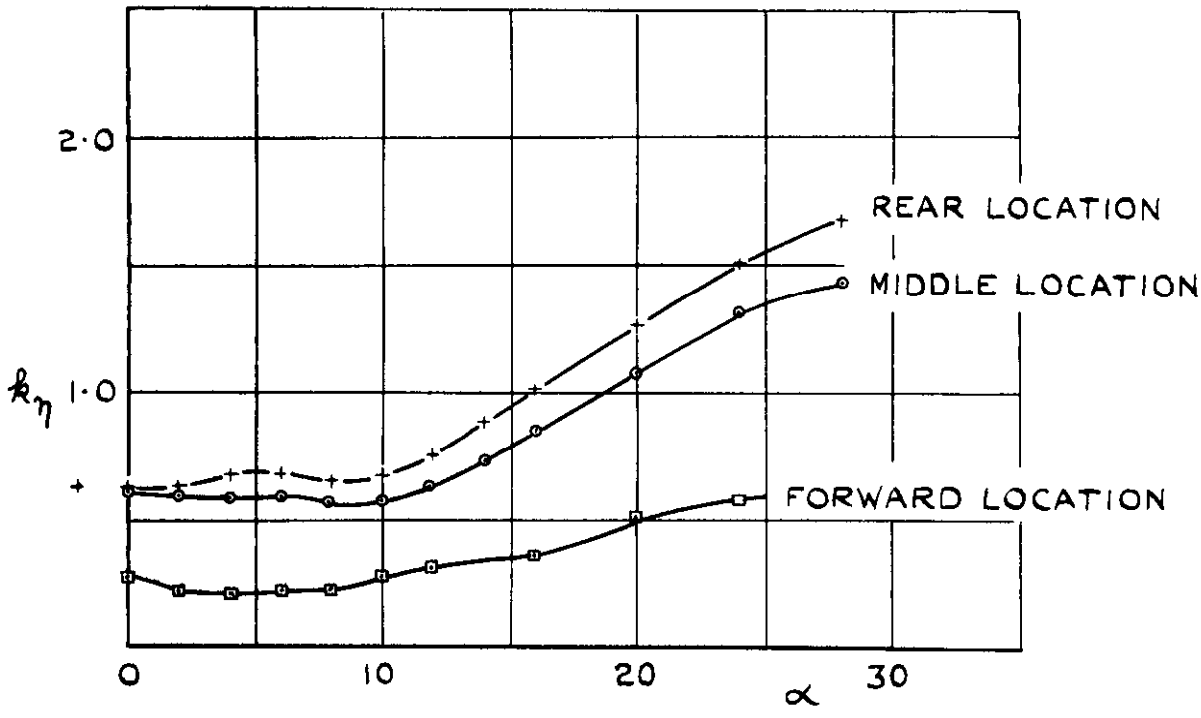


FIG. 19 (a) CONTROL EFFECTIVENESS

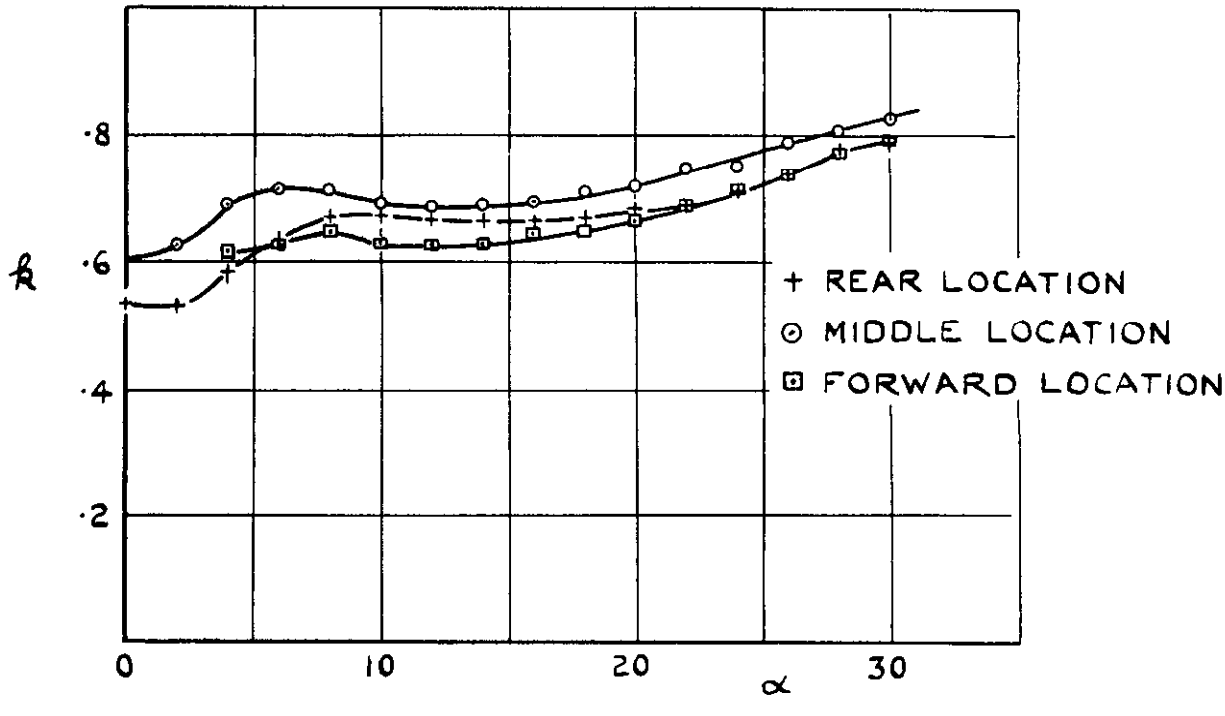


FIG. 19 (b) STABILISING EFFECTIVENESS

FIG.19 CONTROL AND STABILISING EFFECTIVENESS

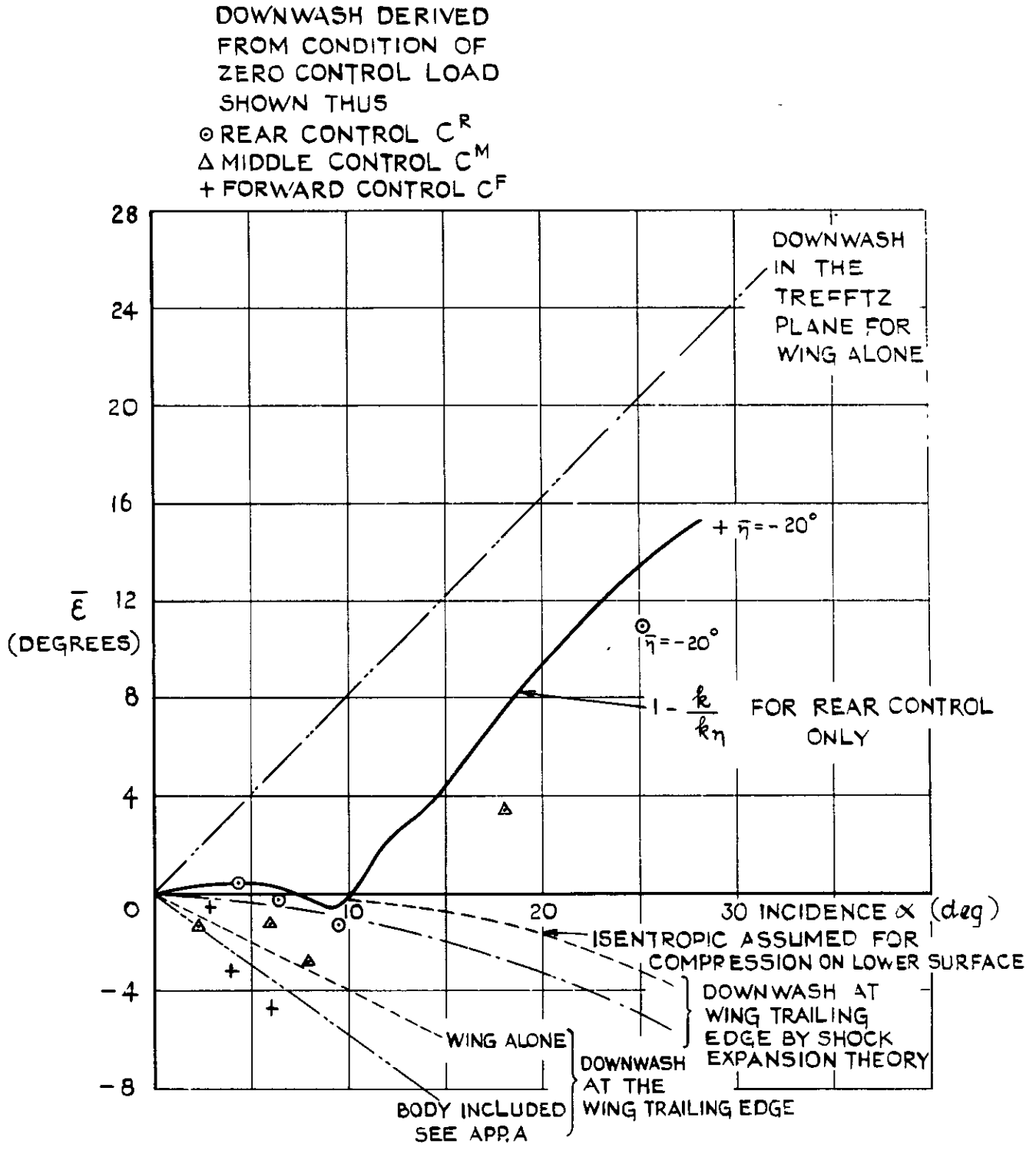


FIG. 20 DOWNWASH ANGLE AT THE CONTROL LOCATIONS

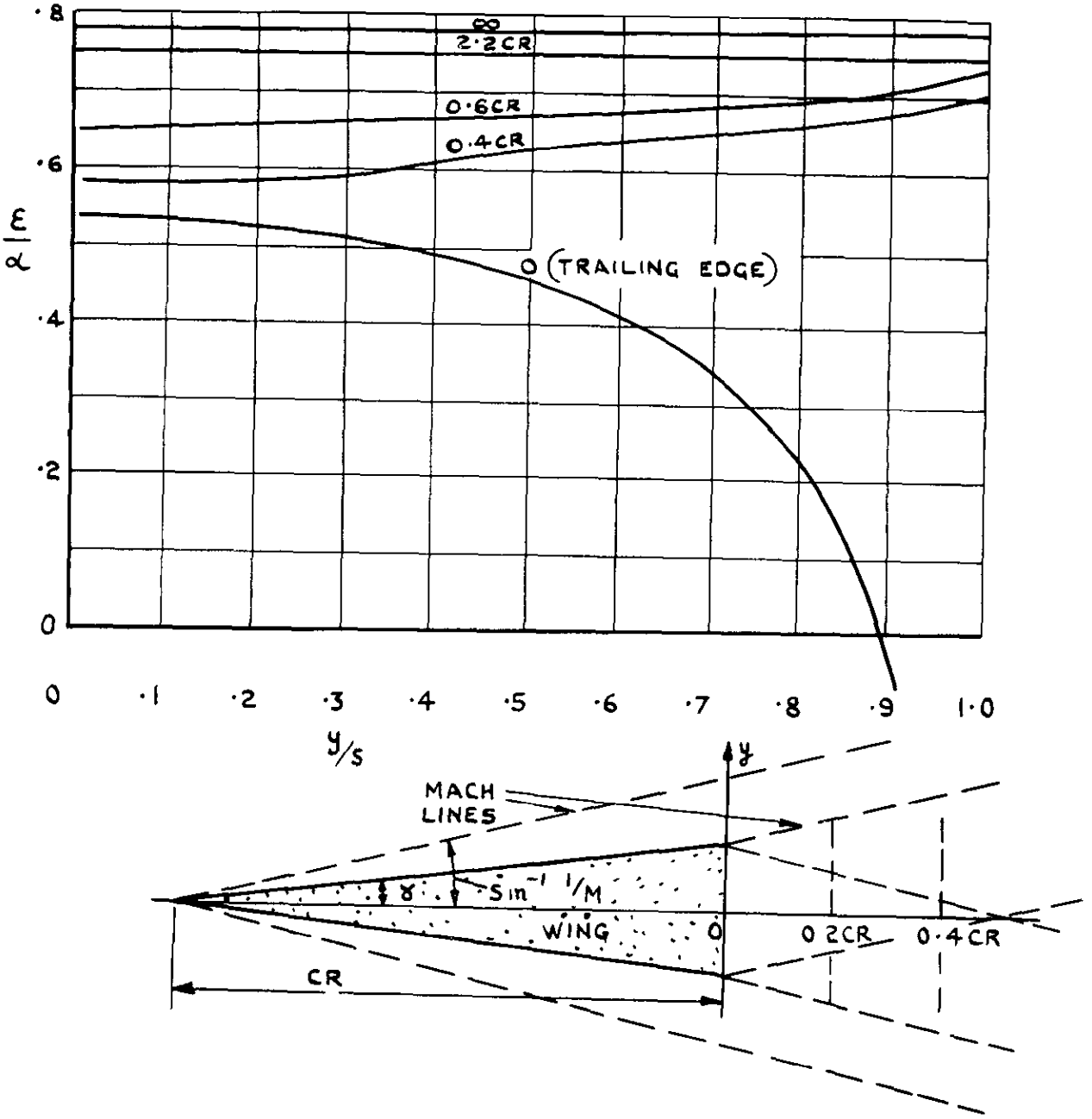


FIG. 21 THEORETICAL VARIATION OF DOWNWASH ACROSS THE SPAN FOR VARIOUS DOWNSTREAM STATIONS (FROM REF. 9) $\beta \tan \gamma = \cdot 6$

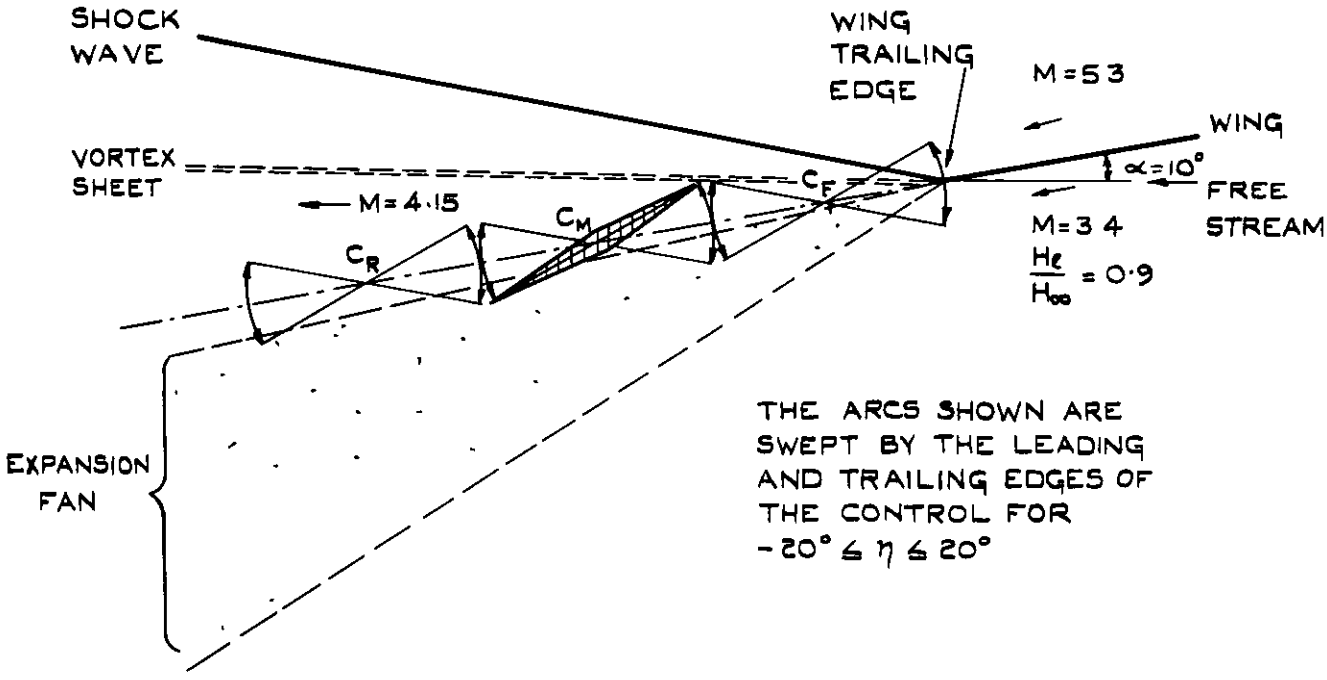


FIG. 22(a) $\alpha = 10^\circ$

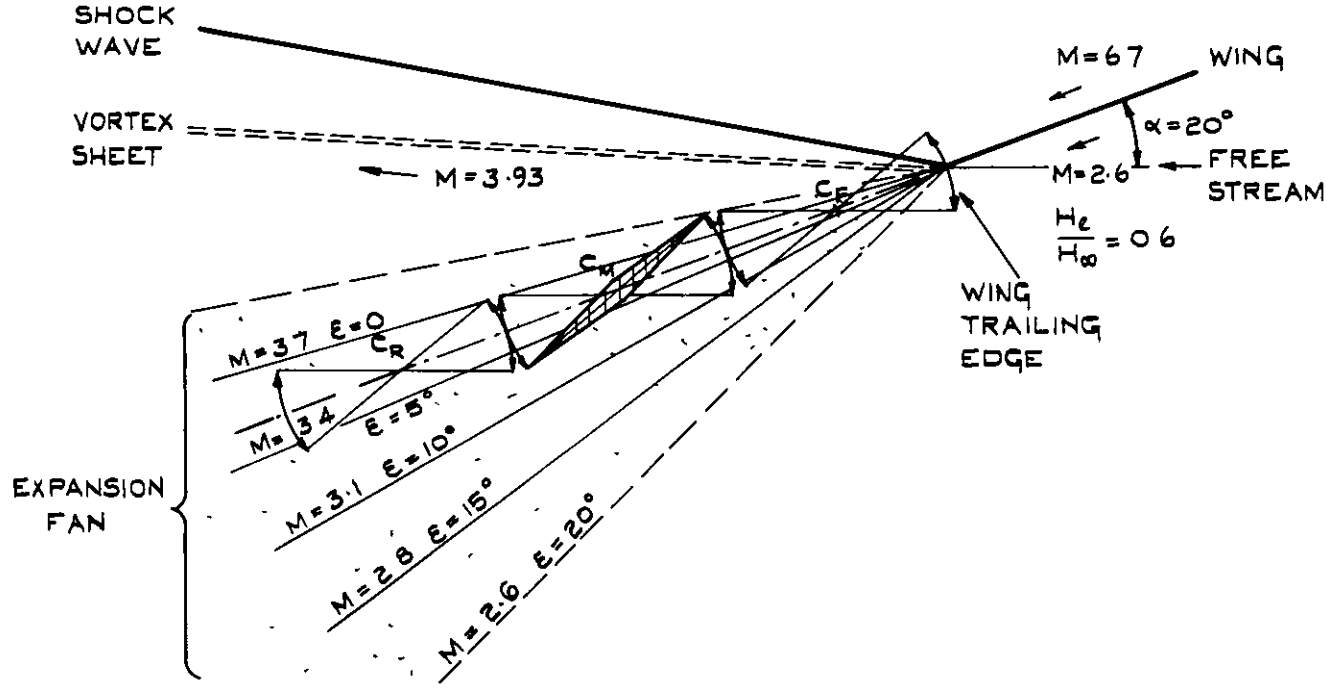


FIG. 22(b) $\alpha = 20^\circ$

FIG. 22 SKETCH OF THE FLOW STRUCTURE NEAR THE WING TRAILING EDGE

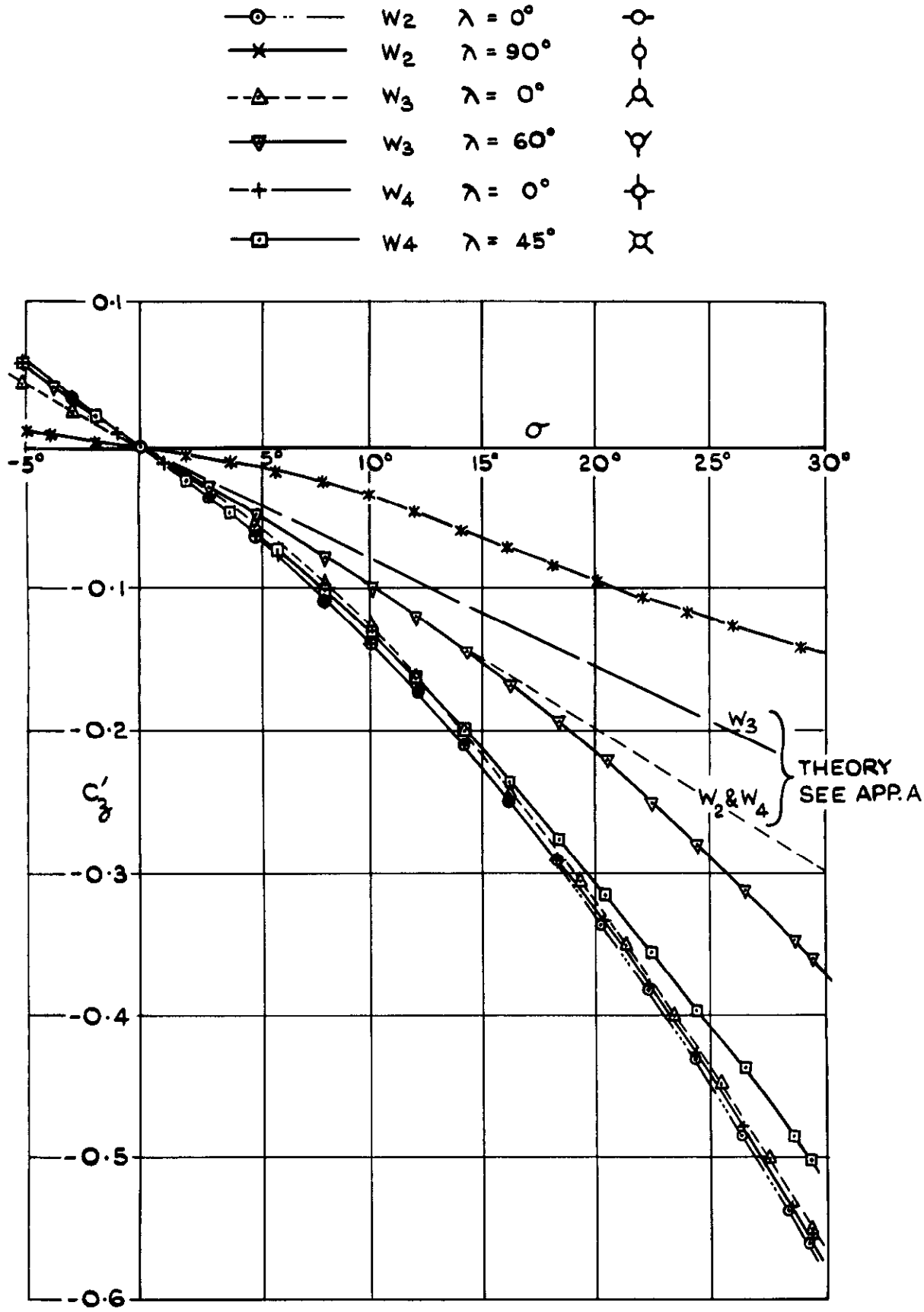


FIG. 23 NORMAL FORCE CHARACTERISTICS FOR W_2, W_3 & W_4

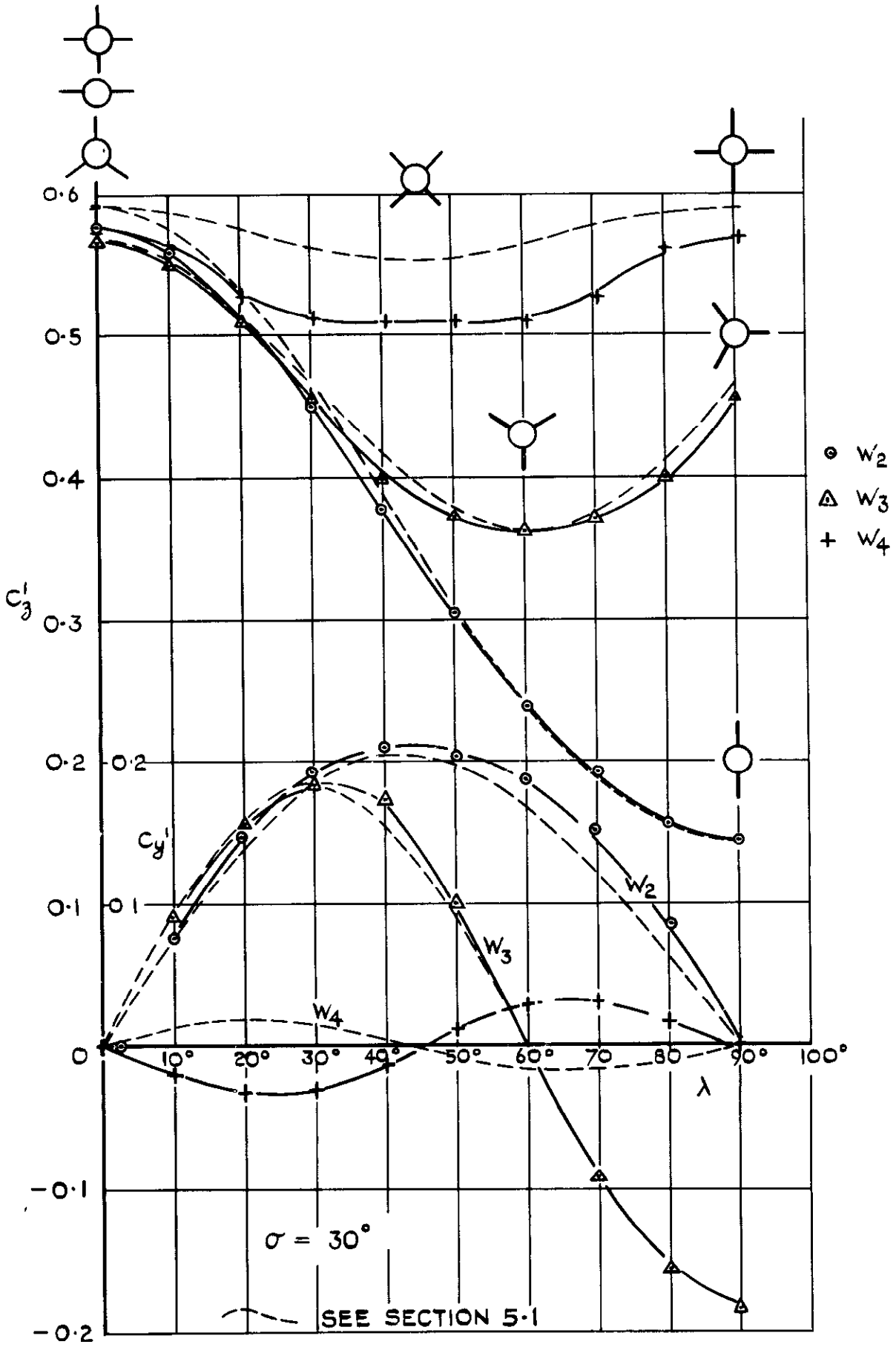


FIG. 24 VARIATION WITH ROLL ANGLE OF THE FORCE IN AND NORMAL TO THE INCIDENCE PLANE FOR MODELS W_2, W_3 AND W_4

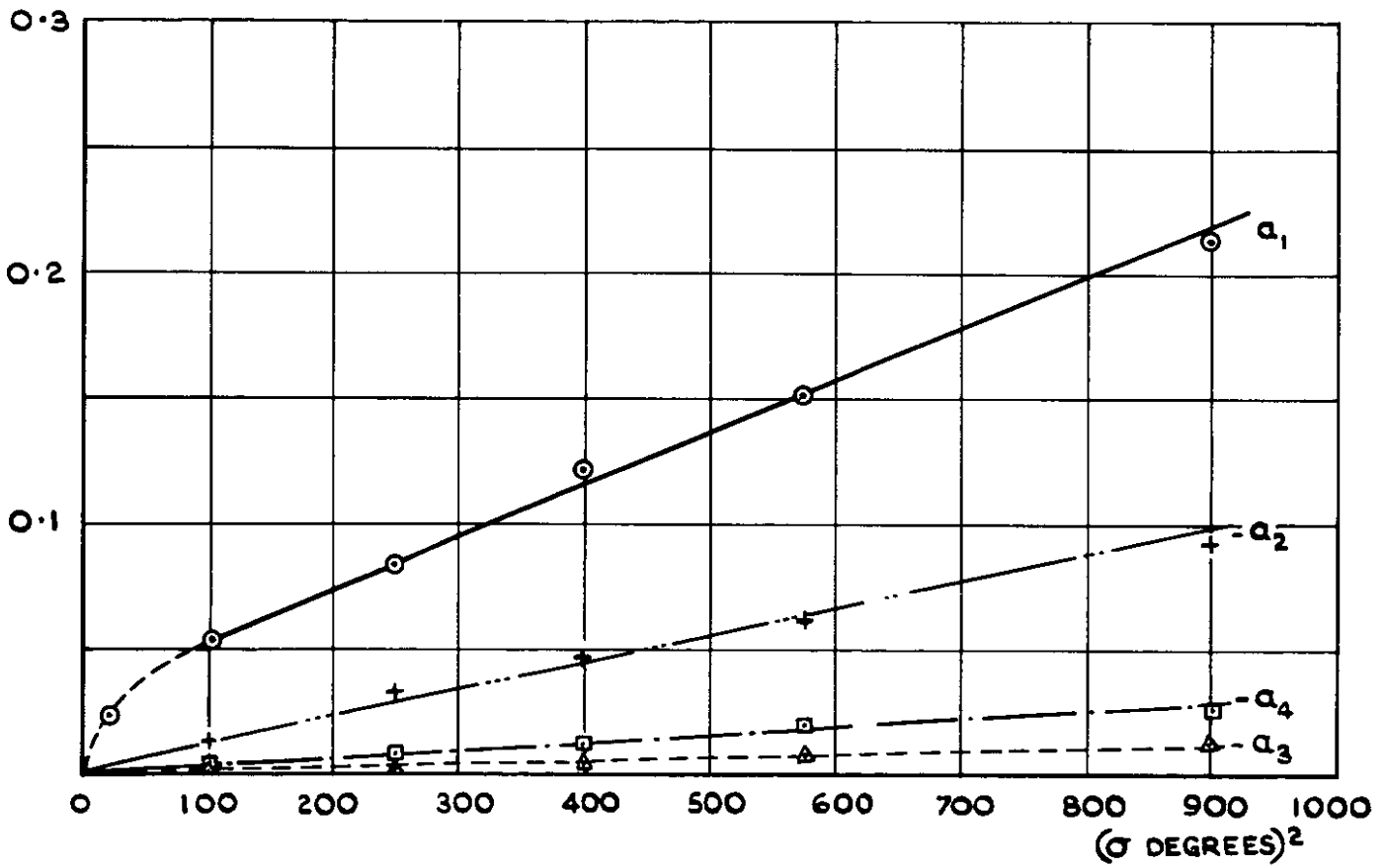


FIG. 25 COEFFICIENTS USED IN EQUATION 9

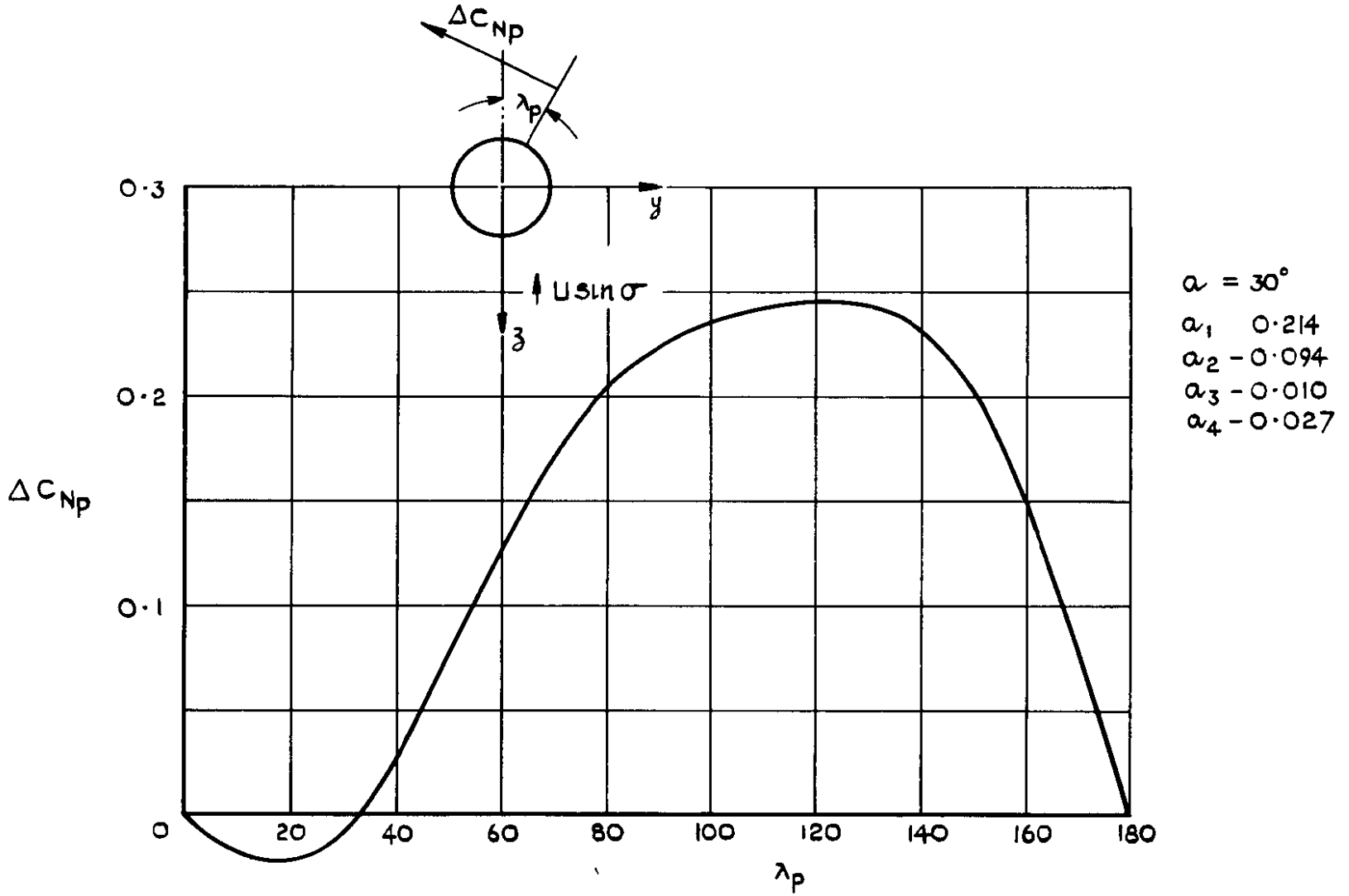


FIG. 26 DERIVED PANEL NORMAL FORCE (SEE EQUATION 9)

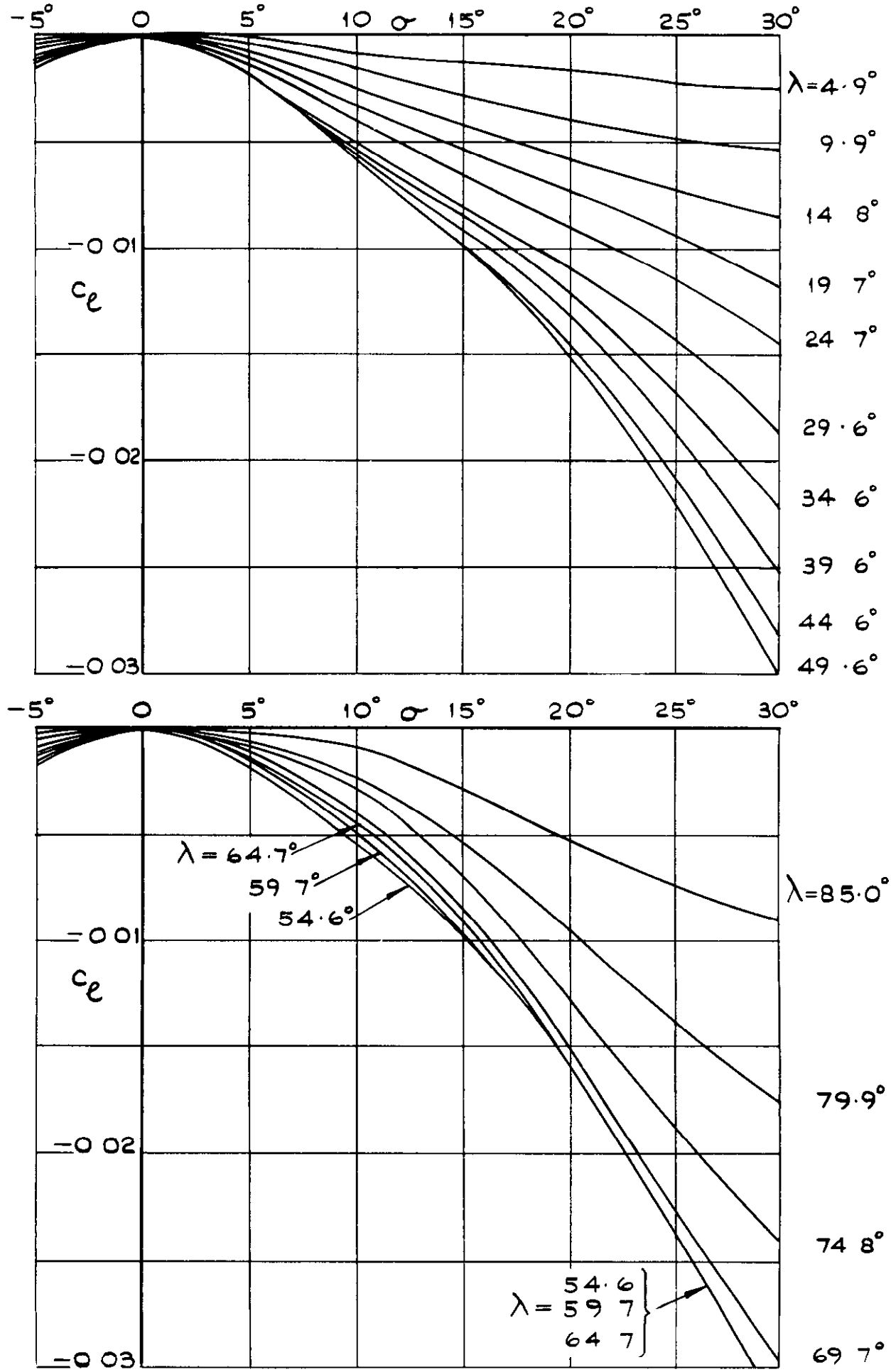


FIG.27 (a) C_ℓ v σ FOR W_2

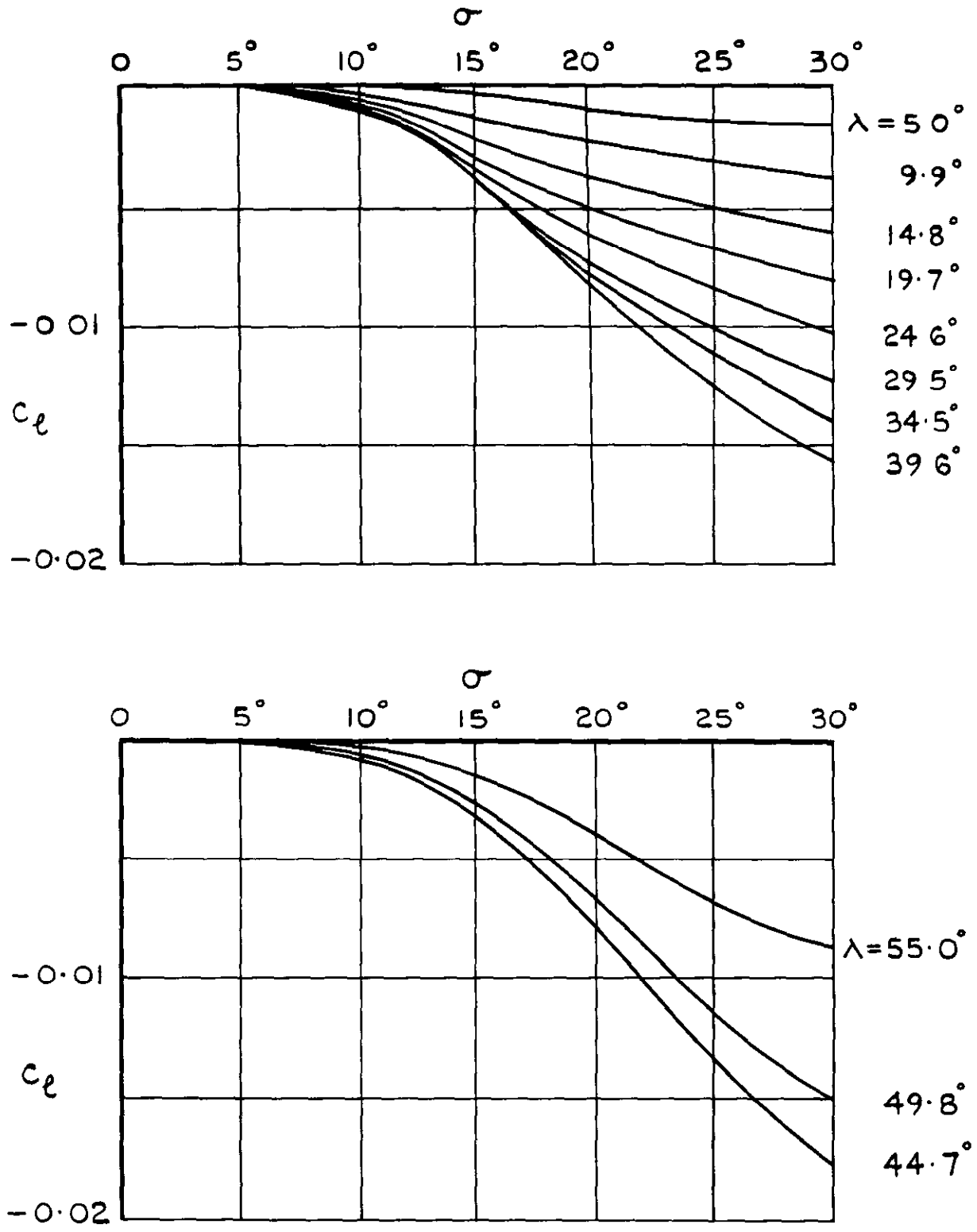


FIG. 27 (b) C_ℓ v σ FOR W_3

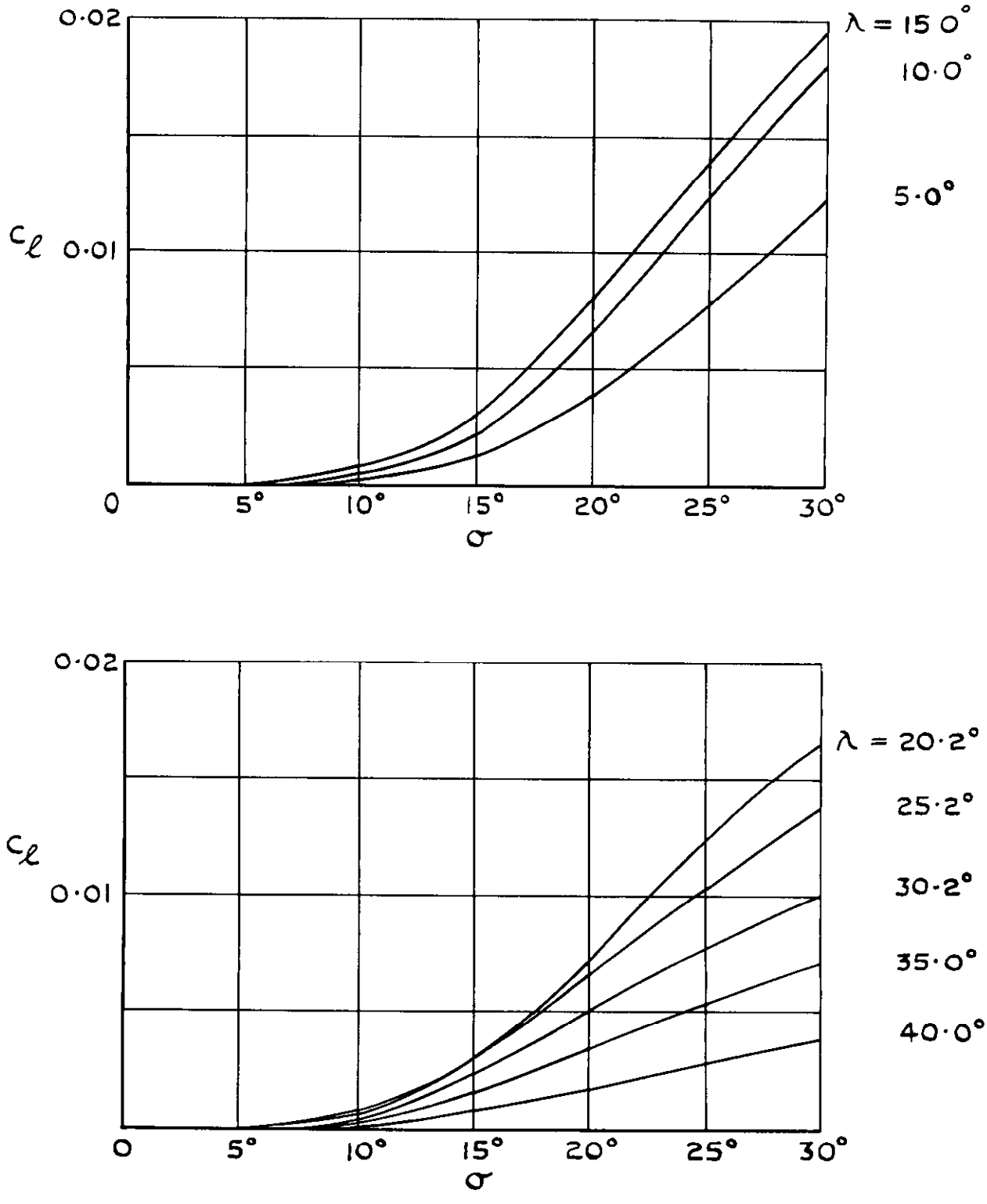


FIG. 27(C) C_ℓ v σ FOR W_4

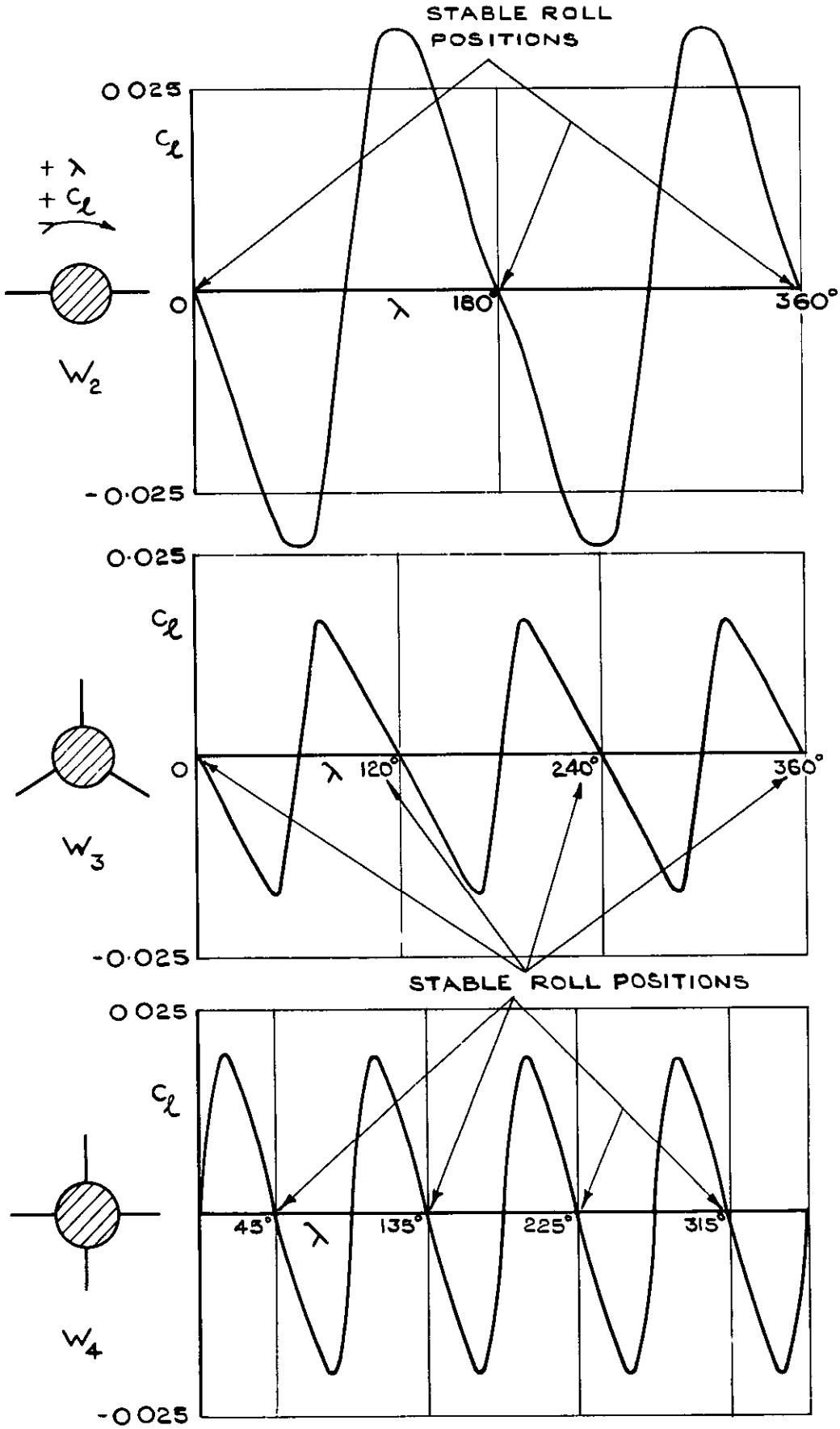


FIG. 28 ROLL STABLE POSITIONS & RELATIVE INDUCED C_ℓ FOR W_2 W_3 & W_4 FOR $\sigma = 30°$

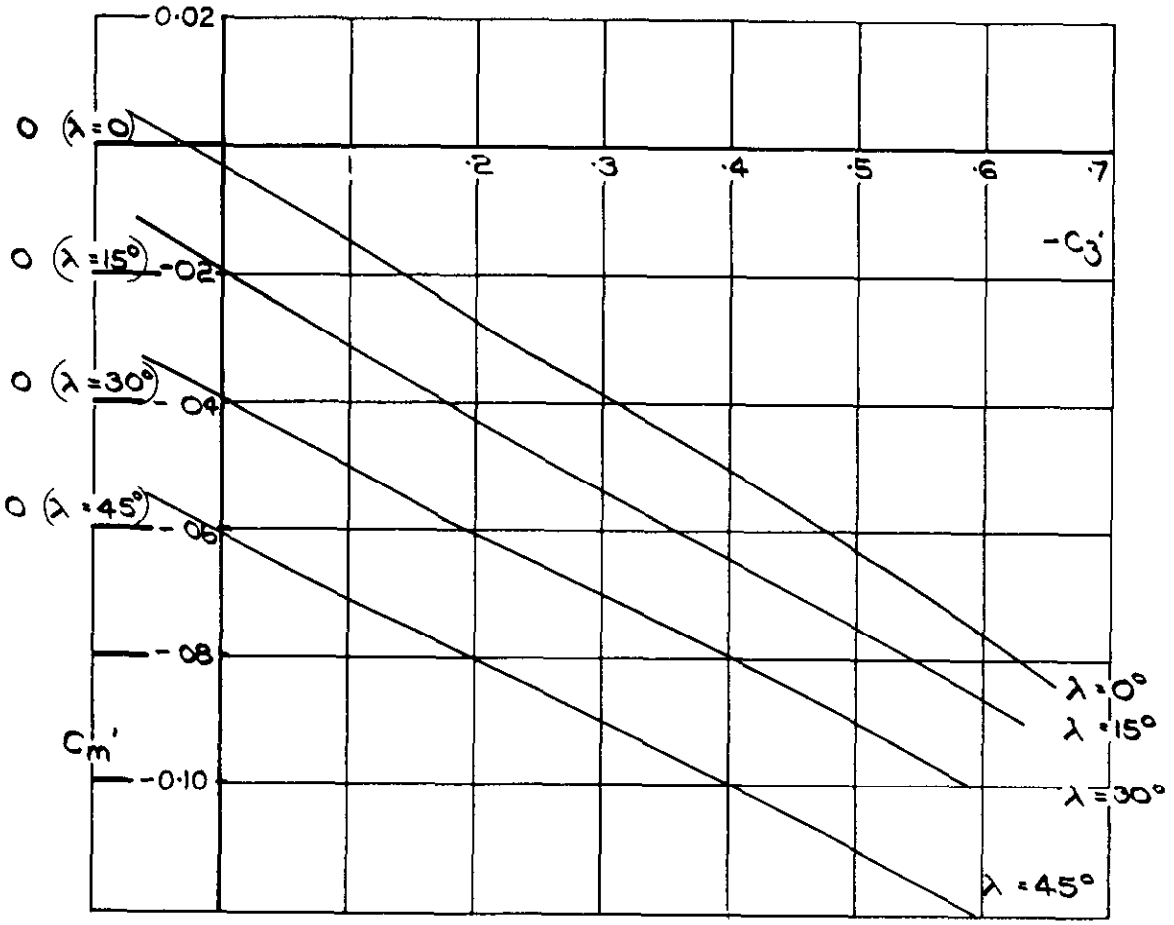


FIG. 29 Cm' v C_3' FOR W_4 BC^R WITH $\eta = 0$
FOR $\lambda = 0, 15, 30$ & 45 DEGREES

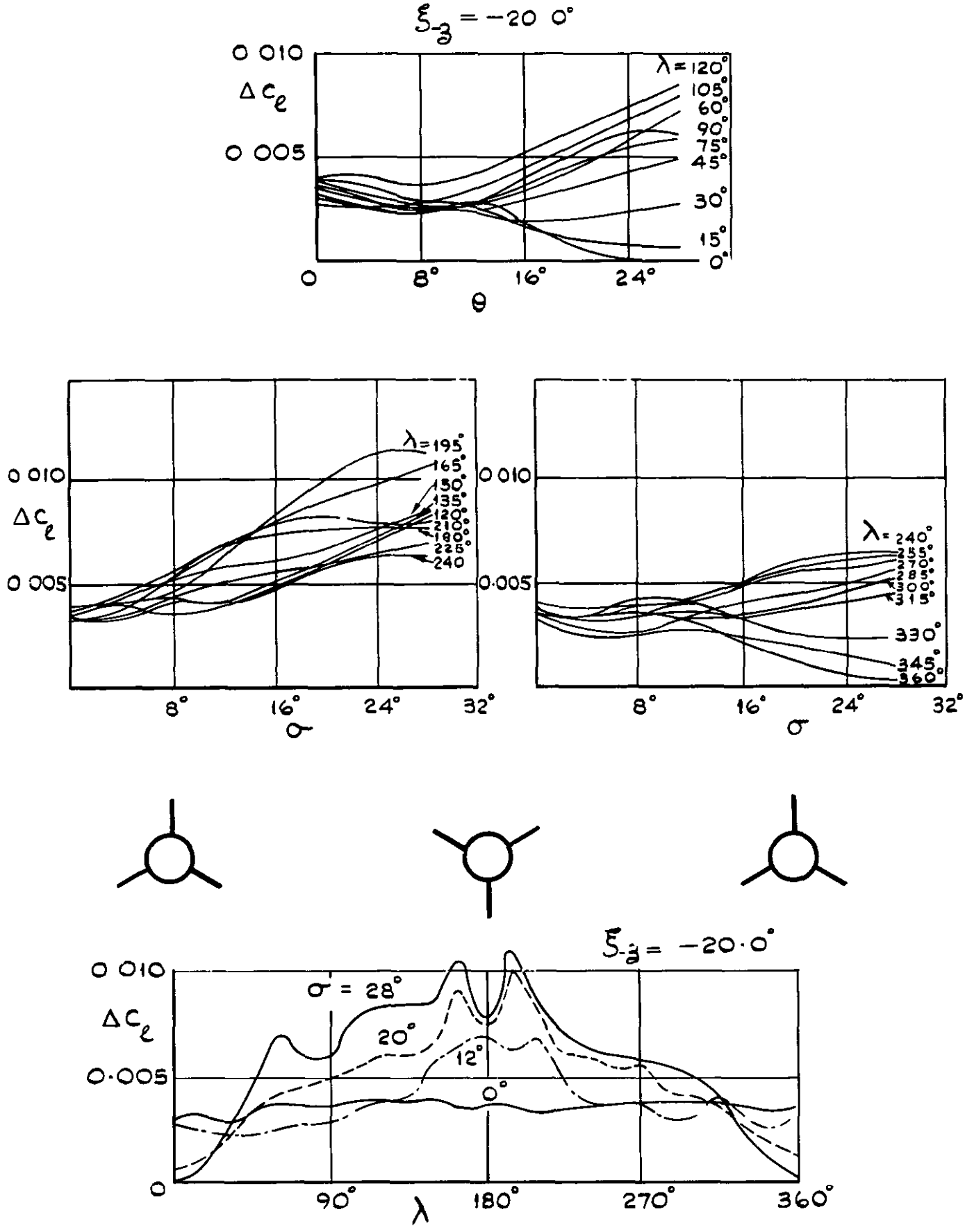


FIG. 30 INCREMENT IN C_ℓ DUE TO MOVEMENT OF ONE CONTROL PANEL ON W_3BC^R

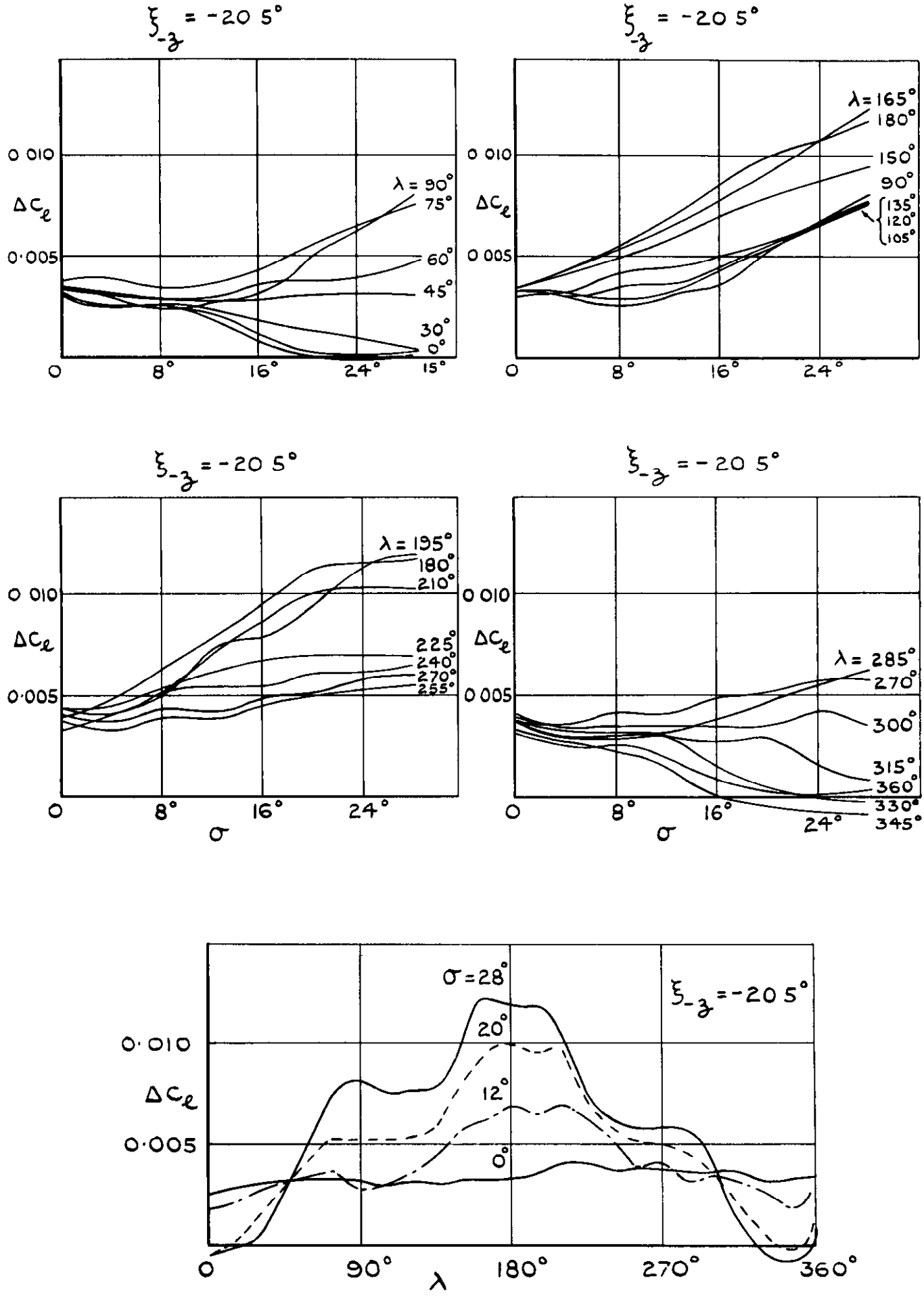


FIG. 31 INCREMENT IN C_ℓ DUE TO MOVEMENT OF ONE CONTROL PANEL ON W_4 B C^R

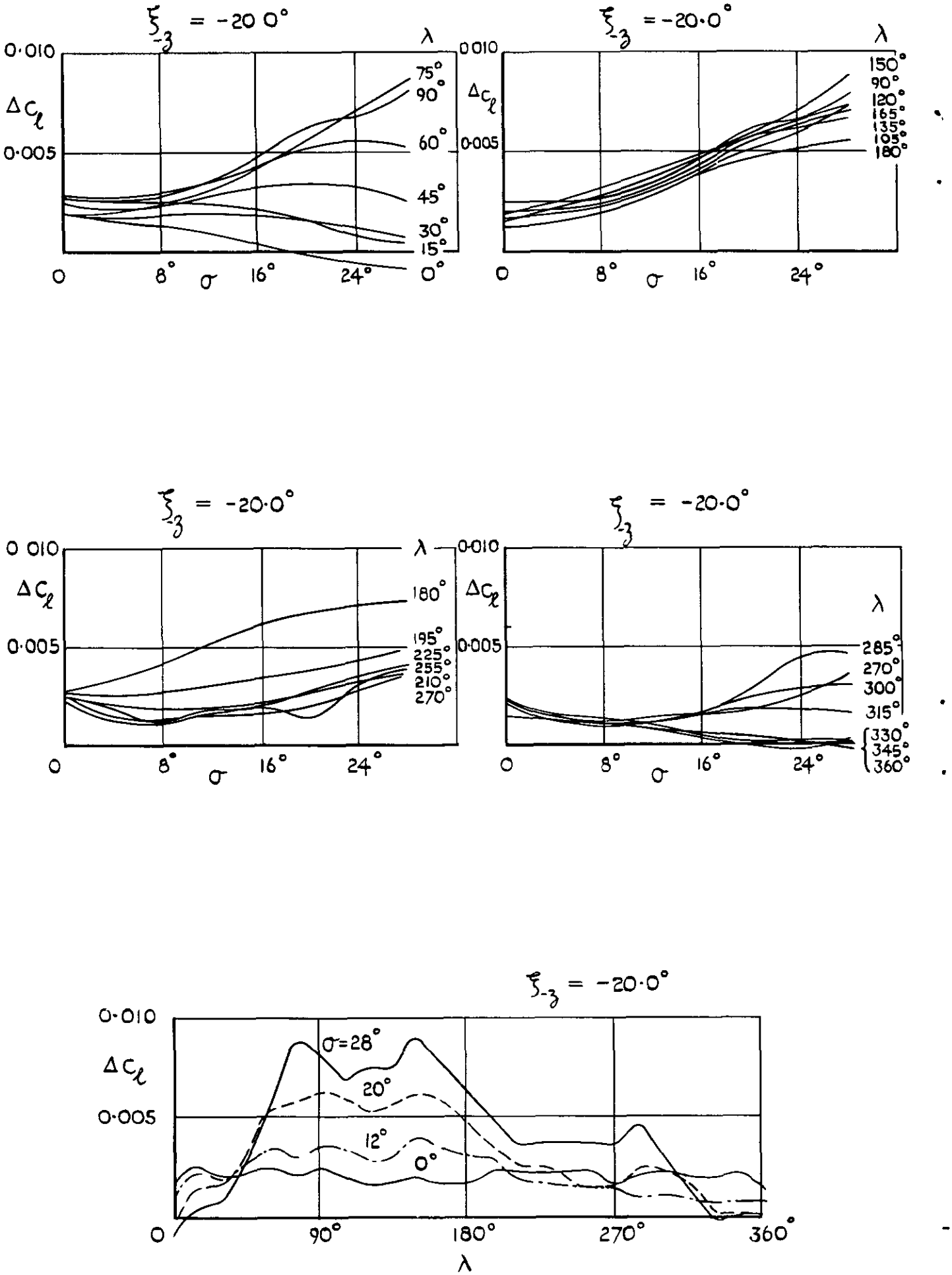


FIG. 32 INCREMENT IN C_ℓ DUE TO MOVEMENT OF ONE CONTROL PANEL ON W_4, BC^F

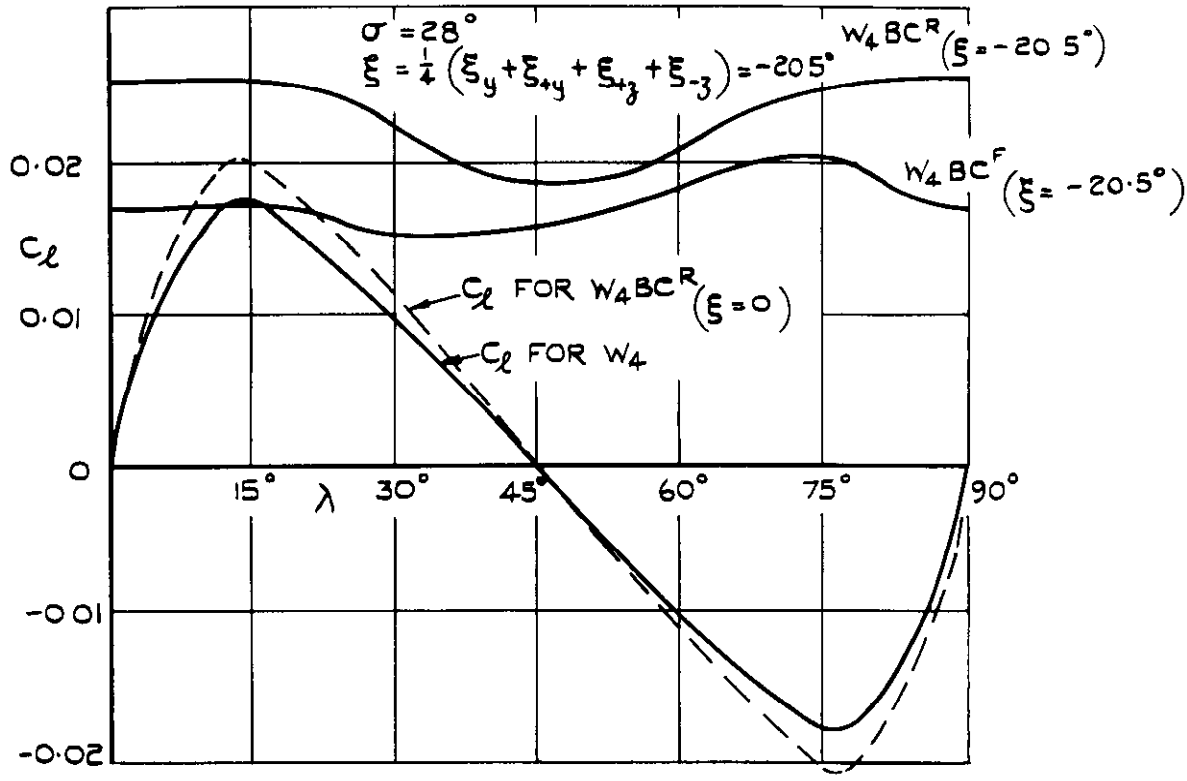


FIG. 33 CONTROL ROLL POWER W_4

$$\sigma = 28^\circ$$
$$\xi = \tfrac{1}{3}\left(\xi_{-z} + \xi_{\text{PORT}} + \xi_{\text{STARBOARD}}\right) = -20{\cdot}0^\circ$$

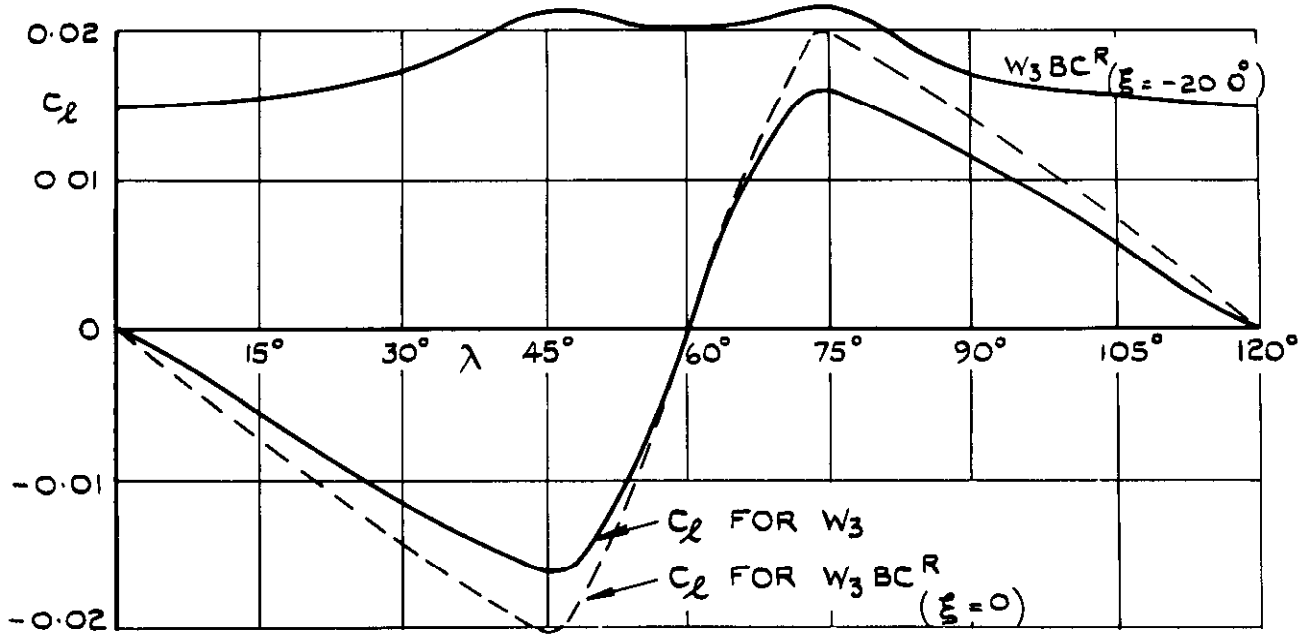


FIG. 34 CONTROL ROLL POWER W_3

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533.693.9 :
533.695.12 :
533.693.3 :
533.694.532 :
533.6.011.5

AERODYNAMIC CHARACTERISTICS AT M = 4.3 OF MONOPLANE, TRIFORM AND CRUCIFORM SLENDER DELTA WING BODIES WITH ALL-MOVING TAIL CONTROL SURFACES

Supersonic wind tunnel tests were made over an incidence range from -4 to +30 degrees for a range of roll angles on a series of conical slender delta wing and body combinations with a short afterbody on which a rectangular tail control surface is mounted.

An examination is made of the characteristics of the wing and body combination and the approximate contributions of the individual wing panels are deduced.

(Over)

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(Over)

The effectiveness of the tail control surfaces as stabilisers and as controls is examined for three different sizes of gap between the control and the wing trailing edge. The non linear behaviour of the controls tested is attributed at low incidences to the viscous losses due to the wing wake, and at high incidence to the influence of the expansion field from the wing trailing edge.

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